

Sta. code	$\Delta$ (deg.)	Az (deg.)	Phase	UTC h min s	Resid (s)	T (s)	A ( $\mu$ m)	Sta. code	$\Delta$ (deg.)	Az (deg.)	Phase	UTC h min s	Resid (s)	T (s)	A ( $\mu$ m)	
<p>MAY 1d 03h 45m 26.4 <math>\pm</math> 0.05s, SD2.30 / 7 40.05 N <math>\pm</math> 0.70km, 103.73 E <math>\pm</math> 0.40km, h12 <math>\pm</math> 0.08km Northern China (323) <math>M_L</math> 3.3 / 6,</p>																
GTA	3.1	259	Pn	03 46 17.2	1.6			SNY	50.3	287	SME				8.0	9.00
			Pg	03 46 22.7	1.8						+iP	16 20 58.4	0.6			
			Sn	03 46 55.0	0.7						PMZ		$m_b = 6.4$	1.2	1.56	
			Sg	03 47 02.0	-1.2						PMZ		$m_B = 6.1$	7.0	4.56	
			SMN		$M_L = 3.0$	0.6	0.068				pP	16 21 47.0	2.8			
			SME			0.6	0.047				ScP	16 25 50.3	3.7			
TIY	7.2	106	ePn	03 47 10.0	-1.7			DL2	53.5	286	iS	16 27 52.0	-1.3			
<p>MAY 1d 11h 44m 35.0 <math>\pm</math> 0.07s, SD1.67 / 189 14.21 N <math>\pm</math> 1.44km, 91.61 W <math>\pm</math> 1.09km, h41 <math>\pm</math> 0.34km Off coast of Chiapas, Mexico (68) <math>M_S</math> 5.8 / 4, <math>m_b</math> 5.0 / 45,</p>																
BJI	120.2	336	ePKP	12 03 22.0	-0.5						SMN			24.0	11.4	
HHC	121.2	340	ePKP	12 03 26.0	1.5						SME			21.0	23.3	
			LZ		$M_S = 5.7$	21.0	1.90				sS	16 29 13.0	-1.5			
WMQ	122.3	1	ePKP	12 03 27.0	0.4						ScS	16 30 24.0	1.1			
			LN		$M_S = 5.6$	20.0	0.77				P	16 21 22.0	0.5			
TIY	123.6	337	ePKP	12 03 31.1	1.8						PMZ		$m_b = 6.1$	1.0	0.53	
			PP	12 05 15.0	-0.3						PMZ		$m_B = 6.1$	4.0	2.23	
			LN		$M_S = 5.9$	21.0	1.43				pP	16 22 10.0	1.7			
			LZ		$M_S = 5.4$	26.0	1.14				sP	16 22 37.0	5.2			
SSE	125.0	325	PKP	12 03 34.0	2.2			BJI	55.3	291	S	16 28 35.0	-0.5			
			PPMZ			16.0	0.44				SMN			15.0	4.31	
			LE		$M_S = 5.4$	14.0	0.32				SME			10.0	7.10	
			LZ		$M_S = 5.5$	20.0	0.92				LN			13.0	7.24	
NJ2	125.5	328	PKP	12 03 32.0	-0.8						LE			14.0	7.56	
			PP	12 05 26.0	-1.6						LZ			30.0	7.73	
			LZ		$M_S = 5.2$	16.0	0.41				eP	16 21 34.0	-0.5			
GTA	125.6	349	ePKP	12 03 35.0	1.9						PMZ		$m_b = 6.0$	1.0	0.39	
			LZ		$M_S = 5.4$	22.0	0.93				PMZ		$m_B = 6.2$	4.0	2.34	
LZH	127.9	344	ePKP	12 03 39.5	1.9						epP	16 22 24.0	2.3			
			LZ		$M_S = 5.6$	22.0	1.46				esP	16 22 46.0	0.9			
XAN	128.2	338	PKP	12 03 38.7	0.6						eS	16 29 00.0	-0.7			
WHN	129.0	331	ePKP	12 03 41.5	2.0						esS	16 30 24.0	0.9			
CD2	132.8	342	PKP	12 03 50.4	3.6						eScS	16 30 57.0	-0.8			
			PP	12 06 12.0	-2.3						LN			15.0	8.13	
			LZ		$M_S = 5.5$	21.0	1.04				LZ			24.0	8.91	
GYA	135.8	336	PKP	12 03 54.6	2.0			HHC	56.9	295	-iP	16 21 47.0	1.1			
KMI	138.5	340	ePKP	12 03 59.5	2.0						PMZ		$m_b = 6.3$	1.0	0.75	
<p>MAY 1d 16h 12m 20.4 <math>\pm</math> 0.03s, SD0.96 / 732 58.85 N <math>\pm</math> 0.61km, 156.94 W <math>\pm</math> 0.45km, h213 <math>\pm</math> 0.37km Alaska Peninsula (12) <math>m_B</math> 6.2 / 42, <math>m_b</math> 6.0 / 122,</p>																
MDJ	45.3	286	+P	16 20 18.7	-0.3						pP	16 22 35.0	1.8			
			PMZ		$m_b = 5.8$	1.0	0.30				sP	16 23 02.0	5.5			
			PMZ		$m_B = 5.8$	4.0	1.30				S	16 29 20.0	-0.3			
			PP	16 22 12.0	4.0						LN			13.0	9.52	
			iS	16 26 42.0	-0.8						LE			14.0	6.54	
			SMN			11.0	4.10				LZ			12.0	7.10	
			LN			18.0	20.4				+P	16 21 53.1	0.6			
			LZ			20.0	11.7				S	16 29 29.0	-3.8			
CN2	47.9	288	+iP	16 20 40.0	0.3			TIA	57.8	288	SMN			12.0	1.87	
			PMZ		$m_b = 6.0$	1.0	0.50				SME			11.0	5.90	
			PMZ		$m_B = 6.3$	4.0	3.80				LN			19.0	12.4	
			pP	16 21 26.0	0.3						LE			15.0	7.94	
			sP	16 21 50.0	0.7						LZ			30.0	8.52	
			PP	16 22 33.0	-0.1			TIY	58.9	292	eP	16 22 00.5	0.3			
			S	16 27 20.0	0.7						PMZ		$m_b = 6.1$	1.1	0.46	
			SMN			8.0	5.00				pP	16 22 50.0	2.1			
<p>MAY 1d 16h 12m 20.4 <math>\pm</math> 0.03s, SD0.96 / 732 58.85 N <math>\pm</math> 0.61km, 156.94 W <math>\pm</math> 0.45km, h213 <math>\pm</math> 0.37km Alaska Peninsula (12) <math>m_B</math> 6.2 / 42, <math>m_b</math> 6.0 / 122,</p>																
											sP	16 23 15.5	4.4			
											iS	16 29 52.0	3.5			
											LN			12.0	6.99	
											LZ			15.0	9.23	
								SSE	59.9	281	+P	16 22 06.5	0.2			
											PMZ		$m_b = 6.1$	1.2	0.50	



		PMZ	$m_b = 6.3$	4.0	2.35			ScS	16 32 20.0	1.1		
		pP	16 22 52.0	-2.3				LN			17.0	3.04
		sP	16 23 21.0	3.5				LZ			28.0	3.71
		PP	16 24 21.0	-1.1		CD2	68.6 294	P	16 23 02.9	-0.2		
		ScP	16 26 31.0	2.7				PMZ	$m_b = 6.3$		1.2	0.71
		iS	16 30 00.0	-0.1				pP	16 23 54.0	1.7		
		sS	16 31 25.0	1.5				sP	16 24 20.0	5.0		
		ScS	16 31 31.0	0.0				S	16 31 49.0	2.7		
		SS	16 34 00.0	0.0				ScS	16 32 41.0	3.1		
		LE			15.0			sS	16 33 18.0	4.9		
		LZ			20.0			LE			13.0	4.40
NJ2	60.3 283	-iP	16 22 08.8	-0.3				LZ			18.0	5.90
		PMZ	$m_b = 6.0$	0.8	0.25	GZH	70.4 282	cP	16 23 14.6	0.8		
		PMZ	$m_b = 6.1$	4.0	1.77			PMZ	$m_b = 6.1$		1.0	0.37
		pP	16 22 57.5	0.3				PMZ	$m_b = 6.4$		4.0	2.95
		PP	16 24 28.3	2.4				pP	16 24 06.0	2.7		
		ScP	16 26 33.0	2.8				iS	16 32 08.0	-0.4		
		iS	16 30 04.0	-1.4				sS	16 33 36.0	1.8		
		ScS	16 31 37.0	2.9				LN			12.0	2.15
		SS	16 34 10.0	3.5				LE			14.0	4.97
GTA	63.4 302	+iP	16 22 30.0	0.0				LZ			20.0	3.14
		PMZ	$m_b = 6.5$	1.2	1.05	GYA	70.9 290	P	16 23 17.6	0.4		
		PMZ	$m_b = 6.4$	4.5	3.79			PMZ	$m_b = 5.9$		1.6	0.43
		S	16 30 40.0	-3.2				PMZ			3.0	3.20
		ScS	16 32 01.4	3.9				pP	16 24 09.0	2.5		
		LE			14.0			S	16 32 16.0	2.9		
		LZ			38.0			sS	16 33 42.0	1.5		
XAN	63.6 292	-P	16 22 32.0	0.8				LN			20.0	7.90
		PMZ	$m_b = 6.2$	6.0	2.80			LE			20.0	8.40
		pP	16 23 20.0	0.3				+iP	16 23 29.0	1.7		
		sP	16 23 45.0	2.3				PMZ	$m_b = 6.7$		4.0	6.80
		S	16 30 50.0	4.4				pP	16 24 22.0	5.2		
		LN			12.0			PP	16 26 13.0	0.0		
		LE			12.0			iS	16 32 36.0	1.9		
WHN	63.8 286	+P	16 22 32.5	0.2				SME			8.0	11.5
		PMZ	$m_b = 6.2$	1.5	0.67	KMI	73.9 292	-P	16 23 35.0	0.0		
		PMZ	$m_b = 6.4$	4.0	3.31			PMZ	$m_b = 6.3$		2.5	1.70
		PcP	16 23 08.0	2.4				PMZ	$m_b = 6.1$		6.0	2.30
		pP	16 23 22.0	1.1				sP	16 24 50.0	2.9		
		S	16 30 50.0	2.2				iS	16 32 48.0	-0.9		
		LN			14.0			ScS	16 33 20.0	-0.1		
		LE			14.0			sS	16 34 17.0	1.9		
		LZ			16.0			LN			18.0	7.80
LZH	64.3 297	+P	16 22 36.0	0.0				LE			14.0	4.20
		PMZ	$m_b = 6.4$	2.0	1.63			LZ			20.0	6.40
		PMZ	$m_b = 6.5$	4.0	3.97	LSA	75.4 303	-P	16 23 45.0	1.5		
		PcP	16 23 07.0	-0.9				iS	16 33 07.0	1.7		
		pP	16 23 26.0	1.5				SME			11.0	5.30
		PP	16 25 02.0	0.9				SS	16 38 03.0	2.3		
		PcS	16 27 10.0	0.1				LE			15.0	3.76
		S	16 30 55.0	0.5				+P	16 23 45.8	1.8		
		SME			12.0			PMZ	$m_b = 6.2$		1.0	0.48
		sS	16 32 25.0	4.7				pP	16 24 36.0	2.0		
		LN			12.0			PP	16 26 36.0	-1.2		
		LE			15.0			S	16 33 09.0	4.2		
		LZ			36.0			sS	16 34 35.0	1.6		
WMQ	64.7 314	-iP	16 22 38.7	0.6				SS	16 38 04.0	0.2		
		PMZ	$m_b = 6.4$	8.0	6.24							
		ScP	16 26 50.0	0.4				MAY 1d 21h 13m $17.4 \pm 0.57s$ , SD3.45 / 9				
		PcS	16 27 09.5	-1.9				29.96 N $\pm 3.05km$ , 90.36 E $\pm 3.78km$ , h13 $\pm 1.02km$				
		S	16 31 05.0	6.4				Tibet (306)				
		SME			22.0			GYA	14.8 100	P	21 16 46.2	-2.3
		LZ			34.0			TIY	19.9 61	eP	21 17 51.8	0.2
QZH	66.2 279	P	16 22 47.3	-0.5				MAY 2d 01h 01m $23.9 \pm 0.05s$ , SD0.97 / 290				
		PMZ	$m_b = 5.9$	1.0	0.24			49.32 N $\pm 0.95km$ , 155.54 E $\pm 0.70km$ , h94 $\pm 0.09km$				
		PMZ	$m_b = 6.3$	4.0	2.21			Kurile Islands (221)				
		pP	16 23 37.0	0.2				$m_b 4.8 / 1, m_b 5.1 / 81,$				
		S	16 31 19.0	1.8								



MDJ	18.3	265	+P	01 05 32.7	-0.1				KMI	47.3	259	-P	01 09 51.0	0.5			
			PMZ		$m_b = 5.0$	1.0	0.070					PMZ		$m_b = 5.5$	1.5	0.10	
			pP	01 05 46.0	-2.4							pP	01 10 10.0	-2.2			
			iS	01 08 54.0	3.6							eS	01 16 40.0	3.6			
			LE			12.0	0.90					LZ			20.0	0.90	
			LZ			24.0	4.50		QZN	47.4	247	eP	01 09 51.3	0.6			
CN2	21.3	266	P	01 06 02.0	-3.0							S	01 16 42.0	6.3			
			PMZ		$m_b = 4.8$	1.0	0.050					LE			15.0	-1.10	
			eS	01 09 53.0	1.5				LSA	51.8	273	P	01 10 25.4	0.4			
			LN			16.0	1.60		-----								
			LE			16.0	1.50		MAY 2d 02h 15m $42.7 \pm 0.04s$ , SD3.11 / 6								
			LZ			22.0	3.50		42.21 N $\pm 0.45km$ , 79.98 E $\pm 0.51km$ , $h \pm km$								
SNY	23.5	264	eP	01 06 26.0	0.2				Kirgiziya-Xinjiang border region (320)								
			PMZ		$m_b = 4.8$	1.2	0.050		$M_L 3.9 / 6$ ,								
			pP	01 06 44.0	-2.0				KSH	4.1	230	Pn	02 16 49.0	2.7			
			S	01 10 28.0	-0.5							Sg	02 17 45.5	-5.3			
			LZ			20.0	2.06					SMN		$M_L = 4.1$	0.6	0.40	
BJI	29.2	267	eP	01 07 18.5	-0.5							SME			0.5	0.40	
			PMZ		$m_b = 4.8$	1.2	0.023		WMQ	5.9	72	ePn	02 17 14.0	3.0			
			ePP	01 08 16.0	-0.7							Sg	02 18 54.0	7.0			
			eS	01 12 07.0	3.5							SMN		$M_L = 3.8$	0.8	0.070	
			LN			15.0	1.02					SME			0.8	0.090	
			LZ			20.0	2.10		-----								
SSE	31.6	248	P	01 07 39.7	-0.2				MAY 2d 04h 19m $40.6 \pm 0.04s$ , SD1.40 / 168								
			PMZ		$m_b = 5.3$	1.0	0.050		$0.07 N \pm 0.79km$ , $124.28 E \pm 1.18km$ , $h 100 \pm 0.28km$								
			pP	01 07 59.0	-1.9				Minahassa Peninsula (Celebes) (265)								
			eS	01 12 46.0	5.2				$m_b 5.4 / 27$ ,								
			eSS	01 14 36.0	0.6				QZN	23.6	324	P	04 24 44.4	1.4			
			LN			14.0	0.75					eS	04 28 49.5	2.7			
			LZ			20.0	1.38					LN			13.0	0.60	
HHC	31.8	271	P	01 07 41.0	-1.0							LE			12.0	0.50	
NJ2	32.3	252	+P	01 07 46.6	0.0				GZH	25.2	336	eP	04 24 59.0	0.1			
			PMZ		$m_b = 5.0$	1.2	0.030					PMZ		$m_b = 5.3$	0.9	0.080	
			S	01 12 58.0	6.0							eS	04 29 14.0	-0.7			
			LZ			22.0	1.01		QZH	25.3	348	eP	04 25 01.4	1.6			
TIY	32.9	266	-P	01 07 51.2	-0.5				SSE	31.0	355	eP	04 25 50.5	-0.4			
			PMZ		$m_b = 5.4$	1.2	0.080					eS	04 30 46.0	-1.3			
			LE			21.0	1.71					LZ			20.0	0.46	
			LZ			30.0	1.57		GYA	31.2	328	-P	04 25 54.4	1.1			
BTO	32.9	272	eP	01 07 51.0	-1.0							PcP	04 28 46.0	1.1			
			eS	01 13 05.0	2.6				WHN	31.7	344	eP	04 25 59.2	1.7			
			LN			15.0	0.80		NJ2	32.2	351	eP	04 26 03.0	1.4			
			LE			15.0	1.60		KMI	32.5	322	+P	04 26 05.5	1.3			
			LZ			15.0	2.00					PMZ		$m_b = 5.1$	1.5	0.050	
WHN	36.2	254	-P	01 08 19.5	0.0				CD2	36.3	329	P	04 26 37.0	0.1			
			PMZ		$m_b = 5.3$	1.0	0.050					PMZ		$m_b = 5.3$	0.9	0.050	
XAN	37.4	264	P	01 08 28.5	-1.2				XAN	36.7	338	P	04 26 39.0	-1.3			
QZH	37.6	243	eP	01 08 32.3	0.6				TIY	39.0	345	eP	04 26 58.2	-1.1			
LZH	39.5	270	P	01 08 47.5	0.4				BJI	40.5	350	eP	04 27 10.0	-1.1			
			PMZ		$m_b = 5.4$	1.4	0.098					PMZ		$m_b = 5.3$	1.2	0.057	
			pP	01 09 04.5	-4.0							eScP	04 32 55.0	4.2			
			eS	01 14 44.0	1.6							eS	04 33 10.0	-2.3			
			SS	01 17 32.0	-0.7							eSS	04 36 11.0	1.1			
			LN			15.0	1.30		LZH	40.6	334	P	04 27 11.7	-0.4			
			LE			13.0	0.87					PMZ		$m_b = 5.4$	1.4	0.091	
			LZ			24.0	2.36					pP	04 27 34.5	-0.4			
GTA	40.2	277	eP	01 08 53.4	0.1							PcP	04 29 13.0	0.5			
			LE			16.0	2.22					eSS	04 36 16.0	3.6			
			LZ			16.0	3.49					LZ			22.0	0.80	
GZH	42.2	247	eP	01 09 08.6	-0.5				SNY	41.6	359	+P	04 27 19.6	-0.6			
			eS	01 15 22.0	0.0							eS	04 33 27.0	-1.8			
CD2	42.7	264	P	01 09 14.4	0.5							esS	04 34 14.0	5.2			
GYA	43.9	257	+iP	01 09 24.0	0.8							LZ			26.0	0.81	
			pP	01 09 43.0	-1.9												
			S	01 15 50.0	4.1				HHC	42.2	346	eP	04 27 26.0	0.4			
			LZ			12.0	0.86		BTO	42.4	344	eP	04 27 27.3	0.3			
WMQ	45.5	290	P	01 09 37.8	1.4				CN2	43.5	1	eP	04 27 36.0	-0.4			
			LE			14.0	1.53					eS	04 33 56.0	-1.7			
			LZ									LZ			24.0	0.50	







GZH	45.9 310	LZ	$M_s=5.9$	20.0	13.8	PP	23 01	45.0	1.5	MDJ	53.3 342	-iP	22 59	44.2	1.2	SMN	10.0	7.48																																					
		-P	22 58	47.4	1.0		S	23 07	02.5			-0.5	SME	10.0	5.16																																								
		PMZ	$m_b=5.6$	1.0	0.075		LN	$M_s=5.9$	14.0			4.11	LE	15.0	4.10																																								
		PMZ	$m_B=6.7$	7.0	7.72		LZ	$M_s=5.2$	40.0			4.42	PMZ	$m_b=6.9$	1.5		2.46																																						
		pP	22 59	10.0	4.3		pP	23 00	08.0			5.3	PP	23 01	48.0		2.5																																						
		PP	23 00	35.5	0.3		PP	23 01	48.0			2.5	iS	23 07	08.0		0.9																																						
		S	23 05	22.0	-1.4		iS	23 07	08.0			0.9	SMN		12.0		19.1																																						
		LN	$M_s=6.4$	15.0	17.2		SS	23 10	48.0			2.4	SS	23 10	48.0		2.4																																						
		LE		16.0	14.0		LZ	$M_s=6.3$	46.0			61.3	-iP	22 59	48.8		0.6																																						
		LZ	$M_s=6.2$	37.0	54.5		-iP	22 59	48.8			0.6	PMZ	$m_b=6.4$	1.0		0.50																																						
QZN	46.7 303	-P	22 58	52.0	-0.3	sP	23 00	23.0	5.5	CN2	54.0 338	PP	23 01	52.0	0.3	SMN	8.0	4.00																																					
		PMZ	$m_b=6.4$	11.0	5.60	PP	23 01	52.0	0.3			SME	8.0	2.00																																									
		pP	22 59	16.0	4.3	S	23 07	14.0	-1.5			LZ	$M_s=6.0$	40.0	25.0																																								
		PP	23 00	42.5	-0.3	SMN						-P	22 59	57.0	0.4																																								
		LN	$M_s=6.4$	24.0	21.0	SME						PMZ	$m_b=6.6$	1.5	1.05																																								
		LE		27.0	34.6	PMZ	$m_B=6.8$	6.0	7.30			PMZ	$m_B=6.8$	6.0	7.30																																								
		-iP	22 59	03.5	1.7	epP	23 00	19.0	2.6			eScP	23 04	47.0	1.4																																								
		PMZ	$m_b=6.4$	1.6	0.71	eScP	23 04	47.0	1.4			eS	23 07	30.0	-2.0																																								
		PMZ	$m_B=7.0$	6.5	12.6	eS	23 07	30.0	-2.0			esS	23 08	12.0	5.5																																								
		pP	22 59	23.0	1.8	esS	23 08	12.0	5.5			LN	$M_s=5.9$	16.0	6.03																																								
PcP	23 00	28.0	-1.0	LN	$M_s=6.3$	36.0	49.0	LZ	$M_s=6.3$	36.0	49.0																																												
NJ2	47.9 323	PP	23 00	54.0	0.2	-P	22 59	58.0	0.1	KMI	55.3 306	PMZ	$m_b=6.5$	2.5	1.60	XAN	55.4 318	PMZ	$m_B=6.5$	7.0	4.10																																		
		PP	23 00	54.0	0.2	PMZ	$m_B=6.5$	7.0	4.10			pP	23 00	23.0	5.5			DL2	51.6 332	P	22 59	31.9	1.8	PP	23 01	58.0	-5.1																												
		iS	23 05	54.0	1.9	pP	23 00	23.0	5.5			iS	23 07	37.0	2.5					TIA	51.9 326	PMZ	$m_b=6.2$	1.4	0.40	LN	$M_s=5.9$	14.0	3.30																										
		ScS	23 08	46.0	2.5	sP	22 59	47.0	2.2			LE		16.0	4.50							GZA	52.8 309	PMZ	$m_B=6.4$	6.0	2.92	LZ	$M_s=6.4$	40.0	59.8																								
		LN	$M_s=6.0$	18.0	7.65	iS	23 06	22.0	4.7			LZ	$M_s=6.4$	40.0	59.8									SNY	53.1 335	-iP	22 59	32.6	0.3	CD2	57.3 312	P	22 59	58.0	-0.7																				
		LE		15.0	7.35	LN	$M_s=6.3$	21.0	15.6			PMZ	$m_b=6.5$	9.0	5.70											HHC	58.2 326	PMZ	$m_B=6.5$			1.6	0.50	TIY	55.6 324	pP	23 00	19.0	0.5																
		LZ	$M_s=5.7$	21.0	8.25	LE		16.0	12.2			PP	23 02	04.0	-0.3													GYN	52.8 309			PMZ	$m_B=6.6$			6.0	4.60	S	23 07	32.0	-2.7														
		-iP	22 59	17.5	1.8	LZ	$M_s=6.0$	20.0	16.3			SS	23 11	25.0	4.7																	SNY	53.1 335			LN	$M_s=6.0$	13.0	4.40	CD2	57.3 312	LN	$M_s=6.0$	13.0	4.40										
		PMZ	$m_b=6.8$	1.5	1.66	LN	$M_s=6.3$	21.0	15.6			LE		16.0	3.90																					SNY	53.1 335	LZ	$M_s=6.3$			20.0	16.3	CD2	57.3 312	LE		16.0	3.90						
		PMZ	$m_B=6.4$	6.0	2.92	LE		16.0	12.2			LZ	$M_s=6.3$	38.0	45.2																							SNY	53.1 335			-iP	22 59			42.0	0.6	CD2	57.3 312	-iP	23 00	11.7	-0.3		
pP	22 59	39.0	3.8	LZ	$M_s=6.0$	20.0	16.3	PMZ	$m_b=6.4$	1.4	0.74	SNY	53.1 335	PMZ	$m_B=6.6$	6.0	4.60																									CD2	57.3 312			PMZ	$m_B=6.6$			8.0	6.52				
sP	22 59	47.0	2.2	S	23 06	36.0	-6.5	pP	23 00	20.5	0.9			SNY	53.1 335	pP	23 00	04.0	4.7																											CD2	57.3 312			pP	23 00	20.5	0.9		
iS	23 06	22.0	4.7	SMN		10.0	4.00	sP	23 00	33.0	3.9					SNY	53.1 335	PP	23 01	41.0	-0.2																													CD2	57.3 312	sP	23 00	33.0	3.9
LN	$M_s=6.3$	21.0	15.6	SME		8.0	3.78	PcP	23 00	53.0	-4.6							SNY	53.1 335	S	23 07	04.0	4.3																													CD2	57.3 312	PcP	23 00
LE		16.0	12.2	LN	$M_s=6.3$	14.0	14.6	S	23 07	39.0	2.3									SNY	53.1 335	S	23 07	39.0	2.3					CD2	57.3 312																							S	23 07
LZ	$M_s=5.7$	21.0	8.25	LZ	$M_s=6.0$	40.0	30.9	sS	23 08	14.5	2.2											SNY	53.1 335	sS	23 08	14.5	2.2							CD2	57.3 312																			sS	23 08
-iP	22 59	17.5	1.8	LZ	$M_s=6.0$	40.0	30.9	LN	$M_s=6.3$	20.0	16.3													SNY	53.1 335	LN	$M_s=6.3$	20.0	16.3																									CD2	57.3 312
PMZ	$m_b=6.8$	1.5	1.66	LZ	$M_s=6.0$	40.0	30.9	LZ	$M_s=6.3$	38.0	45.2															SNY	53.1 335	LZ	$M_s=6.3$			38.0	45.2							CD2	57.3 312														
PMZ	$m_B=6.4$	6.0	2.92	LZ	$M_s=6.0$	40.0	30.9	-iP	23 00	11.7	-0.3																	SNY	53.1 335			-iP	23 00			11.7	-0.3							CD2	57.3 312										
pP	22 59	39.0	3.8	LZ	$M_s=6.0$	40.0	30.9	PMZ	$m_b=6.5$	0.8	0.45																					SNY	53.1 335			PMZ	$m_b=6.5$	0.8	0.45									CD2	57.3 312						
sP	22 59	47.0	2.2	LZ	$M_s=6.0$	40.0	30.9	PMZ	$m_B=6.7$	6.0	5.20	SNY	53.1 335																							PMZ	$m_B=6.7$	6.0	5.20			CD2	57.3 312												
iS	23 06	22.0	4.7	LZ	$M_s=6.0$	40.0	30.9	pP	23 00	36.5	4.6			SNY	53.1 335																					pP	23 00	36.5	4.6							CD2	57.3 312								
LN	$M_s=6.3$	21.0	15.6	LZ	$M_s=6.0$	40.0	30.9	S	23 08	02.0	2.6					SNY	53.1 335																			S	23 08	02.0	2.6											CD2	57.3 312				
LE		16.0	12.2	LZ	$M_s=6.0$	40.0	30.9	LN	$M_s=6.3$	15.0	11.3							SNY	53.1 335																	LN	$M_s=6.3$	15.0	11.3													CD2	57.3 312		
LZ	$M_s=5.7$	21.0	8.25	LZ	$M_s=6.0$	40.0	30.9	LZ	$M_s=6.2$	36.0	32.3									SNY	53.1 335									LZ	$M_s=6.2$					36.0	32.3	CD2	57.3 312																
-iP	22 59	17.5	1.8	LZ	$M_s=6.0$	40.0	30.9	P	23 00	18.4	0.0											SNY	53.1 335							P	23 00			18.4	0.0	CD2	57.3 312																		
PMZ	$m_b=6.8$	1.5	1.66	LZ	$M_s=6.0$	40.0	30.9	PMZ	$m_b=6.6$	1.2	1.00													SNY	53.1 335					PMZ	$m_b=6.6$			1.2	1.00																			CD2	57.3 312
PMZ	$m_B=6.4$	6.0	2.92	LZ	$M_s=6.0$	40.0	30.9																			SNY	53.1 335													CD2	57.3 312														
pP	22 59	39.0	3.8	LZ	$M_s=6.0$	40.0	30.9																					SNY	53.1 335															CD2	57.3 312										
sP	22 59	47.0	2.2	LZ	$M_s=6.0$	40.0	30.9																							SNY	53.1 335																	CD2	57.3 312						
iS	23 06	22.0	4.7	LZ	$M_s=6.0$	40.0	30.9					SNY	53.1 335																													CD2	57.3 312												
LN	$M_s=6.3$	21.0	15.6	LZ	$M_s=6.0$	40.0	30.9							SNY	53.1 335																															CD2	57.3 312								
LE		16.0	12.2	LZ	$M_s=6.0$	40.0	30.9									SNY	53.1 335																																	CD2	57.3 312				
LZ	$M_s=5.7$	21.0	8.25	LZ	$M_s=6.0$	40.0	30.9											SNY	53.1 335																																	CD2	57.3 312		
-iP	22 59	17.5	1.8	LZ	$M_s=6.0$	40.0	30.9													SNY	53.1 335																	CD2	57.3 312																
PMZ	$m_b=6.8$	1.5	1.66	LZ	$M_s=6.0$	40.0	30.9															SNY	53.1 335													CD2	57.3 312																		
PMZ	$m_B=6.4$	6.0	2.92	LZ	$M_s=6.0$	40.0	30.9																	SNY	53.1 335																													CD2	57.3 312
pP	22 59	39.0	3.8	LZ	$M_s=6.0$	40.0	30.9																			SNY	53.1 335													CD2	57.3 312														
sP	22 59	47.0	2.2	LZ	$M_s=6.0$	40.0	30.9																					SNY	53.1 335															CD2	57.3 312										
iS	23 06	22.0	4.7	LZ	$M_s=6.0$	40.0	30.9																							SNY</																									



		PMZ	$m_b = 6.7$	6.0	5.25			LZ	$M_s = 4.2$	28.0	2.76
		pP	23 00 42.0	3.8		CN2	13.6 307	eP	07 48 54.2	0.0	
		S	23 08 14.0	2.8				PMZ	$m_b = 5.9$	1.0	0.20
		SMN		12.0	2.85			pP	07 49 02.0	-2.2	
		SME		10.0	4.08			sP	07 49 08.0	-4.6	
		LN	$M_s = 6.2$	17.0	11.2			eS	07 51 25.0	1.3	
		LE		17.0	3.68			LN	$M_s = 4.3$	10.0	0.50
		LZ	$M_s = 6.3$	40.0	44.5			LE		10.0	0.70
BTO	58.9 325	-iP	23 00 24.0	0.7				LZ	$M_s = 4.2$	30.0	2.30
		PMZ	$m_b = 6.6$	7.0	6.00	SNY	14.2 297	-iP	07 49 03.8	2.6	
		pP	23 00 47.0	3.8				PMZ	$m_b = 5.8$	1.6	0.23
		PP	23 02 35.0	-0.3				sP	07 49 20.0	0.3	
		S	23 08 23.0	2.7				eS	07 51 43.0	6.5	
		SS	23 12 22.0	5.1				LN	$M_s = 4.4$	11.5	0.76
		LN	$M_s = 6.4$	19.0	10.6			LE		13.5	1.13
		LE		19.0	13.3			LZ	$M_s = 4.3$	30.0	2.58
		LZ	$M_s = 6.0$	19.0	12.2	DL2	15.1 285	P	07 49 17.0	3.2	
LZH	60.0 317	-P	23 00 31.1	0.2				PMZ	$m_b = 4.8$	1.0	0.040
		PMZ	$m_b = 6.5$	2.0	1.37			pP	07 49 26.0	1.7	
		PMZ	$m_b = 6.7$	7.0	6.77			sP	07 49 34.0	1.7	
		pP	23 00 54.0	3.1				SME		8.0	0.55
		PcP	23 01 16.0	1.0				LE	$M_s = 4.4$	16.0	1.52
		PP	23 02 43.0	-2.2				LZ	$M_s = 4.2$	18.0	1.24
		S	23 08 34.0	-0.6				eP	07 49 37.0	0.7	
		SME		10.0	6.19	SSE	16.9 257	PMZ	$m_b = 4.4$	1.0	0.019
		SME		15.0	9.29			sP	07 49 55.0	-0.3	
		SS	23 12 32.0	-1.5				eS	07 52 43.0	2.6	
		LN	$M_s = 6.0$	16.0	3.71			sS	07 52 59.0	0.5	
		LE		15.0	4.11			LE	$M_s = 4.1$	12.0	0.49
GTA	64.5 319	-iP	23 01 01.0	0.2				LZ	$M_s = 4.3$	20.0	1.38
		PMZ	$m_b = 6.6$	0.8	0.60	NJ2	18.4 262	-P	07 49 54.5	-0.2	
		PMZ	$m_b = 6.6$	7.0	5.27			PMZ	$m_b = 5.3$	0.9	0.13
		pP	23 01 22.0	1.1				sP	07 50 14.0	0.0	
		sP	23 01 25.5	-4.8				LZ	$M_s = 4.2$	18.0	0.89
		S	23 09 31.0	0.1				-P	07 49 58.5	-1.1	
		sS	23 10 05.0	-2.2				PMZ	$m_b = 5.2$	1.2	0.15
		LN	$M_s = 5.7$	14.0	2.41			pP	07 50 13.0	1.9	
		LZ	$M_s = 6.1$	42.0	24.2			LN	$M_s = 4.3$	12.0	0.50
LSA	66.6 306	-P	23 01 13.6	-0.7				LE		28.0	1.10
		pP	23 01 39.0	4.7		BJI	19.4 288	eP	07 50 05.5	-0.5	
		S	23 09 58.0	1.9				PMZ	$m_b = 4.9$	1.0	0.067
		LE	$M_s = 5.8$	12.0	2.26			eS	07 53 37.0	1.0	
WMQ	74.6 318	-iP	23 02 02.0	-0.3				LE	$M_s = 4.1$	12.0	0.37
		PMZ		14.0	5.20			LZ	$M_s = 4.0$	36.0	1.25
		pP	23 02 25.0	2.1		QZH	22.0 245	-P	07 50 30.7	-2.1	
		PP	23 04 52.0	0.7				PMZ	$m_b = 4.9$	0.7	0.040
		iS	23 11 32.0	1.5		TIY	22.4 282	eP	07 50 35.0	-1.6	
		SME		18.0	10.5			PP	07 51 02.5	-2.1	
		SKS	23 11 57.5	0.4				S	07 54 26.0	-6.4	
		SS	23 16 18.5	-0.9				LE	$M_s = 4.6$	18.0	1.43
		LE	$M_s = 6.0$	14.0	3.25			LZ	$M_s = 4.6$	19.0	1.97
KSH	81.5 311	+iP	23 02 41.5	0.8		WHN	22.6 262	eP	07 50 38.5	0.4	
		PMZ	$m_b = 6.5$	6.0	4.30			PMZ	$m_b = 5.0$	1.0	0.080
		pP	23 03 04.0	2.6				pP	07 50 54.0	1.9	
		PP	23 05 51.0	1.8				eS	07 54 40.0	3.9	
		S	23 12 48.0	4.8				LE	$M_s = 4.5$	12.0	0.75
		LE	$M_s = 6.4$	9.0	5.20			LZ	$M_s = 4.4$	20.0	1.25
						HHC	23.0 290	eP	07 50 40.2	-2.0	
								PP	07 51 08.0	-4.7	
								S	07 54 37.0	-5.5	
								LN	$M_s = 4.4$	10.0	0.34
								LE		12.0	0.40
						BTO	24.1 289	eP	07 50 51.0	-2.6	
								eS	07 55 02.0	-1.9	
								LN	$M_s = 4.5$	13.0	0.30
								LE		13.0	0.70
								LZ	$M_s = 4.2$	13.0	0.50
						XAN	25.9 274	-P	07 51 09.2	-0.6	

MAY 3d 07h 45m  $42.0 \pm 0.03s$ , SD1.02 / 322  
 36.48 N  $\pm 0.87km$ , 140.51 E  $\pm 0.55km$ , h63  $\pm 0.25km$   
 Near east coast of Honshu (228)  
 $M_s 4.4 / 23$ ,  $m_b 5.0 / 2$ ,  $m_b 5.4 / 101$

MDJ	11.6 318	eP	07 48 28.6	1.3	
		PMZ	$m_b = 5.9$	1.0	0.20
		pP	07 48 33.0	-2.9	
		PP	07 48 40.0	2.8	
		SS	07 50 45.0	-5.1	
		LE	$M_s = 4.0$	12.0	0.60









<p>MAY 3d 22h 39m 48.6 ± 0.07s, SD2.06 / 34                  24.65 N ± 0.86km, 122.51 E ± 0.89km, h18 ± 0.31km                  Taiwan region (243)                  M<sub>S</sub>3.9 / 12, M<sub>L</sub>3.9 / 9, m<sub>b</sub>4.1 / 4</p>					<p>eS 03 10 34.0 -5.4                  LN M<sub>S</sub>=4.7 15.0 1.05                  LZ M<sub>S</sub>=4.4 12.0 0.55</p>						
QZH	3.6	276	Pn	22 40 46.0	2.4	CD2	34.8	329	P	03 06 14.0	-0.4
			Su	22 41 28.5	1.2				S	03 11 44.0	2.4
			SMN	M <sub>L</sub> =3.8	0.8	XAN	35.2	339	LZ	M <sub>S</sub> =4.2	20.0
			SME		0.8				P	03 06 18.0	0.2
			LE	M <sub>S</sub> =3.6	8.0	DL2	37.3	357	S	03 11 50.0	2.2
SSE	6.5	350	eP	22 41 25.0	-1.5				LN	M <sub>S</sub> =4.9	14.0
			sP	22 41 34.5	-1.1				eP	03 06 36.0	0.4
			eS	22 42 40.2	-1.0				S	03 12 14.0	-6.2
			SMN	M <sub>L</sub> =3.7	1.0	TIY	37.5	345	LZ	M <sub>S</sub> =4.4	12.0
			SME		1.0				-P	03 06 37.6	0.2
			LN	M <sub>S</sub> =3.4	12.0				S	03 12 29.0	5.7
			LZ	M <sub>S</sub> =3.6	10.0				LN	M <sub>S</sub> =4.8	12.0
NJ2	8.1	337	+P	22 41 46.8	-0.9	BJI	39.0	351	LZ	M <sub>S</sub> =4.6	16.0
			SMN	M <sub>L</sub> =4.4	0.9				eP	03 06 49.0	-0.6
			SME		1.0				PMZ	m <sub>b</sub> =4.6	1.5
			LN	M <sub>S</sub> =3.9	10.0				eS	03 12 47.0	0.3
			LE		10.0				eSS	03 15 32.0	1.8
WHN	9.3	311	eP	22 42 04.7	-0.7				LN	M <sub>S</sub> =4.9	15.0
			LE	M <sub>S</sub> =4.0	8.0	LZH	39.0	334	LZ	M <sub>S</sub> =4.3	16.0
GYA	14.4	281	P	22 43 10.2	-4.1				P	03 06 50.7	0.7
TIY	15.6	329	eP	22 43 29.0	-0.7				PP	03 08 23.5	0.1
			S	22 46 25.0	3.0				PMZ	m <sub>b</sub> =5.0	2.0
			LN	M <sub>S</sub> =4.1	16.0				eS	03 12 48.0	0.5
			LZ	M <sub>S</sub> =4.1	14.0				SME		15.0
BTO	19.0	330	eP	22 44 16.5	3.7				eSS	03 15 32.0	1.2
			LN	M <sub>S</sub> =4.3	13.0				LN	M <sub>S</sub> =4.9	15.0
			LE		13.0				LE		13.0
CN2	19.3	6	eP	22 44 15.0	-0.2	SNY	40.2	360	LZ	M <sub>S</sub> =4.9	14.0
LZH	19.7	310	eP	22 44 18.0	-2.3				eP	03 06 57.2	-2.3
			PMZ	m <sub>b</sub> =4.4	2.0				S	03 13 00.0	-3.7
			sP	22 44 31.0	1.2				sS	03 13 17.0	-2.1
			LE	M <sub>S</sub> =3.9	10.0	HHC	40.7	346	LZ	M <sub>S</sub> =4.5	22.0
			LZ	M <sub>S</sub> =3.8	12.0				eP	03 07 04.3	0.4
					0.26	BTO	40.9	344	LN	M <sub>S</sub> =4.8	13.0
									eS	03 13 13.0	-1.9
									LN	M <sub>S</sub> =4.9	15.0
									LE		12.0
						GTA	43.6	333	+P	03 07 28.0	0.6
									LE	M <sub>S</sub> =4.7	13.0
									LZ	M <sub>S</sub> =4.8	15.0
						WMQ	52.9	328	P	03 08 39.7	0.0
									PcP	03 09 47.0	-0.8
									S	03 16 08.0	3.9
									LZ	M <sub>S</sub> =4.6	16.0
											0.49
<p>MAY 3d 22h 40m 13.9 ± 0.05s, SD2.89 / 10                  31.61 N ± 0.48km, 102.32 E ± 0.28km, h21 ± 0.70km                  Sichuan Province (307)                  M<sub>S</sub>4.0 / 1, M<sub>L</sub>3.3 / 3,</p>					<p>MAY 4d 10h 12m 06.6 ± 0.09s, SD1.16 / 156                  11.77 N ± 1.21km, 40.92 E ± 0.70km, h10 ± 0.17km                  Ethiopia (558)                  M<sub>S</sub>5.0 / 4, m<sub>b</sub>4.9 / 50,</p>						
CD2	1.4	119	Pg	22 40 36.7	-2.5	WMQ	51.3	43	P	10 21 12.5	-1.1
			Sg	22 40 55.0	-3.5				S	10 28 25.0	-5.3
			SMN	M <sub>L</sub> =3.2	0.6				LZ	M <sub>S</sub> =4.9	26.0
			SME		0.8	LZH	61.3	55	eP	10 22 25.3	-0.2
GYA	6.4	142	Pg	22 42 10.2	3.3				PMZ	m <sub>b</sub> =5.3	2.5
									LN	M <sub>S</sub> =4.9	15.0
									LZ	M <sub>S</sub> =4.8	18.0
											0.68
											1.4
											-1.8
											2.1
											0.5
											2.5
											-2.1
											13.0
											0.66
											15.0
											0.91
<p>MAY 4d 02h 59m 23.8 ± 0.04s, SD1.22 / 79                  1.45 N ± 0.63km, 123.60 E ± 0.91km, h30 ± 0.04km                  Minahassa Peninsula (Celebes) (265)                  M<sub>S</sub>4.8 / 17, m<sub>b</sub>4.8 / 18,</p>					<p>MAY 4d 10h 12m 06.6 ± 0.09s, SD1.16 / 156                  11.77 N ± 1.21km, 40.92 E ± 0.70km, h10 ± 0.17km                  Ethiopia (558)                  M<sub>S</sub>5.0 / 4, m<sub>b</sub>4.9 / 50,</p>						
QZN	22.1	323	eP	03 04 21.7	3.6						
			eS	03 08 19.0	4.1						
			sS	03 08 25.0	-3.3						
			SS	03 08 57.0	3.4						
			LN	M <sub>S</sub> =4.8	13.0						
GZH	23.7	336	eP	03 04 36.0	1.9						
			S	03 08 46.0	2.6						
			LN	M <sub>S</sub> =4.9	13.0						
			LE		13.0						
			LZ	M <sub>S</sub> =4.7	15.0						
WHN	30.2	344	eP	03 05 35.5	1.1						
			S	03 10 30.0	-0.3						
			LN	M <sub>S</sub> =5.1	16.0						
			LE		14.0						
NJ2	30.8	352	eP	03 05 37.5	-1.6						



			LZ	$M_s=4.9$	20.0	0.75		
WHN	69.9	62	eP	10 23 20.2	-0.4			
BJI	71.3	52	eP	10 23 29.0	0.2			
			PMZ	$m_b=4.9$	1.5	0.021		
SSE	75.7	61	eP	10 23 55.0	0.0			
			LZ	$M_s=4.8$	16.0	0.44		
SNY	76.8	50	eP	10 24 03.4	2.4			
CN2	78.0	47	eP	10 24 08.5	0.7			

			PMZ	$m_b=5.1$	1.0	0.050		
XAN	86.8	307	P	01 38 10.9	0.6			
CD2	89.6	303	P	01 38 24.2	0.8			
LZH	91.4	308	P	01 38 32.2	0.2			
			PMZ	$m_b=5.4$	1.4	0.067		
GTA	95.6	310	eP	01 38 50.6	-0.3			
WMQ	105.5	311	Pdif	01 39 32.2	-2.9			

MAY 4d 18h 24m  $12.0 \pm 0.05s$ , SD1.76 / 31  
 23.83 N  $\pm 1.28km$ , 123.96 E  $\pm 0.82km$ , h15  $\pm 0.50km$   
 South-western Ryukyu Islands (246)  
 $M_s 4.0 / 1$ ,  $M_L 3.4 / 3$ ,  $m_b 4.6 / 5$

QZH	5.0	284	-Pn	18 25 26.3	-0.8			
			SMN	$M_L=3.0$	0.7	0.020		
			SME		0.7	0.020		
NJ2	9.3	332	+P	18 26 28.4	-1.0			
GYA	15.9	283	P	18 28 02.0	5.0			
TIY	17.0	327	eP	18 28 13.5	2.4			
			LZ	$M_s=3.3$	16.0	0.12		
CD2	19.3	296	P	18 28 37.0	-2.0			
LZH	21.2	310	eP	18 29 00.0	-0.2			
			LE	$M_s=4.0$	13.0	0.31		
			LZ	$M_s=4.0$	16.0	0.46		
GTA	25.7	313	eP	18 29 42.0	-1.4			

MAY 5d 07h 21m  $27.0 \pm 0.06s$ , SD2.42 / 145  
 40.64 N  $\pm 1.34km$ , 16.10 E  $\pm 0.78km$ , h19  $\pm 0.37km$   
 Southern Italy (390)  
 $M_s 5.8 / 28$ ,  $m_b 5.1 / 21$ ,

KSH	45.0	71	eP	07 29 44.0	0.3			
			S	07 36 19.0	-0.9			
			LE	$M_g=5.8$	11.0	4.80		
			LZ	$M_g=5.7$	12.0	5.60		
LSA	60.6	75	eP	07 31 37.0	-3.1			
			S	07 39 50.5	-1.8			
			ScS	07 41 26.5	1.7			
			SMN		7.0	0.67		
LZH	66.1	62	-P	07 32 18.0	1.9			
			sP	07 32 21.0	-5.1			
			ePP	07 34 37.0	-5.9			
			sS	07 41 11.0	-3.2			
			SMN		6.0	0.67		
			LN	$M_s=5.8$	16.0	1.96		
			LE		14.0	1.74		
			LZ	$M_s=5.4$	21.0	2.80		
TIY	70.8	57	P	07 32 40.8	-4.4			
			pP	07 32 48.0	-4.1			
			sP	07 32 54.5	-0.8			
			S	07 41 56.5	-0.3			
			sS	07 42 04.0	-6.0			
			LN	$M_s=6.1$	14.0	3.38		
			LE		14.0	2.82		
			LZ	$M_s=5.8$	14.0	3.57		
KMI	71.7	72	eP	07 32 47.0	-3.4			
			PMZ	$m_b=5.6$	1.5	0.10		
			sP	07 32 59.5	-0.9			
			S	07 42 12.5	5.9			
			LN	$M_s=5.5$	17.0	0.80		
			LE		15.0	0.90		
			LZ	$M_s=5.1$	20.0	1.20		
BJI	71.7	53	eP	07 32 54.0	3.5			
			ePP	07 35 28.0	-2.6			
			eS	07 42 07.0	-1.8			
			LN	$M_s=6.1$	14.0	3.87		
			LE		14.0	3.38		
			LZ	$M_s=5.8$	15.0	3.79		

MAY 4d 22h 21m  $53.5 \pm 0.09s$ , SD2.01 / 41  
 22.26 N  $\pm 0.95km$ , 122.49 E  $\pm 1.14km$ , h21  $\pm 0.24km$   
 Taiwan region (243)  
 $M_s 3.6 / 3$ ,  $M_L 3.7 / 9$ ,  $m_b 4.4 / 5$

QZH	4.5	307	ePn	22 23 00.0	-0.5			
			Sn	22 23 48.2	-5.6			
			SMN	$M_L=3.7$	0.8	0.14		
			SME		0.8	0.13		
SSE	8.9	353	eP	22 24 03.5	-0.3			
			SME	$M_L=3.7$	1.2	0.013		
			LE	$M_s=3.5$	14.0	0.32		
WHN	11.0	320	eP	22 24 35.2	2.0			
			LE	$M_s=3.9$	10.0	0.42		
XAN	16.7	317	eP	22 25 51.0	2.3			
BJI	18.5	345	eP	22 26 11.0	0.2			
			PMZ	$m_b=4.4$	1.5	0.026		
CD2	18.8	301	eP	22 26 17.0	2.4			
HHC	20.7	336	eP	22 26 36.0	0.5			
LZH	21.3	314	eP	22 26 44.5	3.1			
CN2	21.6	6	eP	22 26 46.5	1.9			
MDJ	23.0	13	eP	22 27 01.5	2.7			

			LN	$M_s=6.1$	14.0	3.38		
			LE		14.0	2.82		
			LZ	$M_s=5.4$	21.0	2.80		
TIY	70.8	57	P	07 32 40.8	-4.4			
			pP	07 32 48.0	-4.1			
			sP	07 32 54.5	-0.8			
			S	07 41 56.5	-0.3			
			sS	07 42 04.0	-6.0			
			LN	$M_s=6.1$	14.0	3.38		
			LE		14.0	2.82		
			LZ	$M_s=5.8$	14.0	3.57		
KMI	71.7	72	eP	07 32 47.0	-3.4			
			PMZ	$m_b=5.6$	1.5	0.10		
			sP	07 32 59.5	-0.9			
			S	07 42 12.5	5.9			
			LN	$M_s=5.5$	17.0	0.80		
			LE		15.0	0.90		
			LZ	$M_s=5.1$	20.0	1.20		
BJI	71.7	53	eP	07 32 54.0	3.5			
			ePP	07 35 28.0	-2.6			
			eS	07 42 07.0	-1.8			
			LN	$M_s=6.1$	14.0	3.87		
			LE		14.0	3.38		
			LZ	$M_s=5.8$	15.0	3.79		
GYA	73.7	69	P	07 32 59.2	-3.1			
			sP	07 33 11.8	-0.5			
			S	07 42 36.0	6.4			
			LN	$M_s=5.8$	20.0	1.50		
			LE		20.0	3.10		
			LZ	$M_s=5.1$	22.0	1.10		
CN2	74.6	45	eP	07 33 09.0	1.3			
			eS	07 42 40.0	-1.8			
			LN	$M_s=6.1$	15.0	3.00		
			LE		15.0	3.00		
			LZ	$M_s=5.8$	15.0	4.00		
SNY	74.9	48	+P	07 33 06.0	-3.3			
			PMZ	$m_b=5.0$	1.2	0.020		
			sP	07 33 16.0	-3.4			
			eS	07 42 41.0	-3.9			
			LN	$M_s=6.1$	13.0	2.06		
			LE		13.0	3.95		
			LZ	$M_s=5.8$	14.0	3.35		
DL2	75.7	51	eP	07 33 12.0	-1.8			

MAY 5d 01h 26m  $19.9 \pm 0.04s$ , SD0.96 / 165  
 18.28 S  $\pm 0.68km$ , 177.99 W  $\pm 0.80km$ , h522  $\pm 0.28km$   
 Fiji region (181)  
 $m_b 4.9 / 1$ ,  $m_b 5.0 / 30$ ,

QZH	75.2	303	eP	01 37 11.0	0.3			
SSE	76.3	310	P	01 37 16.0	-0.6			
			PMZ	$m_b=4.5$	0.8	0.018		
NJ2	78.5	309	+P	01 37 29.0	0.5			
			PMZ	$m_b=5.0$	0.9	0.056		
MDJ	78.7	325	-P	01 37 29.3	-0.5			
			PMZ	$m_b=5.1$	1.0	0.080		
SNY	80.5	320	-P	01 37 38.6	-0.6			
CN2	80.6	322	eP	01 37 38.5	-0.9			
			PMZ	$m_b=5.2$	1.0	0.10		
WHN	81.1	306	eP	01 37 42.0	-0.4			
TIA	81.8	312	eP	01 37 45.3	-0.4			
BJI	84.3	315	eP	01 37 58.0	-0.3			
			PMZ	$m_b=5.0$	1.0	0.050		
GYA	85.6	300	P	01 38 05.4	0.9			
TIY	85.8	312	-iP	01 38 06.0	0.4			

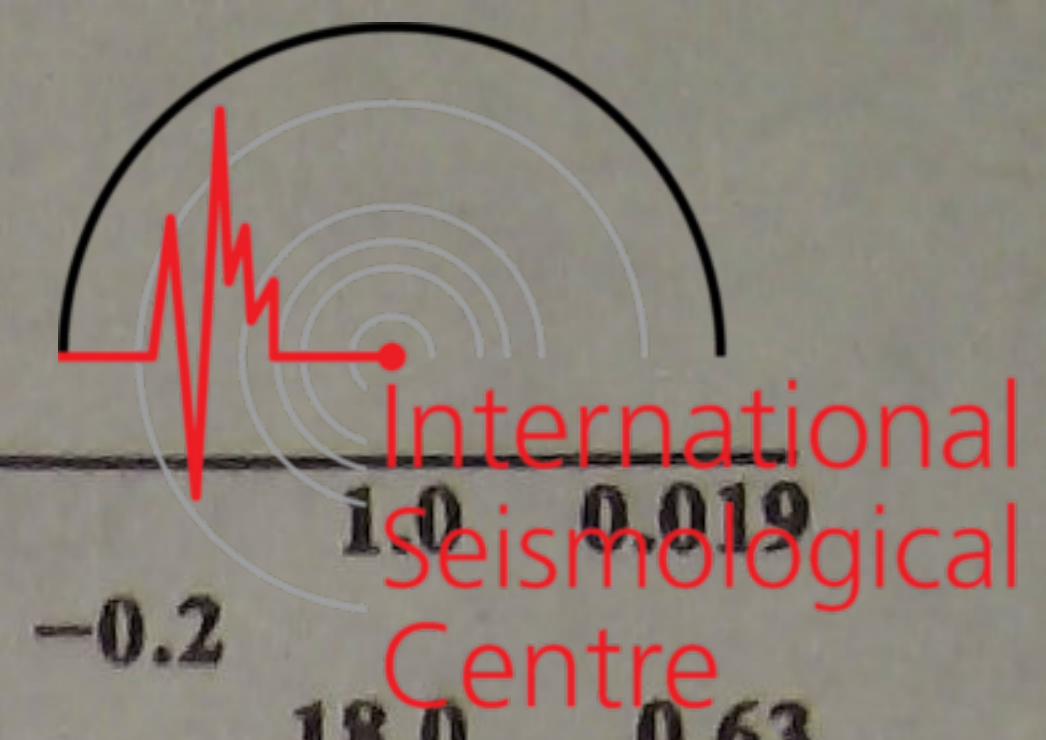


	eS	07 42	58.0	4.4					WHN	20.9	82	eP	10 34	49.5	-0.8		
	LN		$M_S=6.1$	14.0	2.73							eS	10 38	40.0	3.1		
	LE			14.0	3.24							LN		$M_S=4.6$	10.0	0.73	
	LZ		$M_S=5.4$	18.0	1.81							LE			12.0	0.50	
MDJ	76.3	42	eP	07 33	14.2	-2.8			QZN	21.0	117	eP	10 34	51.9	1.2		
			LN		$M_S=6.0$	18.0	2.82		BJI	23.5	58	eP	10 35	17.0	1.2		
			LE			18.0	3.14					PMZ		$m_b=4.0$	1.0	0.0060	
			LZ		$M_S=5.6$	18.0	2.99					esS	10 39	36.0	-2.7		
WHN	76.5	61	eP	07 33	14.5	-3.6						LN		$M_S=4.7$	11.0	0.87	
			sP	07 33	24.0	-4.3						LE			11.0	0.47	
			eS	07 43	06.0	4.0			CN2	31.2	54	eP	10 36	24.6	-1.8		
			LE		$M_S=5.7$	12.0	1.49		MAY 6d 16h 46m $12.6 \pm 0.06s$ , SD1.84 / 97 $35.22 S \pm 2.20km$ , $104.23 W \pm 1.50km$ , $h11 \pm 0.32km$ Southern Pacific Ocean (692) $m_b 4.9 / 6$ ,								
NJ2	78.5	58	-P	07 33	26.0	-3.2			MDJ	138.3	300	PKP	17 05	39.0	-0.3		
			PP	07 36	34.0	6.3			CN2	141.2	298	ePKP	17 05	45.0	0.5		
			LN		$M_S=5.7$	15.0	1.21		SSE	142.0	277	PKP	17 05	48.0	2.2		
			LE			15.0	1.22					LZ		$M_S=5.3$	20.0	0.46	
			LZ		$M_S=5.2$	16.0	0.94		NJ2	144.2	277	ePKP	17 05	45.0	-4.6		
SSE	80.6	57	-P	07 33	45.0	4.3			GZH	145.2	260	ePKP	17 05	52.0	0.6		
			PP	07 36	42.0	-3.3			QZN	145.9	251	PKP	17 05	53.6	1.1		
			S	07 43	44.0	-0.3			TIA	146.6	284	PKP	17 05	52.4	-1.4		
			sS	07 43	55.0	-2.7			WHN	147.4	273	ePKP	17 05	53.0	-2.1		
			SS	07 49	00.0	0.1			BJI	147.8	291	ePKP	17 05	56.0	0.2		
			LZ		$M_S=5.1$	20.0	0.92		TIY	150.5	286	PKP	17 06	04.0	3.9		
QZN	80.6	73	eP	07 33	38.2	-2.6						LZ		$M_S=5.5$	18.0	0.61	
MAY 5d 13h 10m $27.1 \pm 0.06s$ , SD1.71 / 13 $46.89 N \pm 0.42km$ , $129.71 E \pm 0.47km$ , $h13 \pm 0.22km$ North-Eastern China (658) $M_L 4.2 / 10$ ,									HHC	151.4	292	ePKP	17 06	05.0	3.5		
MDJ	2.3	182	Pn	13 11	05.3	0.5			BTO	152.6	292	ePKP	17 06	05.2	2.0		
			Pg	13 11	08.5	1.2			XAN	152.8	277	ePKP	17 06	06.0	2.6		
			Sg	13 11	38.0	-0.5			KMI	154.7	254	ePKP	17 06	09.0	2.8		
			SMN		$M_L=3.8$	0.6	0.66		CD2	156.2	268	ePKP	17 06	08.8	0.8		
			LE			1.5	5.75		LZH	157.2	280	ePKP	17 06	11.0	1.5		
CN2	4.3	226	-Pn	13 11	32.9	0.1						PKP2	17 06	42.0	0.8		
			Pg	13 11	46.2	3.0			GTA	160.4	289	ePKP	17 06	11.5	-1.8	25.0	0.80
			Sn	13 12	22.0	-2.9						LZ		$M_S=5.5$	24.0	0.64	
			Sg	13 12	45.0	2.9			WMQ	167.4	317	ePKP	17 06	17.7	-2.0	36.0	0.91
			SMN		$M_L=4.2$	0.8	0.45					LZ		$M_S=5.4$			
			SME			0.8	0.46		MAY 6d 10h 30m $07.8 \pm 0.06s$ , SD2.15 / 42 $29.99 N \pm 0.94km$ , $90.12 E \pm 0.66km$ , $h34 \pm 0.12km$ Tibet (306) $M_S 4.6 / 12$ , $m_b 4.4 / 6$ ,								
LSA	0.9	108	-iP	10 30	22.9	-2.4			BJI	85.3	313	eP	24 06	20.0	1.9		
			S	10 30	36.3	-0.8						PMZ		$m_b=5.1$	1.5	0.026	
			LN			6.0	15.6					eS	24 16	40.0	-6.0		
CD2	11.8	82	eP	10 32	56.6	-0.5						esS	24 16	56.0	-4.1		
KMI	12.2	110	eP	10 33	05.0	2.5						LZ		$M_S=4.8$	24.0	0.45	
			pP	10 33	12.0	2.6			TIY	87.1	310	eP	24 06	29.4	2.4		
			eS	10 35	24.0	5.5						S	24 17	00.0	-1.6		
			LN		$M_S=4.4$	10.0	1.20					sS	24 17	17.0	-0.4		
			LE			10.0	0.60					LZ		$M_S=5.3$	18.0	0.97	
			LZ		$M_S=4.1$	12.0	0.90		MAY 7d 01h 18m $39.3 \pm 0.06s$ , SD2.56 / 13 $24.38 N \pm 0.71km$ , $123.63 E \pm 0.80km$ , $h11 \pm 0.26km$ South-western Ryukyu Islands (246) $M_L 3.7 / 3$ , $m_b 4.0 / 2$ ,								
GYA	15.0	100	P	10 33	39.8	0.4			TIY	16.4	327	eP	01 22	28.3	-2.7		
			pP	10 33	50.0	3.3			MAY 7d 05h 17m $33.7 \pm 0.04s$ , SD1.43 / 301 $36.10 N \pm 0.70km$ , $100.36 E \pm 0.54km$ , $h10 \pm 0.09km$ Qinghai Province (325) $M_S 5.5 / 55$ , $M_L 4.8 / 6$ , $m_b 5.3 / 13$ ,								
			LN		$M_S=4.6$	11.0	1.50		LZH	2.8	89	+Pn	05 18	22.5	3.1		
			LE			11.0	0.60					Pg	05 18	25.0	1.5		
TIY	20.0	62	eP	10 34	38.9	-2.2						Sg	05 19	03.5	1.3		
			S	10 38	22.5	3.5											
			LN		$M_S=4.4$	12.0	0.76										
			LZ		$M_S=4.6$	9.0	1.07										
HHC	20.5	52	eP	10 34	45.6	-0.4											
			sS	10 38	37.0	-5.1											
			LN		$M_S=4.7$	12.0	1.05										
			LE			13.0	1.12										
			LZ		$M_S=4.5$	14.0	1.18										



GTA	3.3	353	+iPn	05 18	31.0	4.6			NJ2	15.8	99	-P	05 21	17.5	-1.3		
			Pg	05 18	38.6	6.0						pP	05 21	24.0	0.7		
			LE		$M_s=5.4$	10.0	74.0					S	05 24	11.0	-3.3		
CD2	5.9	150	Pn	05 19	06.0	4.4			DL2	17.1	74	LN		$M_b=5.5$	11.0	10.2	
			Sg	05 20	42.0	3.4						LE			12.0	4.29	
			SMN		$M_L=4.7$	1.0	0.54					LZ		$M_s=5.1$	12.0	6.58	
			SME			1.0	0.60					-P	05 21	36.0	1.2		
			LN		$M_s=5.7$	8.0	60.7					PMZ		$m_b=4.8$	1.0	0.050	
XAN	7.3	104	LZ		$M_s=4.5$	50.0	22.9		GZH	17.2	135	sP	05 21	47.0	4.1		
			iPn	05 19	21.5	0.5						eS	05 24	44.0	0.0		
			Sg	05 21	25.0	2.2						SMN			8.0	0.86	
			SMN		$M_L=5.0$	1.0	0.73					SME			7.0	1.10	
			SME			1.0	0.54					LN		$M_s=5.2$	14.0	6.83	
BTO	8.8	56	LN		$M_s=5.3$	10.0	18.8		SSE	18.0	100	LZ		$M_s=5.1$	14.0	6.03	
			LE			10.0	10.0					eP	05 21	36.8	1.2		
			P	05 19	44.5	0.0						S	05 24	43.5	-1.4		
			S	05 21	25.0	0.5						LN		$M_s=5.6$	9.0	5.10	
			LN		$M_s=5.1$	10.3	8.00					LE			8.0	8.60	
TIY	9.8	77	LE			13.7	8.00		SNY	18.9	65	LZ		$M_s=5.1$	14.0	6.20	
			LZ		$M_s=5.2$	6.2	8.00					eP	05 21	47.0	0.5		
			+iP	05 19	56.6	-1.5						PMZ		$m_b=5.1$	8.0	0.77	
			S	05 21	53.0	4.0						PP	05 22	00.5	-0.3		
			LN		$M_s=5.7$	10.0	33.3					sS	05 25	18.0	5.1		
HHC	10.0	58	LZ		$M_s=5.5$	8.0	19.4		QZN	18.9	151	LN		$M_s=5.4$	9.0	4.79	
			P	05 20	00.0	-0.6						LE			9.0	5.34	
			S	05 21	51.0	-2.4						LZ		$M_s=5.0$	16.0	5.47	
			LN		$M_s=5.5$	9.0	17.2					+P	05 21	57.0	-0.2		
			LE			10.0	8.44					PMZ		$m_b=5.0$	1.1	0.080	
LSA	10.0	233	LZ		$M_s=5.2$	12.0	15.0		QZH	19.2	120	PMZ		$m_b=5.2$	11.0	1.36	
			P	05 20	02.2	0.6						pP	05 22	05.5	3.7		
			S	05 21	56.0	1.6						eS	05 25	23.0	-2.1		
			LN		$M_s=5.5$	6.5	9.43					SMN			18.0	1.66	
			LE			6.0	7.19					SME			10.0	1.60	
GYA	11.0	149	LZ		$M_s=5.5$	6.0	12.8		KSH	19.6	287	LN		$M_s=5.4$	11.0	5.77	
			P	05 20	15.0	0.2						LE			7.0	3.12	
			S	05 22	17.0	-1.6						LZ		$M_s=4.9$	12.0	3.38	
			LN		$M_s=5.6$	8.0	17.4					P	05 21	57.0	-0.7		
			LE			8.0	9.60					PMZ		$m_b=5.1$	1.0	0.10	
KMI	11.1	169	LZ		$M_s=5.1$	10.0	9.20		CN2	20.7	60	eS	05 25	24.0	-1.9		
			-P	05 20	16.0	-0.1						sS	05 25	37.0	3.6		
			PMZ		$m_b=5.0$	2.0	0.090					LN		$M_s=5.7$	13.0	6.90	
			PMZ		$m_b=4.5$	4.0	0.050					LE			13.0	14.9	
			PP	05 20	24.0	0.0						eP	05 22	00.7	0.0		
WMQ	12.4	312	S	05 22	16.0	-4.9			MDJ	23.7	60	LN		$M_s=5.5$	9.0	5.45	
			LN		$M_s=5.5$	10.0	4.10					LE			9.0	4.66	
			LE			10.0	15.6					LZ		$M_s=5.1$	11.0	5.05	
			LZ		$M_s=5.4$	11.0	18.5					P	05 22	05.2	0.1		
			P	05 20	32.5	-0.8						PMZ		$m_b=5.7$	6.0	2.00	
WHN	12.9	111	S	05 22	51.0	-1.0			TIA	13.6	85	eS	05 25	39.0	-1.7		
			LZ		$M_s=4.7$	8.0	2.41					LE		$M_s=5.7$	10.0	12.5	
			-P	05 20	44.2	3.5						LZ		$M_s=5.2$	15.0	8.30	
			PMZ		$m_b=5.0$	0.6	0.020					+P	05 22	16.0	-0.6		
			sP	05 20	52.0	3.4						PMZ		$m_b=5.2$	1.0	0.10	
BJI	13.1	68	eS	05 23	07.6	1.8			MDJ	23.7	60	PMZ		$m_b=5.4$	5.0	0.80	
			LN		$M_s=5.8$	10.0	16.8					pP	05 22	25.0	3.3		
			LE			9.0	21.0					S	05 26	00.0	-1.9		
			LZ		$M_s=5.6$	8.0	17.0					SMN			8.0	1.20	
			eP	05 20	42.0	-0.4						SME			8.0	2.20	
TIA	13.6	85	PMZ		$m_b=5.2$	1.5	0.079		MDJ	23.7	60	LN		$M_s=5.6$	10.0	9.00	
			PMZ		$m_b=5.4$	5.0	0.40					LE			10.0	2.30	
			LN		$M_s=5.3$	10.0	8.16					+P	05 22	49.5	2.2		
			LE			9.0	2.71					PMZ		$m_b=5.2$	2.0	0.20	
			LZ		$M_s=5.1$	12.0	7.50					pP	05 22	58.0	5.4		
TIA	13.6	85	P	05 20	46.6	-2.2			MDJ	23.7	60	sP	05 23	01.5	5.9		
			S	05 23	20.0	-0.1						PP	05 23	25.0	5.3		
			LN		$M_s=5.5$	9.0	11.2					iS	05 27	04.0	4.6		
			LE			7.0	5.00					SME			9.0	1.50	
			LN		$M_s=5.0$	14.0	5.82										





MAY 7d 09h 33m 06.8 ± 0.04s, SD2.14 / 10 32.50 N ± 0.37km, 105.58 E ± 0.35km, h16 ± 0.09km Sichuan Province (307) M <sub>L</sub> 3.3 / 8,					MAY 7d 14h 52m 51.3 ± 0.06s, SD1.30 / 64 9.64 S ± 0.65km, 155.55 E ± 1.01km, h25 ± 0.15km D'Entrecasteaux Islands region (194) M <sub>S</sub> 5.1 / 7, m <sub>b</sub> 4.9 / 15,					MAY 8d 00h 01m 39.5 ± 0.03s, SD1.35 / 518 6.95 N ± 1.05km, 82.59 W ± 0.89km, h8 ± 0.20km Off coast of Central America (76) M <sub>S</sub> 6.7 / 44, m <sub>B</sub> 6.6 / 28, m <sub>b</sub> 6.1 / 51															
LN			M <sub>S</sub> = 5.5	13.0	8.00	SSE	52.2	322	eP	15 02 03.0	0.1				PMZ			m <sub>b</sub> = 4.8	10.0	0.019					
LZ			M <sub>S</sub> = 5.3	8.0	4.20	WHN	56.2	317	eP	15 02 33.0	0.6				sS	21 02	40.0	-0.2							
MAY 7d 09h 33m 06.8 ± 0.04s, SD2.14 / 10 32.50 N ± 0.37km, 105.58 E ± 0.35km, h16 ± 0.09km Sichuan Province (307) M <sub>L</sub> 3.3 / 8,					MAY 7d 14h 52m 51.3 ± 0.06s, SD1.30 / 64 9.64 S ± 0.65km, 155.55 E ± 1.01km, h25 ± 0.15km D'Entrecasteaux Islands region (194) M <sub>S</sub> 5.1 / 7, m <sub>b</sub> 4.9 / 15,					MAY 8d 00h 01m 39.5 ± 0.03s, SD1.35 / 518 6.95 N ± 1.05km, 82.59 W ± 0.89km, h8 ± 0.20km Off coast of Central America (76) M <sub>S</sub> 6.7 / 44, m <sub>B</sub> 6.6 / 28, m <sub>b</sub> 6.1 / 51															
CD2	2.2	225	Pn	09 33 43.2	-0.3	TIA	58.2	324	eP	15 02 50.9	4.5				LE			M <sub>S</sub> = 4.4	18.0	0.63					
			Pg	09 33 46.7	0.6	MDJ	58.9	339	eP	15 02 50.0	-1.2				LZ			M <sub>S</sub> = 4.1	18.0	0.45					
			Sn	09 34 11.6	-0.7	eS	15 10 50.0	-4.2							LN										
			Sg	09 34 15.8	-0.7	LZ			M <sub>S</sub> = 5.0	16.0	0.90	MDJ	121.1	334	PKP	00 20 36.5	2.5	LE			M <sub>S</sub> = 6.4	18.0	3.90		
			SMN		M <sub>L</sub> = 3.6	0.6	0.47	GYA	59.5	308	P	15 02 56.4	0.8	PPMZ			m <sub>B</sub> = 6.8	8.0	2.00	LZ			M <sub>S</sub> = 6.3	40.0	13.5
			SME			0.5	0.41	CN2	59.8	335	+P	15 02 56.8	-0.8	PP	00 22 08.0	1.4				LN			M <sub>S</sub> = 6.3	19.0	2.00
XAN	3.2	60	Pn	09 33 59.0	2.1	PMZ			m <sub>b</sub> = 5.0	1.0	0.020	SKKS	00 28 56.0	-1.5				LZ			M <sub>S</sub> = 6.6	22.0	13.0		
			Pg	09 34 04.5	1.3	pP	15 03 08.5	3.0				SS	00 38 32.0	-4.2				LE							
			Sg	09 34 45.0	-1.9	eS	15 11 00.0	-6.1				LE			M <sub>S</sub> = 6.4	18.0	3.90	LZ			M <sub>S</sub> = 6.3	40.0	13.5		
			SMN		M <sub>L</sub> = 3.4	0.5	0.13	LN			M <sub>S</sub> = 5.0	11.0	0.30	PKP	00 20 39.0	0.4				LZ			M <sub>S</sub> = 6.6	22.0	13.0
			SME			0.5	0.13	LE			M <sub>S</sub> = 5.1	13.0	0.65	ePKP	00 20 26.0	2.5				LE					
GYA	6.1	171	ePg	09 34 55.0	0.3	LZ			M <sub>S</sub> = 5.1	14.0	1.07	PPMZ			m <sub>B</sub> = 6.8	5.0	1.40	LZ			M <sub>S</sub> = 6.6	22.0	13.0		
			Sn	09 35 44.0	-4.3	BJI	61.4	326	eP	15 03 08.5	0.1	LN			M <sub>S</sub> = 6.3	19.0	2.00	PP	00 22 40.0	0.7					
			SMN		M <sub>L</sub> = 3.5	1.2	0.050	PMZ			m <sub>b</sub> = 4.7	1.5	0.016	LN			M <sub>S</sub> = 6.3	19.0	2.50	LZ			M <sub>S</sub> = 6.6	22.0	13.0
			SME			1.2	0.020	eS	15 11 00.0	-6.1				LZ			M <sub>S</sub> = 6.6	22.0	13.0	LZ					
MAY 7d 09h 33m 06.8 ± 0.04s, SD2.14 / 10 32.50 N ± 0.37km, 105.58 E ± 0.35km, h16 ± 0.09km Sichuan Province (307) M <sub>L</sub> 3.3 / 8,					MAY 7d 14h 52m 51.3 ± 0.06s, SD1.30 / 64 9.64 S ± 0.65km, 155.55 E ± 1.01km, h25 ± 0.15km D'Entrecasteaux Islands region (194) M <sub>S</sub> 5.1 / 7, m <sub>b</sub> 4.9 / 15,					MAY 8d 00h 01m 39.5 ± 0.03s, SD1.35 / 518 6.95 N ± 1.05km, 82.59 W ± 0.89km, h8 ± 0.20km Off coast of Central America (76) M <sub>S</sub> 6.7 / 44, m <sub>B</sub> 6.6 / 28, m <sub>b</sub> 6.1 / 51															
WHN	34.0	302	eP	20 58 23.0	-0.1	TIY	62.0	322	eP	15 03 12.0	-0.5	MDJ	123.5	336	ePKP	00 20 39.0	0.4	PKP	00 20 36.5	2.5					
QZN	36.3	281	+P	20 58 44.1	1.2	eS	15 11 32.0	-2.3				ePP	00 22 26.0	2.5				PPMZ			m <sub>B</sub> = 6.8	5.0	1.40		
BJI	36.7	318	eP	20 58 46.0	-0.5	LE			M <sub>S</sub> = 5.1	13.0	0.65	PPMZ			m <sub>B</sub> = 6.6	10.0	1.73	LN			M <sub>S</sub> = 6.3	19.0	2.00		
PMZ			m <sub>b</sub> = 5.1	1.5	0.052	LZ			M <sub>S</sub> = 5.1	14.0	1.07	LN			M <sub>S</sub> = 6.3	19.0	2.50	LZ			M <sub>S</sub> = 6.6	22.0	13.0		
eS	21 04	26.5	-0.2			CD2	63.9	311	eP	15 03 22.4	-3.0	SNY	125.9	336	-PKP	00 20 46.0	2.8	PP	00 22 40.0	0.7					
LZ			M <sub>S</sub> = 4.1	20.0	0.40	BTO	65.3	323	eP	15 03 33.0	-1.1	PP	00 22 56.0	-2.3				PPMZ			m <sub>B</sub> = 6.6	10.0	1.73		
WHN	34.0	302	eP	20 58 23.0	-0.1	LZH	66.6	316	+P	15 03 42.5	0.0	LZ			M <sub>S</sub> = 6.4	23.0	8.44	LZ			M <sub>S</sub> = 6.4	23.0	8.44		
QZN	36.3	281	+P	20 58 44.1	1.2	PMZ			m <sub>b</sub> = 5.3	2.5	0.094	SNY	125.9	336	-PKP	00 20 46.0	2.8	SKS	00 28 00.0	3.2					
BJI	36.7	318	eP	20 58 46.0	-0.5	sP	15 04 00.0	6.2				PP	00 22 40.0	0.7				SKKS	00 29 46.0	-2.3					
PMZ			m <sub>b</sub> = 5.1	1.5	0.052	LE			M <sub>S</sub> = 5.1	13.0	0.50	PPMZ			m <sub>B</sub> = 6.5	8.0	1.17	LN			M <sub>S</sub> = 6.8	19.0	10.8		
eS	21 04	26.5	-0.2			LZ			M <sub>S</sub> = 4.8	18.0	0.60	LZ			M <sub>S</sub> = 6.4	23.0	8.44	PP	00 23 00.0	-1.0					
LZ			M <sub>S</sub> = 4.1	20.0	0.40	WMQ	81.1	317	P	15 05 07.5	0.4	WMQ	128.7	9	PKP	00 20 49.0	0.1	PPMZ			m <sub>B</sub> = 6.5	8.0	1.17		
WHN	34.0	302	eP	20 58 23.0	-0.1	KSH	88.2	310	eP	15 05 47.0	4.5	PP	00 22 56.0	-2.3				LZ			M <sub>S</sub> = 6.4	23.0	8.44		
QZN	36.3	281	+P	20 58 44.1	1.2	MAY 7d 20h 51m 41.0 ± 0.04s, SD0.94 / 129 15.60 N ± 0.60km, 147.74 E ± 0.53km, h41 ± 0.17km Marianas region (215) M <sub>S</sub> 4.3 / 2, m <sub>b</sub> 4.9 / 31,					PPMZ			m <sub>B</sub> = 6.6	10.0	1.73	LZ			M <sub>S</sub> = 6.6	22.0	13.0			
BJI	36.7	318	eP	20 58 46.0	-0.5	SSE	28.7	307	-P	20 57 35.7	-1.5	LN			M <sub>S</sub> = 6.6	22.0	13.0	SKS	00 28 00.0	3.2					
PMZ			m <sub>b</sub> = 5.1	1.5	0.052	MAY 7d 20h 51m 41.0 ± 0.04s, SD0.94 / 129 15.60 N ± 0.60km, 147.74 E ± 0.53km, h41 ± 0.17km Marianas region (215) M <sub>S</sub> 4.3 / 2, m <sub>b</sub> 4.9 / 31,					SKKS	00 29 46.0	-2.3				LN			M <sub>S</sub> = 6.8	19.0	10.8			
eS	21 04	26.5	-0.2			SSE	28.7	307	-P	20 57 35.7	-1.5	PP	00 23 00.0	-1.0				PP	00 23 00.0	-1.0					
LZ			M <sub>S</sub> = 4.1	20.0	0.40	MAY 7d 20h 51m 41.0 ± 0.04s, SD0.94 / 129 15.60 N ± 0.60km, 147.74 E ± 0.53km, h41 ± 0.17km Marianas region (215) M <sub>S</sub> 4.3 / 2, m <sub>b</sub> 4.9 / 31,					PPMZ			m <sub>B</sub> = 6.8	8.0	2.50	PPMZ			m <sub>B</sub> = 6.8	8.0	2.50			













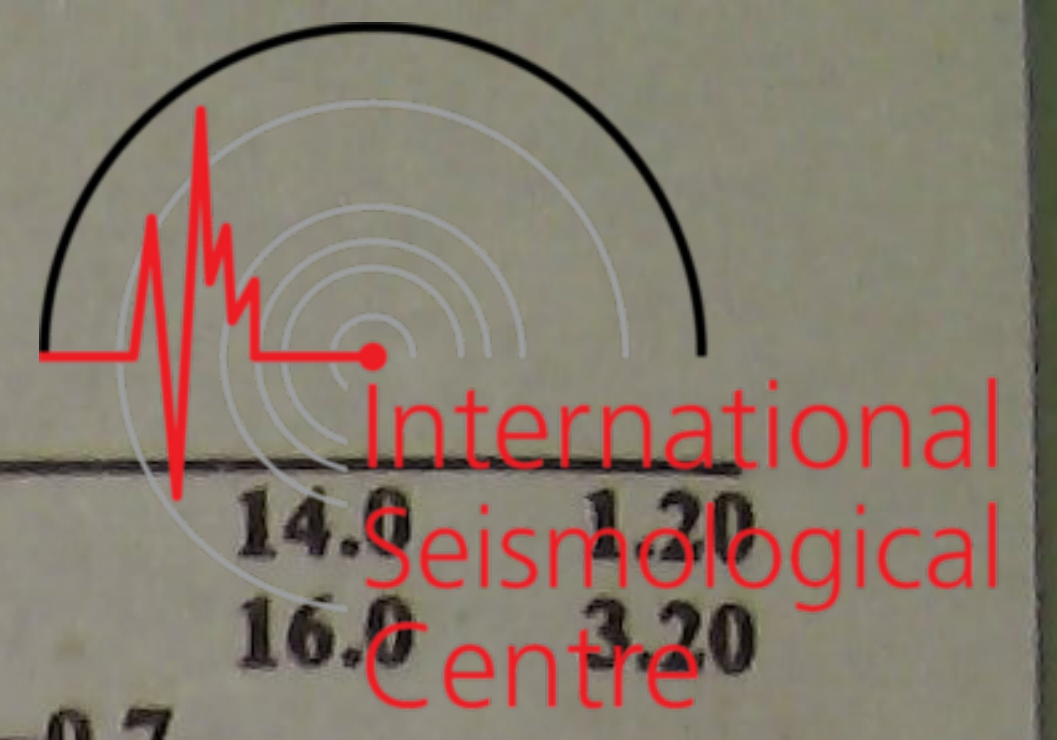












SNY	43.0	283	+P	09 32	06.4	0.2		
			PMZ		$m_b = 5.1$		1.2	0.040
DL2	46.0	280	eP	09 32	30.0	0.1		
			pP	09 32	36.0	-3.1		
BJI	48.6	285	eP	09 32	50.5	0.2		
			PMZ		$m_b = 4.8$		1.0	0.012
HHC	50.8	289	eP	09 33	07.0	-0.6		
SSE	51.3	273	+P	09 33	11.5	0.0		
			PMZ		$m_b = 5.1$		1.0	0.024
			sP	09 33	26.6	1.9		
BTO	51.9	290	P	09 33	16.0	0.4		
NJ2	52.1	276	eP	09 33	20.0	2.5		
TIY	52.3	285	+P	09 33	19.0	0.2		
			LZ		$M_s = 4.8$		16.0	0.72
WHN	56.0	278	eP	09 33	46.0	0.4		
XAN	56.9	284	P	09 33	51.0	-1.2		
LZH	58.5	290	+P	09 34	03.0	-0.7		
			PMZ		$m_b = 5.3$		1.5	0.058
			LZ		$M_s = 4.2$		20.0	0.20
GTA	58.5	295	+iP	09 34	03.0	-0.9		
WMQ	61.9	306	P	09 34	26.5	-0.7		
CD2	62.2	285	P	09 34	28.4	-0.3		
GYA	63.6	280	P	09 34	38.8	0.5		
LSA	70.5	293	P	09 35	22.4	0.5		

MAY 11d 01h 37m  $20.3 \pm 0.05s$ , SD1.89 / 12  
 33.37 N  $\pm 0.43km$ , 81.00 E  $\pm 0.55km$ , h30  $\pm 0.12km$   
 Tibet (306)  
 $M_L 3.3 / 1$ ,  $m_b 3.9 / 1$ ,

KMI	20.6	108	+P	01 42	00.0	-0.4		
TIY	25.9	71	eP	01 42	52.1	0.5		

MAY 11d 04h 10m  $06.5 \pm 0.06s$ , SD2.76 / 9  
 41.59 N  $\pm 0.89km$ , 90.46 E  $\pm 0.48km$ , h26  $\pm 0.01km$   
 Southern Xinjiang Province (321)  
 $M_L 4.1 / 8$ ,

WMQ	3.0	319	iPn	04 10	53.6	0.5		
			Sn	04 11	32.0	2.2		
			Sg	04 11	37.6	-3.3		
GTA	7.5	104	Pn	04 11	56.0	1.7		
			Pg	04 12	20.0	1.8		
			Sg	04 13	53.8	-6.4		
			SMN		$M_L = 4.1$		0.8	0.079
			SME				0.8	0.054

MAY 11d 05h 03m  $26.5 \pm 0.06s$ , SD0.99 / 170  
 51.56 N  $\pm 1.06km$ , 159.35 E  $\pm 0.82km$ , h11  $\pm 0.10km$   
 Near east coast of Kamchatka (218)  
 $M_s 5.3 / 34$ ,  $m_b 5.3 / 1$ ,  $m_b 5.0 / 59$

MDJ	21.0	262	eP	05 08	10.0	-2.4		
			LZ		$M_s = 4.3$		20.0	3.26
CN2	23.9	265	eP	05 08	42.0	0.1		
			eS	05 12	53.0	-2.4		
			LN		$M_s = 5.2$		17.0	4.90
			LE				17.0	2.40
			LZ		$M_s = 5.2$		16.0	6.50
SNY	26.2	262	-P	05 09	03.0	-0.1		
			eS	05 13	30.0	-2.7		
			LN		$M_s = 5.3$		14.0	2.98
			LE				15.0	3.93
			LZ		$M_s = 5.4$		14.0	6.77
DL2	29.1	259	eP	05 09	29.0	-0.7		
			eS	05 14	18.0	-2.1		
			LN		$M_s = 5.2$		16.0	3.85
			LZ		$M_s = 4.9$		14.0	1.77
BJI	31.8	266	eP	05 09	55.0	1.4		
			esS	05 15	16.0	4.0		
			LN		$M_s = 5.2$		15.0	2.90

								LE		14.0	1.30	
								LZ	$M_s = 5.1$	16.0	3.20	
TIA	33.6	260	-P	05 10	08.4	-0.7		LN	$M_s = 5.2$	15.0	2.22	
								LE		15.0	1.91	
								LZ	$M_s = 5.1$	16.0	2.84	
HHC	34.2	271	eP	05 10	14.0	-0.7		LN	$M_s = 5.4$	12.0	1.22	
								LE		13.0	2.90	
								LZ	$M_s = 5.3$	16.0	4.99	
SSE	34.7	249	eP	05 10	17.4	-1.2		LN	$M_s = 4.9$	13.0	0.77	
								LE		13.0	0.61	
								LZ	$M_s = 4.5$	20.0	0.92	
BTO	35.3	272	eP	05 10	23.7	-0.5		PcS		05 16	44.0	4.1
								LN	$M_s = 5.6$	16.0	5.70	
								LE		16.0	2.60	
NJ2	35.3	252	+P	05 10	25.0	0.6		LN	$M_s = 5.3$	15.0	2.42	
								LE		15.0	1.22	
								LZ	$M_s = 4.8$	18.0	1.43	
TIY	35.5	266	-P	05 10	26.1	0.1		S		05 15	55.0	-4.8
								LN	$M_s = 5.4$	16.0	4.16	
								LZ	$M_s = 5.3$	15.0	3.79	
WHN	39.1	255	eP	05 10	56.5	0.3		pP		05 11	05.0	3.2
								eS		05 16	53.5	-2.3
								LE	$M_s = 5.1$	13.0	1.43	
								LZ	$M_s = 5.0$	16.0	1.78	
XAN	40.1	264	P	05 11	03.6	-0.4						
QZH	40.8	245	eP	05 11	08.0	-2.2		LN	$M_s = 4.9$	14.0	0.82	
								LZ	$M_s = 4.9$	14.0	0.82	
LZH	41.9	271	+P	05 11	19.5	0.2		PMZ	$m_b = 5.0$	1.5	0.042	
								pP		05 11	28.5	3.9
								LN	$M_s = 5.5$	14.0	2.21	
								LE		15.0	2.57	
								LZ	$M_s = 5.3$	18.0	3.59	
GTA	42.3	278	eP	05 11	22.5	-0.5		LE	$M_s = 5.6$	14.0	3.89	
								LZ	$M_s = 5.6$	14.0	5.42	
CD2	45.4	265	eP	05 11	47.0	-0.4		eS		05 18	24.5	-3.5
								LN	$M_s = 5.4$	15.0	2.52	
								LZ	$M_s = 5.1$	16.0	1.70	
GYA	46.7	258	+iP	05 11	59.8	1.6		PMZ	$m_b = 5.3$	1.2	0.060	
								sP		05 12	09.0	2.6
								S		05 18	48.4	2.1
								LN	$M_s = 5.4$	18.0	2.10	
								LE		18.0	1.40	
WMQ	47.1	290	P	05 12	00.4	-0.4						
								pP		05 12	07.5	1.3
								LE	$M_s = 5.6$	14.0	3.25	
								LZ	$M_s = 5.5$	15.0	4.50	
KMI	50.1	261	+P	05 12	25.0	0.6		PMZ	$m_b = 5.5$	1.5	0.10	
								LN	$M_s = 5.4$	15.0	1.70	
								LE		18.0	1.30	
								LZ	$M_s = 5.3$	15.0	2.30	
QZN	50.5	249	eP	05 12	28.4	1.4		eS		05 19	38.0	-1.6
								LN	$M_s = 5.4$	17.0	1.52	
								LE		17.0	1.58	
KSH	56.6	293	eP	05 13	16.0	3.3						



MAY 11d 13h 10m 19.8 ± 0.04s, SD0.98 / 613									
41.87 N ± 0.61km, 130.92 E ± 0.61km, h582 ± 0.32km									
North Korea (659)									
m <sub>b</sub> 6.4 / 38, m <sub>b</sub> 5.7 / 129,									
MDJ	2.9	341	+P	13 11 39.0	1.5				
			PMZ			8.0	27.5		
			S	13 12 38.0	-0.6				
			SMN			15.0	73.6		
CN2	4.5	298	ScS	13 23 53.0	-0.7				
			+iP	13 11 48.0	0.0				
			PMZ			4.0	24.3		
			S	13 13 00.0	2.5				
SNY	5.5	272	SMN			7.0	31.6		
			SME			7.0	37.3		
			PcS	13 21 17.0	-0.7				
			ScS	13 23 50.0	-4.7				
DL2	7.7	250	+iP	13 11 58.0	1.7				
			PMZ		m <sub>b</sub> = 5.9	1.4	2.09		
			PMZ			15.0	25.2		
			iS	13 13 13.1	0.6				
BJI	11.3	266	ScS	13 23 52.0	-3.7				
			+iP	13 12 17.0	0.8				
			PMZ		m <sub>b</sub> = 5.8	1.0	0.95		
			PMZ		m <sub>b</sub> = 6.4	4.0	15.8		
TIA	12.1	247	sP	13 13 46.0	-4.3				
			eS	13 13 47.0	-1.8				
			SMN			4.0	29.1		
			SME			4.0	22.3		
SSE	13.3	219	ScS	13 23 57.0	-1.4				
			-P	13 12 53.0	1.2				
			PMZ		m <sub>b</sub> = 5.8	1.4	0.88		
			PMZ		m <sub>b</sub> = 6.4	5.0	14.1		
HHC	14.6	272	esP	13 14 44.0	2.5				
			eS	13 14 52.0	-1.8				
			eScP	13 20 30.0	-0.2				
			eScS	13 24 03.0	-1.8				
NJ2	13.7	228	-P	13 13 00.0	0.1				
			PMZ		m <sub>B</sub> = 6.2	4.0	6.50		
			S	13 15 11.0	2.9				
			ScP	13 20 29.8	-1.6				
TIY	14.8	260	ScS	13 24 07.0	0.5				
			+P	13 13 11.0	-0.6				
			PMZ		m <sub>b</sub> = 5.4	1.0	0.23		
			S	13 15 27.0	-2.1				
BTO	15.8	272	ScP	13 20 32.0	-1.2				
			ScS	13 24 09.0	-0.2				
			-iP	13 13 16.0	0.0				
			PMZ		m <sub>b</sub> = 5.7	2.5	1.10		
KSH	41.2	286	S	13 15 42.5	5.3				
			ScP	13 20 32.6	-1.4				
			ScS	13 24 09.6	-0.7				
			-P	13 13 26.2	1.8				
KMI	28.6	243	PMZ		m <sub>b</sub> = 5.4	1.2	0.21		
			PMZ		m <sub>B</sub> = 6.5	6.0	14.1		
			sP	13 15 31.0	4.0				
			S	13 15 57.0	4.7				
GZH	23.8	224	SMN			12.0	44.7		
			SME			12.0	57.2		
			-iP	13 13 28.4	1.8				
			PMZ		m <sub>b</sub> = 6.1	0.8	0.70		
GTA	23.7	274	PMZ		m <sub>B</sub> = 6.6	6.0	17.1		
			sP	13 15 35.5	5.4				
			iS	13 16 03.0	5.9				
			SMN			15.0	51.2		
GZA	25.2	240	SME			12.0	34.2		
			ScS	13 24 10.0	-3.0				
			-iP	13 13 37.5	1.4				
			PMZ		m <sub>B</sub> = 6.7	6.0	18.2		
GZH	23.8	224	+P	13 11 39.0	1.5				
			PMZ			8.0	27.5		
			S	13 12 38.0	-0.6				
			SMN			15.0	73.6		
GZA	25.2	240	ScS	13 23 53.0	-0.7				
			+iP	13 11 48.0	0.0				
			PMZ			4.0	24.3		
			S	13 13 00.0	2.5				
GZA	25.2	240	SMN			7.0	31.6		
			SME			7.0	37.3		
			PcS	13 21 17.0	-0.7				
			ScS	13 23 50.0	-4.7				
GZA	25.2	240	+iP	13 11 58.0	1.7				
			PMZ		m <sub>b</sub> = 5.9	1.4	2.09		
			PMZ			15.0	25.2		
			iS	13 13 13.1	0.6				
GZA	25.2	240	ScS	13 23 52.0	-3.7				
			+iP	13 12 17.0	0.8				
			PMZ		m <sub>b</sub> = 5.8	1.0	0.95		
			PMZ		m <sub>B</sub> = 6.4	4.0	15.8		
GZA	25.2	240	sP	13 13 46.0	-4.3				
			eS	13 13 47.0	-1.8				
			SMN			4.0	29.1		
			SME			4.0	22.3		
GZA	25.2	240	ScS	13 23 57.0	-1.4				
			-P	13 12 53.0	1.2				
			PMZ		m <sub>b</sub> = 5.8	1.4	0.88		
			PMZ		m <sub>B</sub> = 6.4	5.0	14.1		
GZA	25.2	240	esP	13 14 44.0	2.5				
			eS	13 14 52.0	-1.8				
			eScP	13 20 30.0	-0.2				
			eScS	13 24 03.0	-1.8				
GZA	25.2	240	-P	13 13 00.0	0.1				
			PMZ		m <sub>B</sub> = 6.2	4.0	6.50		
			S	13 15 11.0	2.9				
			ScP	13 20 29.8	-1.6				
GZA	25.2	240	ScS	13 24 07.0	0.5				
			+P	13 13 11.0	-0.6				
			PMZ		m <sub>b</sub> = 5.4	1.0	0.23		
			S	13 15 27.0	-2.1				
GZA	25.2	240	ScP	13 20 32.0	-1.2				
			ScS	13 24 09.0	-0.2				
			-iP	13 13 16.0	0.0				
			PMZ		m <sub>b</sub> = 5.7	2.5	1.10		
GZA	25.2	240	S	13 15 42.5	5.3				
			ScP	13 20 32.6	-1.4				
			ScS	13 24 09.6	-0.7				
			-P	13 13 26.2	1.8				
GZA	25.2	240	PMZ		m <sub>b</sub> = 5.4	1.2	0.21		
			PMZ		m <sub>B</sub> = 6.5	6.0	14.1		
			sP	13 15 31.0	4.0				
			S	13 15 57.0	4.7				
GZA	25.2	240	SMN			12.0	44.7		
			SME			12.0	57.2		
			-iP	13 13 28.4	1.8				
			PMZ		m <sub>b</sub> = 6.1	0.8	0.70		
GZA	25.2	240	PMZ		m <sub>B</sub> = 6.6	6.0	17.1		
			sP	13 15 35.5	5.4				
			iS	13 16 03.0	5.9				
			SMN			15.0	51.2		
GZA	25.2	240	SME			12.0	34.2		
			ScS	13 24 10.0	-3.0				
			-iP	13 13 37.5	1.4				
			PMZ		m <sub>B</sub> = 6.7	6.0	18.2		
GZA	25.2	240	+P	13 11 39.0	1.5				
			PMZ			8.0	27.5		
			S	13 12 38.0	-0.6				
			SMN			15.0	73.6		
GZA	25.2	240	ScS	13 23 53.0	-0.7				
			+iP	13 11 48.0	0.0				
			PMZ			4.0	24.3		
			S	13 13 00.0	2.5				
GZA	25.2	240	SMN			7.0	31.6		
			SME			7.0	37.3		
			PcS	13 21 17.0	-0.7				
			ScS	13 23 50.0	-4.7				
GZA	25.2	240	+iP	13 11 58.0	1.7				
			PMZ		m <sub>b</sub> = 5.9	1.4	2.09		
			PMZ			15.0	25.2		
			iS	13 13 13.1	0.6				
GZA	25.2	240	ScS	13 23 52.0	-3.7				
			+iP	13 12 17.0	0.8				
			PMZ		m <sub>b</sub> = 5.8	1.0	0.95		
			PMZ		m <sub>B</sub> = 6.4	4.0	15.8		
GZA	25.2	240	sP	13 13 46.0	-4.3				
			eS	13 13 47.0	-1.8				
			SMN			4.0	29.1		
			SME			4.0	22.3		
GZA	25.2	240	ScS	13 23 57.0	-1.4				
			-P	13 12 53.0	1.2				
			PMZ		m <sub>b</sub> = 5.8	1.4	0.88		
			PMZ		m <sub>B</sub> = 6.4	5.0	14.1		
GZA	25.2	240	esP	13 14 44.0	2.5				
			eS	13 14 52.0	-1.8				
			eScP	13 20 30.0	-0.2				
			eScS	13 24 03.0	-1.8				
GZA	25.2	240	-P	13 13 00.0	0.1				
			PMZ		m <sub>B</sub> = 6.2	4.0	6.50		
			S	13 15 11.0	2.9				
			ScP	13 20 29.8	-1.6				
GZA	25.2	240	ScS	13 24 07.0	0.5				
			+P	13 13 11.0	-0.6				
			PMZ		m <sub>b</sub> = 5.4	1.0	0.23		
			S	13 15 27.0	-2.1				
GZA	25.2	240	ScP	13 20 32.0	-1.2				
			ScS	13 24 09.0	-0.2				
			-iP	13 13 16.0	0.0				
			PMZ		m <sub>b</sub> = 5.7	2.5	1.10		
GZA	25.2	240	S	13 15 42.5	5.3				
			ScP	13 20 32.6	-1.4				
			ScS	13 24 09.6	-0.7				
			-P	13 13 26.2	1.8				







$M_s 4.3 / 4, m_b 4.4 / 10,$

SSE	19.1	349	eP	21 09 54.0	-1.1		
			eS	21 13 26.0	3.1		
NJ2	20.6	344	eP	21 10 13.6	2.8		
WHN	20.9	332	eP	21 10 14.0	0.1		
GYA	22.6	311	P	21 10 33.8	2.2		
			LN	$M_s = 4.3$		15.0	0.50
			LE			15.0	0.40
TIA	25.0	344	eP	21 10 53.6	-0.6		
KMI	25.0	304	-P	21 10 56.0	1.2		
			pP	21 11 03.5	-1.1		
			LZ	$M_s = 4.2$		18.0	0.70
XAN	26.4	328	P	21 11 07.0	-0.5		
CD2	27.3	316	eP	21 11 15.2	-0.9		
TIY	27.9	337	eP	21 11 20.6	-0.5		
			LN	$M_s = 4.3$		16.0	0.52
			LZ	$M_s = 4.2$		18.0	0.61
BJI	28.8	345	eP	21 11 28.0	-1.5		
			PMZ	$m_b = 4.3$		1.2	0.0080
LZH	30.7	324	P	21 11 47.0	0.6		
			LN	$M_s = 4.5$		15.0	0.60
			LZ	$M_s = 4.4$		16.0	0.60
BTO	31.3	337	eP	21 11 50.2	-1.5		
GTA	35.3	324	eP	21 12 26.3	0.0		
LSA	36.3	304	P	21 12 35.0	0.2		
WMQ	45.2	321	P	21 13 47.8	0.0		

CN2	12.5	251	+iP	04 52 51.0	-0.6		
			PMZ	$m_b = 6.8$			
			S	04 55 00.0	-2.5		
SNY	14.7	247	+iP	04 53 13.5	0.2		
			PMZ	$m_b = 6.7$		6.5	26.5
			sP	04 55 24.0	4.3		
			iS	04 55 43.0	0.4		
			iScS	05 03 54.2	-2.4		
DL2	17.7	243	P	04 53 42.0	0.3		
			PMZ	$m_b = 6.2$		1.0	0.79
			PMZ	$m_b = 6.8$		5.0	15.9
			S	04 56 31.0	-2.3		
			SMN			12.0	61.7
			SME			12.0	50.2
BJI	20.3	253	-eP	04 54 06.0	0.0		
			PMZ	$m_b = 6.9$		7.0	22.4
			sP	04 56 30.0	-4.6		
			eS	04 57 16.0	-1.5		
			eScS	05 04 14.0	0.1		
TIA	22.2	244	+P	04 54 22.2	-0.5		
			PMZ	$m_b = 6.3$		9.0	6.90
			ScS	05 04 15.9	-4.8		
HHC	22.8	260	-iP	04 54 29.6	0.7		
			sP	04 57 07.0	1.2		
			S	04 57 59.0	1.8		
SSE	23.8	229	-P	04 54 37.0	-0.3		
			PMZ	$m_b = 6.5$		4.0	5.22
			sP	04 57 15.0	-1.3		
			PcP	04 57 59.0	0.3		
			S	04 58 12.0	-0.4		
			ScP	05 00 39.0	-0.9		
			ScS	05 04 27.0	-0.1		
BTO	24.0	261	-iP	04 54 38.0	-1.0		
			PMZ	$m_b = 6.8$		4.0	8.70
			sP	04 57 18.0	-0.2		
TIY	24.1	253	-iP	04 54 40.0	0.3		
			PMZ	$m_b = 6.4$		1.0	0.98
			PMZ	$m_b = 6.7$		7.0	13.6
			sP	04 57 19.0	0.0		
			sS	04 58 20.0	3.8		
NJ2	24.2	234	-iP	04 54 40.5	-0.6		
			PMZ	$m_b = 6.2$		0.7	0.39
			PMZ	$m_b = 6.4$		4.0	4.10
			S	04 58 16.0	-3.3		
			ScS	05 04 28.2	-0.7		
WHN	27.9	239	-iP	04 55 12.5	-0.2		
			PMZ	$m_b = 6.3$		1.0	0.74
			PMZ	$m_b = 6.7$		4.0	7.68
			iS	04 59 14.5	-2.1		
XAN	28.6	251	-iP	04 55 19.0	-0.1		
			PMZ	$m_b = 6.7$		5.0	10.0
			PcP	04 58 10.0	0.0		
			S	04 59 25.0	-2.2		
			SMN			8.0	24.4
			SME			7.0	26.1
QZH	30.2	226	+P	04 55 32.0	-0.7		
			PMZ	$m_b = 6.3$		0.8	0.67
			PMZ	$m_b = 6.3$		4.0	3.10
			sP	04 58 20.0	2.2		
			iS	04 59 50.0	-2.7		
LZH	30.5	259	-iP	04 55 36.6	0.9		
			PMZ	$m_b = 6.7$		2.0	4.44
			PMZ	$m_b = 6.9$		6.0	20.4
			sP	04 58 25.0	4.2		
			iS	04 59 57.0	-1.2		
			SMN			10.0	43.7
			SME			12.0	81.5
			ScP	05 01 00.0	-0.3		

MAY 11d 23h 43m  $49.9 \pm 0.03s$ , SD1.19 / 146  
 17.29 N  $\pm 0.90km$ , 100.66 W  $\pm 0.75km$ , h27  $\pm 0.35km$   
 Near coast of Guerrero, Mexico (58)  
 $m_b 5.2 / 51,$

WMQ	118.7	353	PKP	24 02 36.8	-0.1		
GYA	129.0	328	PKP	24 02 56.8	-0.1		
KMI	132.0	331	-PKP	24 03 04.0	1.3		

MAY 12d 00h 36m  $50.3 \pm 0.08s$ , SD2.87 / 26  
 36.27 N  $\pm 0.78km$ , 100.25 E  $\pm 0.79km$ , h31  $\pm 0.19km$   
 Qinghai Province (325)  
 $M_s 3.7 / 2, M_L 4.1 / 3, m_b 3.6 / 2$

LZH	2.9	93	+Pn	00 37 36.5	1.3		
			Pg	00 37 41.0	-1.0		
			Sg	00 38 20.0	-2.0		
			SMN			2.0	1.17
			SME			1.8	1.24
			LN			5.0	1.13
GTA	3.2	354	Pn	00 37 42.0	3.6		
CD2	6.1	150	ePg	00 38 40.6	2.4		
XAN	7.4	105	ePn	00 38 35.4	-1.9		
BTO	8.8	58	eP	00 38 58.0	-0.5		
			LN	$M_s = 3.6$		10.0	0.20
			LE			10.0	0.20
TIY	9.9	78	eP	00 39 13.4	0.3		
			sS	00 41 12.0	-2.4		
			LN	$M_s = 3.8$		15.0	0.66
WMQ	12.2	312	P	00 39 40.5	-4.6		
			S	00 42 02.4	1.7		
SSE	18.2	100	eP	00 41 00.5	-1.5		
			S	00 44 22.0	1.8		
			LZ	$M_s = 4.2$		16.0	0.88

MAY 12d 04h 50m  $07.8 \pm 0.03s$ , SD0.91 / 750  
 49.08 N  $\pm 0.66km$ , 141.87 E  $\pm 0.63km$ , h606  $\pm 0.18km$   
 Sakhalin (662)  
 $m_b 6.6 / 39, m_b 6.1 / 71,$

MDJ	9.5	247	+iP	04 52 22.9	0.5		
			PMZ	$m_b = 6.4$		12.0	46.2
			iS	04 54 04.0	-6.2		
			ScS	05 03 47.5	2.3		

MAY 12d 04h 50m  $07.8 \pm 0.03s$ , SD0.91 / 750  
 49.08 N  $\pm 0.66km$ , 141.87 E  $\pm 0.63km$ , h606  $\pm 0.18km$   
 Sakhalin (662)  
 $m_b 6.6 / 39, m_b 6.1 / 71,$

LZH	30.5	259	-iP	04 55 36.6	0.9		
			PMZ	$m_b = 6.7$		2.0	4.44
			PMZ	$m_b = 6.9$		6.0	20.4
			sP	04 58 25.0	4.2		
			iS	04 59 57.0	-1.2		
			SMN			10.0	43.7
			SME			12.0	81.5
			ScP	05 01 00.0	-0.3		







TIY	55.7	324	S	21 32	38.0	2.6			GZH	85.9	305	+P	04 35	48.0	-1.5								
			LN			$M_s = 5.4$	19.0	1.90				PMZ		$m_b = 6.2$	1.0	0.22							
			eP	21 24	59.0	-1.1						PMZ		$m_b = 6.2$	8.0	1.79							
			pP	21 25	17.0	-1.2						eS	04 46	16.0	-4.8								
			S	21 32	41.0	2.7						LE		$M_s = 6.4$	17.0	8.18							
CD2	57.3	313	LN			$M_s = 5.6$	20.0	3.50	SSE	87.3	315	-P	04 35	56.0	-0.5								
			LZ			$M_s = 5.6$	25.0	6.81				PMZ		$m_b = 5.6$	1.3	0.066							
			eP	21 25	10.0	-1.4						PMZ		$m_b = 6.3$	6.0	1.71							
			eS	21 33	04.5	3.9						SKS	04 46	20.0	0.7								
			LN			$M_s = 5.6$	20.0	2.94				S	04 46	32.0	-1.0								
HHC	58.3	327	LZ			$M_s = 5.2$	27.0	2.80	NJ2	89.3	314	+iP	04 36	05.0	-1.1								
			+P	21 25	18.0	-0.8						PMZ		$m_b = 6.1$	8.0	1.04							
			S	21 33	10.0	-3.0						pP	04 36	14.2	0.8								
			LN			$M_s = 5.7$	19.0	2.51				SKS	04 46	35.0	3.3								
			LE				19.0	2.42				S	04 46	55.0	3.4								
BTO	59.0	325	P	21 25	22.0	-1.6			WHN	90.8	311	P	04 36	11.6	-1.1								
			S	21 33	18.0	-4.0						PMZ		$m_b = 6.1$	1.0	0.12							
			LN			$M_s = 5.7$	18.0	2.80				PMZ		$m_b = 6.3$	6.0	1.04							
			LE				18.0	1.50				pP	04 36	20.0	0.0								
			LZH	60.1	318	eP	21 25	29.5				-1.2											
GTA	64.6	319	PMZ			$m_b = 5.1$	2.0	0.047	GYA	92.5	303	+iP	04 36	20.0	-1.1								
			PMZ			$m_b = 5.4$	7.0	0.37				pP	04 36	30.0	1.7								
			pP	21 25	49.0	0.1						sP	04 36	34.4	3.0								
			sP	21 25	56.0	-1.4						PP	04 40	02.0	-1.9								
			ePP	21 27	49.0	4.1						S	04 47	24.0	3.9								
			S	21 33	37.0	1.8						SKS	04 46	53.0	2.6								
			SME				7.0	0.62				SS	04 53	38.0	2.1								
			sS	21 34	12.0	3.9						LN		$M_s = 6.5$	20.0	8.80							
			LN			$M_s = 5.5$	16.0	0.72				LE			20.0	6.30							
			LE				20.0	2.32				LZ		$M_s = 6.0$	20.0	4.90							
			LZ			$M_s = 5.4$	28.0	4.41				LZ		$M_s = 5.9$	20.0	5.02							
			eP	21 25	59.8	-0.8						DL2	93.2	321	P	04 36	23.0	-1.0					
			pP	21 26	18.5	-0.5									PMZ		$m_b = 5.8$	8.0	0.36				
			eS	21 34	36.0	2.7									PP	04 40	06.0	-3.2					
			LE			$M_s = 5.2$	17.0	0.88							SKS	04 46	52.0	-2.1					
LZ			$M_s = 5.3$	30.0	2.91				S	04 47	24.0	-1.9											
LSA	66.5	306	P	21 26	13.0	-0.2																	
WMQ	74.6	318	P	21 27	04.0	1.9																	
KSH	81.5	311	PMZ			$m_b = 4.6$	1.0	0.010	TIA	93.4	316	P	04 36	24.7	-0.3								
			pP	21 27	17.4	-3.5						SKS	04 46	55.4	0.0								
			sP	21 27	32.5	3.2						eS	04 47	29.5	-0.1								
			S	21 36	36.0	6.4						LN		$M_s = 6.4$	18.0	2.80							
			SMN				5.0	0.19				LE			18.0	6.30							
			SKS	21 36	54.0	-3.8						LZ		$M_s = 6.1$	21.0	6.50							
			LZ			$M_s = 5.4$	22.0	2.24				KMI	94.2	299	+P	04 36	29.5	0.7					
			eP	21 27	40.0	-0.1									PMZ		$m_b = 5.9$	2.0	0.10				
			QZH	84.1	310	PMZ						$m_b = 6.3$	1.0	0.31	MDJ	94.3	329	eP	04 36	28.4	-0.5		
						PMZ						$m_b = 6.3$	6.0	1.80				SKS	04 47	00.0	-0.1		
PP	04 38	58.0				2.8			S	04 47	42.0	6.8											
S	04 46	00.0				-1.3			LN		$M_s = 6.5$	18.0	5.80										
sS	04 46	16.0				0.8			LE			20.0	8.60										
SS	04 51	38.0				5.2			LZ		$M_s = 6.5$	18.0	15.2										
LE						$M_s = 6.1$	22.0	5.88															
LZ						$M_s = 5.8$	42.0	8.41															
+P	04 35	46.0				-0.3																	
PMZ						$m_b = 6.1$	7.5	1.30															
QZN	85.3	300	PP	04 39	04.0	-0.6																	
			SKS	04 46	04.0	-1.5																	
			eS	04 46	12.0	-2.6																	
			SS	04 51	50.0	-0.4																	
			LN			$M_s = 6.5$	17.5	8.20															
LE				18.0	4.70																		

MAY 13d 04h 23m 08.8 ± 0.04s, SD1.19 / 442  
 40.28 S ± 0.90km, 176.09 E ± 0.89km, h20 ± 0.29km  
 North Island, New Zealand (159)  
 $M_s 6.4 / 46, m_b 6.2 / 20, m_b 5.9 / 56$

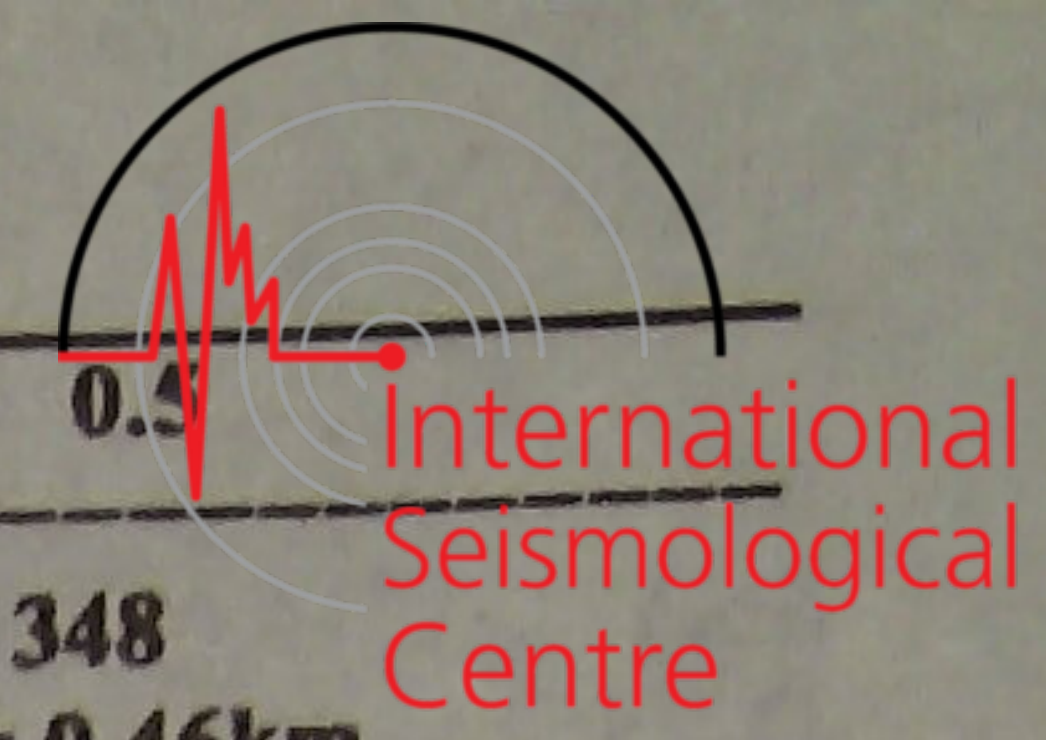


SNY	94.6 323	LZ	$M_s=6.1$	24.0	7.26	GTA	105.5 309	Pdif	04 37 18.0	-1.2	International Seismological Centre									
		+iP	04 36 29.0	-1.3	PP			04 41 41.0	-1.9											
		PMZ		13.0	1.07			SS	04 56 32.0	-4.1										
		pP	04 36 37.0	-0.6	LN			$M_s=6.5$	18.0	6.38										
		PP	04 40 17.0	-2.5	LZ			$M_s=6.4$	18.0	9.42										
		SKS	04 46 58.0	-3.7	WMQ			115.4 307	ePKP	04 41 50.5		0.2								
		iS	04 47 40.0	0.6					PP	04 42 53.0		-2.3								
		SMN		28.0					4.62	PPMZ		$m_B=6.5$	6.0	0.97						
		SME		24.0					6.44	PKS		04 45 26.0	1.4							
		SS	04 54 04.0	-0.8					LZ	$M_s=6.2$		19.0	5.69							
LN	$M_s=6.3$	17.0	4.00	KSH		120.8 298	PKP		04 42 02.0	1.0										
LE		18.0	3.10				SKS		04 49 09.0	0.9										
LZ	$M_s=6.0$	38.0	10.9				LE		$M_s=6.7$	18.0	9.20									
CN2	95.3 326	+P	04 36 33.0				-0.7		-----											
		PMZ	$m_b=6.1$				1.0		0.060	MAY 13d 04h 43m 46.4 ± 0.05s, SD2.44 / 14										
		PMZ	$m_B=6.1$		5.0		0.30	32.46 N ± 0.85km, 92.70 E ± 0.61km, h12 ± 0.20km												
		pP	04 36 41.0		0.0		Tibet (306)													
		PPMZ	$m_B=6.3$		5.0		0.50	$M_L 4.0 / 1, m_b 4.4 / 4,$												
		SKS	04 47 02.0		-3.8		LSA	3.1 206	Pn	04 44 40.0	4.4									
		eS	04 47 43.0		-2.8				Sg	04 45 23.4	1.0									
		eSS	04 54 15.0	-0.3	SMN	$M_L=4.0$			0.9	0.61										
		LN	$M_s=6.4$	18.0	6.50	SME				0.9	0.56									
		LE		18.0	2.00	CD2			9.5 96	eP	04 46 09.2	2.1								
LZ	$M_s=6.2$	20.0	8.00	TIY	17.0 67					eP	04 47 47.6	1.9								
XAN	96.5 310	eP	04 36 37.7							-1.2	QZN	20.4 127	eP	04 48 25.5	-0.7					
		PP	04 40 35.5							1.3			-----							
		PMZ	$m_B=6.4$							12.0			1.10	MAY 13d 08h 08m 38.1 ± 0.04s, SD2.10 / 60						
		LN	$M_s=6.5$							17.0			4.60	36.22 N ± 0.67km, 100.14 E ± 0.57km, h14 ± 0.10km						
		LE					18.0	6.10		Qinghai Province (325)										
		BJI	96.8 318				eP	04 36 39.5		-0.8			LZH	3.0 92	ePn	08 09 27.4	1.5			
							PMZ	$m_b=5.7$		1.2					0.023	Pg	08 09 31.5	0.3		
							PMZ	$m_B=6.3$		12.0					0.90	Sg	08 10 10.0	-2.3		
						ePP	04 40 36.0	-0.9	SMN	$M_L=4.7$					1.0	2.63				
				eSKS	04 47 12.0	-1.3	SME		1.0	3.81										
eS	04 47 57.0			-1.2	LN	$M_s=4.5$	5.0	3.62												
eSS	04 54 37.0			1.3	LE		5.0	3.60												
LN	$M_s=6.4$			20.0	6.90	GTA	3.2 356	Pn	08 09 33.0	4.6										
LZ	$M_s=6.3$			22.0	12.3			Pg	08 09 40.4	5.9										
TIY	97.1 314			+P	04 36 41.0			-0.7	CD2	6.1 149	ePn	08 10 13.0			4.7					
		PP	04 40 43.0	3.9	eSn			08 11 23.0			2.9									
		SKS	04 47 14.0	-0.8	SME			$M_L=3.9$			1.0	0.080								
		S	04 48 03.0	4.2	LN			$M_s=4.1$			8.0	1.48								
		LN	$M_s=6.3$	18.0	5.09			LZ			$M_s=4.0$	10.0	1.14							
		LZ	$M_s=6.2$	26.0	11.4			XAN			7.5 104	Pn	08 10 28.8	1.0						
		CD2	97.4 304	eP	04 36 42.0							-1.4	BTO	8.9 58	eP	08 10 47.5	-2.1			
				eSKS	04 47 15.0							-2.0			LN	$M_s=3.9$	12.0	0.60		
				LN	$M_s=6.6$	18.0	10.8					LE				12.0	0.30			
				LZ	$M_s=6.2$	20.0	7.72					TIY			10.0 78	eP	08 11 03.4	-0.7		
HHC	99.8 316			eP	04 36 53.8	-0.3	HHC		10.1 59	eP						08 11 04.1	-1.7			
				PP	04 40 58.0	-1.9				S						08 12 57.5	-1.7			
				SKS	04 47 30.0	1.1				LN						$M_s=4.3$	7.0	0.66		
				LN	$M_s=6.4$	17.0				5.16						LE		5.0	0.32	
				LE		16.0				1.18						GYA	11.2 148	P	08 11 21.6	0.1
				LZ	$M_s=6.2$	18.0		6.05		sP	08 11 33.0							3.3		
		BTO	100.4 315	eP	04 36 55.0	-2.0		WMQ		12.2 312	P		08 11 32.5	-1.8						
				PP	04 41 03.5	-1.6					S		08 13 47.5	-2.8						
				SKS	04 47 31.0	-1.1					LN		$M_s=4.3$	8.0				0.50		
				LN	$M_s=6.6$	17.0					5.10	LE		8.0	0.60					
LE				17.0	7.40	WHN	13.2 111		eP		08 11 47.9	0.5								
LZH	100.9 308			eP	04 36 58.5				-0.6		-----									
				PMZ	$m_B=6.1$				9.0		0.31									
				pP	04 37 08.0				1.9											
				PP	04 41 07.5				-1.1											
				SKS	04 47 33.0				-1.2											
		S	04 48 30.0	-0.8																
		sS	04 48 47.0	2.1																
		SS	04 55 30.0	-2.9																
		LN	$M_s=6.5$	17.0	7.47															







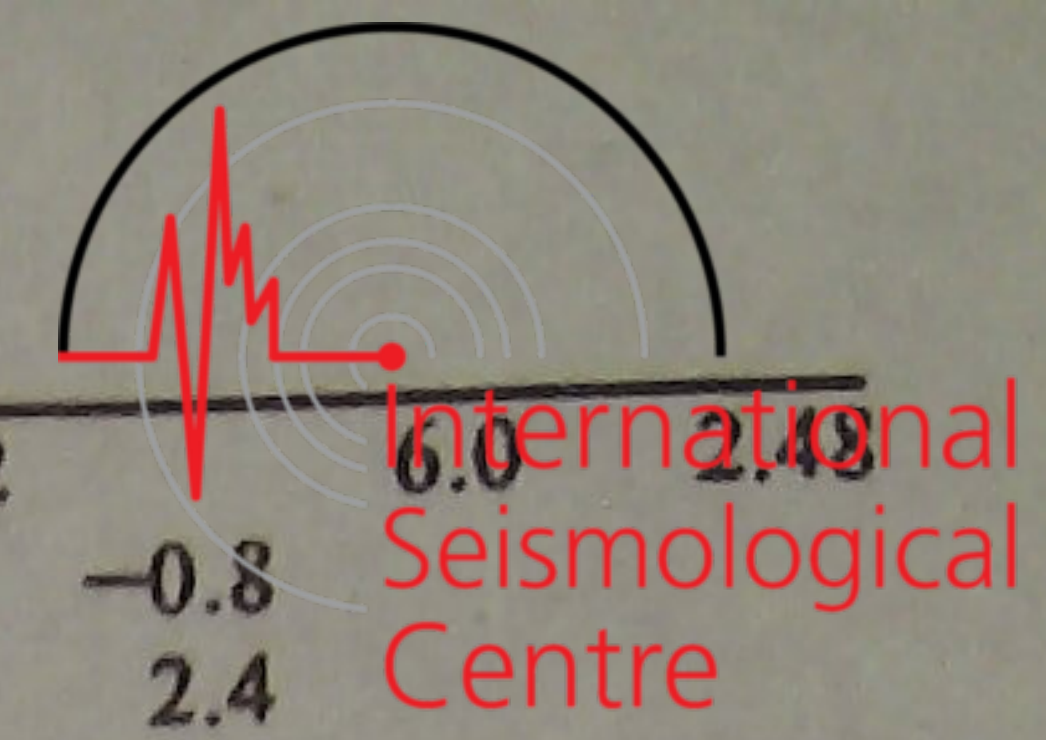


				PMZ		$m_b = 5.3$	1.5	0.033	TIY	88.1	313	+P	12 06 25.0	0.4	International Seismological Centre			
				LZ		$M_s = 5.2$	24.0	0.97	MAY 14d 21h 34m 03.8 ± 0.05s, SD1.20 / 348									
									35.90 S ± 0.64km, 71.53 W ± 1.24km, h76 ± 0.46km									
									Near coast of Central Chile (135)									
									$M_s 5.8 / 18, m_b 6.0 / 25, m_b 5.7 / 32$									
GTA	90.1	38	eP	07 05	12.8	-0.7			KSH	154.1	72	+PKP	21 53	48.0	0.5			
XAN	90.9	47	P	07 05	18.7	1.2						epPKP	21 54	10.0	2.0			
WHN	91.8	52	eP	07 05	21.3	-0.1						PP	21 57	43.0	-3.5			
TIY	95.5	46	eP	07 05	39.0	0.4						SKKS	22 04	25.0	-0.4			
			S	07 16	56.5	5.6						LN		$M_s = 6.4$	8.0	1.50		
			LN		$M_s = 5.6$		18.0	1.00				ePKP	21 53	55.0	-1.6			
			LZ		$M_s = 5.2$		20.0	0.75				PP	21 53	58.0	0.8			
NJ2	95.7	54	-P	07 05	40.2	1.0						PKP2	21 54	46.0	0.4			
			LZ		$M_s = 5.1$		20.0	0.61				PP	21 58	28.5	-1.8			
MAY 14d 09h 11m 13.5 ± 0.06s, SD2.19 / 42																		
36.14 N ± 0.58km, 100.23 E ± 0.63km, h14 ± 0.15km																		
Qinghai Province (325)																		
$M_s 4.3 / 21, M_L 4.3 / 8, m_b 3.9 / 4$																		
LZH	2.9	90	Pn	09 12	03.0	2.7						PPMZ		$m_b = 6.1$	10.0	1.80		
			Pg	09 12	07.0	1.8						LZ		$M_s = 6.0$	28.0	2.87		
			Sn	09 12	40.0	3.0						PKP	21 54	00.0	2.0			
			Sg	09 12	46.8	1.5						sPKP	21 54	25.0	-2.2			
			SMN		$M_L = 5.1$		1.5	7.45				PKP2	21 54	51.0	1.4			
			SME				1.5	6.96				PP	21 58	35.0	0.0			
GTA	3.3	354	Pg	09 12	10.6	-1.2						SKKS	22 05	12.0	-1.8			
			Sg	09 12	59.8	3.3						eSS	22 18	47.0	-4.3			
			SMN		$M_L = 3.9$		1.0	0.40				PKP	21 54	02.0	2.4			
			SME				1.0	0.40				PKP2	21 54	55.0	0.9			
			LE		$M_s = 4.1$		9.0	3.46				PPMZ		$m_b = 6.1$	4.5	0.83		
CD2	6.0	150	ePg	09 13	02.3	2.9						PP	21 58	41.0	-0.2			
			LN		$M_s = 4.3$		9.0	2.43				SKKS	22 05	19.0	0.0			
			LZ		$M_s = 4.2$		8.0	1.72				ePKP	21 53	58.5	-1.2			
XAN	7.4	104	Pn	09 13	02.2	0.2						pPKP	21 54	20.0	-0.3			
			Sn	09 14	26.0	-2.4						PP	21 58	45.0	1.0			
			Sg	09 15	05.2	-1.0						PPMZ		$m_b = 5.9$	5.0	0.70		
			SMN		$M_L = 4.6$		1.0	0.17				SS	22 19	11.0	2.6			
			SME				1.2	0.22				LZ		$M_s = 5.9$	24.0	1.80		
BTO	8.9	57	eP	09 13	26.0	1.2						ePKP	21 54	02.0	1.2			
			LN		$M_s = 4.0$		10.0	0.50				PP	21 58	53.0	2.7			
			LE				10.0	0.70				SKKS	22 05	28.0	-0.1			
TIY	9.9	77	eP	09 13	34.8	-4.0						PKP	21 54	02.0	0.8			
			LN		$M_s = 3.6$		12.0	0.28				PP	21 58	50.0	-2.9			
			LZ		$M_s = 4.2$		10.0	1.27				PPMZ		$m_b = 5.9$	6.0	0.81		
HHC	10.1	59	P	09 13	40.6	-0.4						SKKS	22 05	32.0	1.3			
			S	09 15	36.0	1.8						+iPKP	21 54	00.0	-1.4			
			LN		$M_s = 4.2$		8.0	0.49				pPKP	21 54	24.0	2.0			
			LE				8.0	0.62				PP	21 58	56.0	1.7			
			LZ		$M_s = 4.0$		15.0	1.16				PPMZ		$m_b = 6.0$	7.0	1.12		
GYA	11.1	149	P	09 13	54.4	-1.0						SKKS	22 05	34.0	1.9			
			pP	09 13	58.4	-2.2						SS	22 19	30.0	1.0			
			LN		$M_s = 4.3$		8.0	0.70				LZ		$M_s = 5.9$	32.0	2.93		
			LE				8.0	0.70				PKP	21 54	03.0	0.5			
KMI	11.2	168	eP	09 13	55.5	-0.9						pPKP	21 54	27.0	4.1			
WHN	13.1	111	eP	09 14	20.5	-1.1						PKP2	21 55	11.0	-0.6			
			LN		$M_s = 4.7$		9.0	1.59				PP	21 58	56.0	-5.2			
			LE				7.0	0.80				PPMZ		$m_b = 5.8$	6.0	0.60		
SSE	18.2	100	P	09 15	26.5	-0.8						SKKS	22 05	39.0	-0.1			
			PP	09 15	45.5	3.9						SS	22 19	40.0	-2.9			
			LE		$M_s = 4.2$		10.0	0.41				LZ		$M_s = 5.8$	27.0	2.10		
			LZ		$M_s = 4.1$		11.0	0.46				PKP	21 54	00.0	-2.3			
QZN	19.0	151	eP	09 15	37.0	-1.1						pPKP	21 54	26.0	3.1			
			eS	09 19	07.5	0.7						sPKP	21 54	36.0	4.5			
			LN		$M_s = 4.5$		12.0	0.43				PKP2	21 55	12.0	-0.3			
			LE				12.0	0.80				PP	21 59	00.0	-1.9			
MAY 14d 11h 54m 29.7 ± 0.03s, SD0.92 / 111																		
23.77 S ± 1.27km, 179.95 E ± 0.74km, h540 ± 0.32km																		
South of Fiji (171)																		
$m_b 5.0 / 21,$																		
CN2	83.8	324	+P	12 06	04.3	0.6						PPMZ			20.0	0.92		
												SKKS	22 05	41.0	1.2			
												SS	22 19	44.0	-0.3			
												LE		$M_s = 5.6$	11.0	0.35		
												LZ		$M_s = 5.7$	20.0	1.01		
												ePKP	21 54	02.0	-0.8			
												pPKP	21 54	25.0	1.6			



GYA	170.5	170	PPMZ	$m_B = 6.0$	7.0	1.19	XAN	178.1	192	SKKS	22 06 20.0	1.6	MAY 15d 05h 04m 13.7 ± 0.09s, SD4.80 / 7 40.92 N ± 0.98km, 76.75 E ± 0.48km, h22 ± 1.20km Kirgizliya-Xinjiang border region (320) $M_S 4.0 / 1, M_L 4.3 / 4,$								
			SS	22 19 54.0	2.1	LN				$M_S = 5.7$	19.0	1.14									
			LZ	$M_S = 5.7$	30.0	1.84				LZ	$M_S = 5.9$	14.0		1.90							
			iPKP	21 54 04.6	0.9	PKP				21 54 06.5	0.2										
			pPKP	21 54 28.0	3.8																
			PKP2	21 55 21.0	-0.6																
			PP	21 59 10.0	-2.5																
NJ2	170.6	249	PPMZ	$m_B = 6.3$	5.0	1.70	GTA	17.7	87	eP	05 08 22.0	1.1	MAY 15d 05h 07m 04.2 ± 0.05s, SD1.41 / 73 4.95 S ± 0.67km, 81.06 W ± 0.75km, h31 ± 0.33km Near coast of Northern Peru (109) $m_B 5.0 / 13,$								
			SKKS	22 05 51.0	0.7	WMQ				8.6 67 P	05 06 18.3	-2.1									
			LZ	$M_S = 5.9$	38.0	3.20				LE	$M_S = 4.0$	4.0		0.31							
			iPKP	21 54 04.0	0.4																
			PKP2	21 55 23.0	0.9																
			PP	21 59 13.0	0.1																
			SKKS	22 05 50.0	-0.8																
GTA	172.3	60	SS	22 20 02.0	-3.7		WMQ	140.0	13	ePKP	05 26 33.0	2.0	MAY 15d 14h 25m 20.1 ± 0.03s, SD1.03 / 548 36.09 N ± 0.93km, 70.42 E ± 0.45km, h112 ± 0.09km Hindu Kush region (718) $m_B 6.2 / 34, m_B 6.0 / 125,$								
			LZ	$M_S = 5.5$	26.0	1.02				TIA	144.7 334 ePKP	05 26 37.4		-1.5							
			+iPKP	21 54 05.2	0.3					TIY	145.1 341 ePKP	05 26 38.0		-1.8							
			pPKP	21 54 27.8	2.5					GTA	145.7 359 +PKP	05 26 41.0		0.2							
			PKP2	21 55 30.9	1.2					SSE	146.6 324 PKP	05 26 44.2		1.9							
			SKKS	22 05 58.0	-1.5					NJ2	147.2 328 PKP	05 26 43.0		-0.2							
			SS	22 20 20.0	-2.7					LZH	148.7 352 ePKP	05 26 47.5		1.7							
BJI	172.6	306	LZ	$M_S = 6.0$	34.0	4.21				pPKP	05 26 55.0	0.4	MAY 15d 14h 25m 20.1 ± 0.03s, SD1.03 / 548 36.09 N ± 0.93km, 70.42 E ± 0.45km, h112 ± 0.09km Hindu Kush region (718) $m_B 6.2 / 34, m_B 6.0 / 125,$								
			PKP	21 54 04.5	-0.1		XAN	149.6 343 PKP	05 26 52.0	4.8											
			pPKP	21 54 28.0	2.9		WHN	150.7 332 ePKP	05 26 47.4	-1.3											
			ePP	21 59 28.0	4.7						pPKP	05 26 55.5		-2.4							
			LZ	$M_S = 5.7$	40.0	2.79															
			PKP	21 54 05.5	0.8																
			pPKP	21 54 30.0	4.7																
WHN	172.7	224	PKP2	21 55 33.0	1.4		KSH	5.5	50	P	14 26 44.0	2.2	MAY 15d 14h 25m 20.1 ± 0.03s, SD1.03 / 548 36.09 N ± 0.93km, 70.42 E ± 0.45km, h112 ± 0.09km Hindu Kush region (718) $m_B 6.2 / 34, m_B 6.0 / 125,$								
			SKKS	22 06 02.0	0.5					WMQ	15.3 55 +iP	14 28 50.0		-1.7							
			LZ	$M_S = 5.7$	20.0	1.26									PMZ	$m_B = 5.9$	5.5	2.69			
			PKP	21 54 04.9	-0.1										PP	14 29 06.0	-1.5				
			pPKP	21 54 28.0	2.3										S	14 31 34.0	-3.9				
			PPMZ		20.0	1.84									PcP	14 33 48.0	-2.1				
			SKKS	22 06 03.0	0.2										LN		5.0	11.5			
TIA	173.0	275	LZ	$M_S = 5.7$	40.0	2.77				LSA	18.5 104 +iP	14 29 30.0	-1.0	MAY 15d 14h 25m 20.1 ± 0.03s, SD1.03 / 548 36.09 N ± 0.93km, 70.42 E ± 0.45km, h112 ± 0.09km Hindu Kush region (718) $m_B 6.2 / 34, m_B 6.0 / 125,$							
			+PKP	21 54 05.4	-1.5								PMZ		$m_B = 6.2$	2.0	2.35				
			pPKP	21 54 28.0	0.2										sP	14 30 03.0	-1.0				
			PKP2	21 55 34.0	-1.8										iS	14 32 49.5	-1.7				
			iPP	21 59 25.0	-3.4										GTA	23.4 73 +iP	14 30 22.6	2.3			
			PPMZ	$m_B = 6.3$	5.0	1.61										sP	14 30 59.9	2.6			
			SKKS	22 06 05.0	-2.0											sS	14 35 07.5	5.2			
CD2	173.7	140	LZ	$M_S = 5.7$	40.0	2.77															
			+PKP	21 54 05.4	-1.5																
			pPKP	21 54 28.0	0.2																
			PKP2	21 55 34.0	-1.8																
			iPP	21 59 25.0	-3.4																
			PPMZ	$m_B = 6.3$	5.0	1.61															
			SKKS	22 06 05.0	-2.0																
HHC	174.5	335	LZ	$M_S = 5.8$	26.0	2.14															
			PKP	21 54 06.0	-1.0																
			pPKP	21 54 30.0	3.1																
			PP	21 59 32.0	-0.6																
			PPMZ	$m_B = 6.0$	8.0	1.31															
			SKKS	22 06 10.0	-0.6																
			LN	$M_S = 5.9$	20.0	1.30															
BTO	175.2	346	LE		24.0	1.50															
			LZ	$M_S = 5.9$	40.0	5.03															
			iPKP	21 54 06.0	0.3																
			pPKP	21 54 30.0	3.7																
			PP	21 59 37.0	1.1																
			SKKS	22 06 13.0	0.4																
			SS	22 20 50.0	-0.2																
LZH	176.2	86	-iPKP	21 54 07.0	0.8																
			pPKP	21 54 29.0	2.3																
			sPKP	21 54 40.0	4.9																
			PKP2	21 55 48.0	0.8																
			PP	21 59 39.5	-1.7																
			PPMZ	$m_B = 6.5$	7.0	4.27															
			SKKS	22 06 18.0	0.0																
TIY	176.3	301	SS	22 20 56.0	-4.0																
			LN	$M_S = 5.8$	24.0	1.70															
			PKP	21 54 06.0	-0.1																
			pPKP	21 54 29.0	2.3																
			PPMZ	$m_B = 6.0$	7.0	1.25															





Station	Mag	Depth	Type	Time	Mag	Depth	Type	Time	Mag	Depth	Type	Time	Mag	Depth	Type	Time			
KMI	29.8	102	LN		12.5	7.48			PMZ	$m_B = 6.2$									
			-P	14 31 18.5	-0.3			sP	14 33 02.0	-0.8									
			PMZ		$m_b = 5.8$	2.5	0.50	PP	14 33 56.0	2.4									
			PMZ		$m_B = 6.0$	4.0	1.30	S	14 38 06.5	3.2									
BTO	31.2	70	sP	14 31 52.5	-3.9			sS	14 38 52.0	4.0									
			iS	14 36 07.0	1.0			+P	14 32 34.0	0.1									
			+iP	14 31 32.0	0.7			sP	14 33 12.0	-0.3									
			PMZ			3.0	3.10	PP	14 34 07.0	0.1									
			sP	14 32 10.0	0.8			PcP	14 34 46.0	1.7									
			iS	14 36 31.5	3.1			S	14 38 21.0	0.5									
			sS	14 37 16.0	4.9			SMN			9.0	1.83							
XAN	31.4	82	LN		7.0	7.10	SME			10.0	4.40								
			LE		7.0	4.20	sS	14 39 08.0	2.7										
			+P	14 31 33.1	-0.3			SS	14 41 06.0	-1.0									
			sP	14 32 09.0	-2.4			+P	14 32 40.0	0.8									
			PP	14 32 42.5	1.8			PMZ		$m_b = 6.0$	1.2	0.32							
			S	14 36 34.0	2.8			PMZ		$m_B = 6.3$	5.0	2.48							
			SMN			5.0	3.60	sP	14 33 20.0	2.2									
			SME			5.0	2.60	PcP	14 34 49.0	2.7									
			sS	14 37 16.0	1.0			iS	14 38 32.5	1.3									
			LN			9.0	4.15	LN			14.0	3.06							
GYA	32.3	97	LE		8.0	1.45	LE			11.0	1.31								
			+iP	14 31 41.0	0.3			+iP	14 32 46.5	0.7									
			PMZ		$m_b = 6.1$	1.2	0.40	PMZ		$m_b = 6.0$	0.9	0.22							
			PMZ		$m_B = 6.5$	2.0	1.60	PMZ		$m_B = 6.1$	6.0	2.17							
			sP	14 32 21.0	2.3			sP	14 33 25.5	1.1									
			PP	14 32 49.0	-2.2			PP	14 34 23.0	0.3									
			S	14 36 44.0	-0.2			S	14 38 44.0	1.9									
			sS	14 37 33.0	4.9			sS	14 39 30.0	3.0									
			LN			12.0	3.70	+iP	14 32 49.0	0.8									
			LE			12.0	2.90	PMZ		$m_b = 6.5$	1.0	0.79							
HHC	32.3	69	LZ		16.0	2.10	PMZ		$m_B = 6.5$	4.0	3.24								
			+P	14 31 42.1	0.8			sP	14 33 26.5	-0.3									
			PMZ		$m_b = 6.4$	1.4	0.91	iS	14 38 49.0	1.6									
			PMZ		$m_B = 6.3$	4.0	2.40	SMN			6.0	3.33							
			sP	14 32 19.5	0.2			SME			5.0	2.24							
			PP	14 32 53.0	0.9			LE			12.0	2.01							
			S	14 36 50.0	4.7			LZ			19.0	1.91							
			SMN			7.0	1.80	+iP	14 32 55.0	-0.5									
			LN			7.0	1.30	PMZ		$m_b = 5.8$	0.8	0.13							
			LE			6.0	2.30	PMZ		$m_B = 6.2$	5.0	2.13							
TIY	33.4	74	LE		8.0	1.20	sP	14 33 33.0	-1.1										
			+iP	14 31 50.9	0.2			PP	14 34 36.0	1.5									
			PMZ		$m_b = 6.1$	1.9	0.65	iS	14 39 00.0	-0.5									
			sP	14 32 28.0	-0.8			SMN			10.0	1.58							
			iS	14 37 05.0	1.8			SME			5.0	1.19							
			sS	14 37 50.0	3.8			sS	14 39 44.0	-0.7									
			+P	14 32 13.0	1.1			SS	14 42 04.0	0.9									
BJI	35.9	70	PMZ		$m_b = 6.1$	1.4	0.50	ScS	14 42 43.0	-2.2									
			PMZ		$m_B = 6.0$	6.0	1.62	-P	14 33 04.5	0.7									
			sP	14 32 51.0	0.7			PMZ		$m_b = 6.1$	1.2	0.41							
			PP	14 33 36.0	1.0			PMZ		$m_B = 6.5$	4.0	3.22							
			eS	14 37 42.0	0.4			pP	14 33 30.0	0.8									
			ScP	14 38 09.5	-1.2			sP	14 33 44.0	1.6									
			esS	14 38 28.0	3.0			PP	14 34 48.0	2.5									
			LN			7.0	2.61	S	14 39 14.0	-0.5									
			LE			8.0	3.57	sS	14 40 02.0	2.3									
			LZ			18.0	22.4	ScS	14 42 50.0	-1.3									
WHN	36.9	86	+iP	14 32 21.0	1.1			LN			12.0	1.12							
			PMZ		$m_b = 6.1$	1.2	0.40	LZ			20.0	1.87							
			PMZ		$m_B = 6.4$	4.0	2.46	+iP	14 33 04.0	0.1									
			sP	14 33 00.0	1.7			PMZ		$m_b = 5.9$	1.0	0.20							
			iS	14 37 58.0	2.0			PMZ		$m_B = 6.1$	5.0	1.70							
			LN			12.0	4.33	sP	14 33 44.0	1.4									
			LE			9.0	11.7	S	14 39 18.0	3.2									
TIA	37.4	76	LZ		24.0	2.73	sS	14 40 01.0	1.0										
			+P	14 32 25.3	0.9			cSS	14 42 20.0	-1.9									
			PMZ		$m_b = 6.4$	1.6	1.04	ScS	14 42 50.0	-1.4									







1.18 N ± 0.63km, 123.88 E ± 0.86km, h28 ± 0.02km Minahassa Peninsula (Celebes) (265) M <sub>s</sub> 5.7 / 59, m <sub>b</sub> 6.0 / 26, m <sub>b</sub> 5.6 / 57								
QZN	22.4 323	-P	18 36 37.5	-0.2				
		sP	18 36 50.0	0.3				
		PP	18 37 08.5	3.7				
		S	18 40 38.0	0.9				
		SMN			12.0	10.6		
		SME			11.0	15.6		
		SS	18 41 22.0	3.3				
		LN	M <sub>s</sub> =5.7		15.5	16.2		
		LE			15.0	4.30		
		GZH	24.1 336	-P	18 36 54.0	0.6		
		PMZ	m <sub>b</sub> =5.6		1.2	0.32		
		PMZ	m <sub>b</sub> =6.2		6.0	6.03		
		S	18 41 08.0	2.5				
		LN	M <sub>s</sub> =5.8		14.0	12.4		
		LE			13.0	8.66		
		LZ	M <sub>s</sub> =5.7		18.0	22.3		
QZH	24.2 348	-iP	18 36 55.0	0.5				
		PMZ	m <sub>b</sub> =6.1		6.0	5.00		
		PMZ	m <sub>b</sub> =5.8		2.0	0.83		
		S	18 41 12.0	4.6				
		LE	M <sub>s</sub> =5.3		16.0	6.05		
		LZ	M <sub>s</sub> =5.4		22.0	14.3		
		SSE	29.9 355	eP	18 37 47.0	0.1		
		S	18 42 40.9	0.7				
		SS	18 44 20.0	3.3				
		LN	M <sub>s</sub> =5.3		15.0	3.52		
		LE			15.0	2.30		
		LZ	M <sub>s</sub> =5.3		20.0	7.41		
		GYA	30.1 328	-P	18 37 50.0	0.8		
		PMZ	m <sub>b</sub> =6.1		5.0	1.60		
		pP	18 38 00.0	2.5				
		PP	18 38 46.0	-1.0				
		S	18 42 42.0	-2.0				
		ScS	18 48 25.0	2.2				
		LN	M <sub>s</sub> =5.8		16.0	10.0		
		LE			16.0	10.2		
		LZ	M <sub>s</sub> =5.5		18.0	9.60		
		WHN	30.6 344	P	18 37 53.5	0.3		
				PMZ	m <sub>b</sub> =5.6		1.2	0.12
PMZ	m <sub>b</sub> =6.0				6.0	1.46		
sP	18 38 06.0			0.7				
S	18 42 54.0			2.6				
LN	M <sub>s</sub> =5.8				15.0	10.9		
LE					16.0	7.03		
LZ	M <sub>s</sub> =5.5				20.0	10.7		
NJ2	31.1 352			-P	18 37 58.0	0.4		
		PMZ	m <sub>b</sub> =5.9		6.5	1.33		
		S	18 43 00.0	0.8				
		LN	M <sub>s</sub> =5.5		15.0	5.64		
		LE			13.0	2.44		
		LZ	M <sub>s</sub> =5.2		18.0	4.77		
		KMI	31.4 321	-P	18 38 01.5	0.9		
		PMZ	m <sub>b</sub> =5.8		2.5	0.40		
		PMZ	m <sub>b</sub> =6.2		5.0	1.90		
		pP	18 38 10.5	1.9				
		iS	18 43 10.0	4.7				
		LN	M <sub>s</sub> =5.6		14.0	2.80		
		LE			16.0	6.80		
		LZ	M <sub>s</sub> =5.7		18.0	14.2		
		CD2	35.2 329	-iP	18 38 33.2	-0.2		
		PMZ	m <sub>b</sub> =5.7		0.9	0.11		
		PMZ	m <sub>b</sub> =6.1		4.0	1.50		
		iS	18 44 03.5	-0.8				
		LN	M <sub>s</sub> =5.8		15.0	9.45		
		LZ	M <sub>s</sub> =5.4		28.0	9.00		
		TIA	35.4 351	P	18 38 34.0	-1.3		
		S	18 44 06.5	-0.3				
		LN	M <sub>s</sub> =5.4		12.0	2.90		
		LZ	M <sub>s</sub> =5.4		40.0	12.0		
		XAN	35.6 338	-P	18 38 36.0	-0.6		
				PMZ	m <sub>b</sub> =5.9		6.0	1.41
				S	18 44 05.0	-4.1		
				SMN			1.0	0.016
				SME			1.0	0.018
				LN	M <sub>s</sub> =6.0		16.0	15.4
				LE			14.0	5.21
DL2	37.6 357			eP	18 38 53.0	-0.7		
				PMZ	m <sub>b</sub> =5.9		6.0	1.31
		eS	18 44 40.0	-1.3				
		SMN			27.0	8.62		
		LN	M <sub>s</sub> =5.6		14.0	4.55		
		LZ	M <sub>s</sub> =5.2		20.0	4.23		
		TIY	37.8 345	eP	18 38 55.0	-1.0		
				sP	18 39 13.0	5.0		
				S	18 44 46.0	1.8		
		LN	M <sub>s</sub> =5.9		16.0	10.9		
		LZ	M <sub>s</sub> =5.7		22.0	11.7		
		BJI	39.3 351	eP	18 39 07.0	-1.0		
				PMZ	m <sub>b</sub> =5.6		1.5	0.14
				PMZ	m <sub>b</sub> =5.8		5.0	0.81
				ePP	18 40 40.0	-2.3		
eS	18 45 07.0			-0.2				
LN	M <sub>s</sub> =5.4				16.0	3.62		
LZ	M <sub>s</sub> =5.5				32.0	10.6		
LZH	39.4 334			-iP	18 39 10.0	1.1		
				PMZ	m <sub>b</sub> =6.1		2.0	0.70
		PMZ	m <sub>b</sub> =6.1		6.0	2.04		
		pP	18 39 17.5	0.3				
		sP	18 39 22.5	1.5				
		PP	18 40 40.0	-3.3				
		S	18 45 08.0	0.4				
		SMN			14.0	7.35		
		eSS	18 47 54.0	-0.7				
		LN	M <sub>s</sub> =5.7		14.0	4.26		
		LE			14.0	4.13		
		LZ	M <sub>s</sub> =5.8		20.0	14.6		
		SNY	40.5 360	-iP	18 39 16.0	-1.6		
		PMZ	m <sub>b</sub> =5.1		1.5	0.050		
		PMZ	m <sub>b</sub> =5.7		6.5	0.80		
		sP	18 39 28.5	-1.3				
		PP	18 40 54.0	-0.6				
		S	18 45 20.0	-3.6				
		SMN			17.0	1.47		
		LN	M <sub>s</sub> =5.7		16.0	3.37		
		LE			16.0	6.26		
HHC	41.0 346	-P	18 39 22.0	-0.4				
		sP	18 39 36.0	1.4				
		PP	18 41 03.0	2.9				
		S	18 45 34.0	2.0				
		SMN			16.0	7.80		
		SME			9.0	1.70		
		LN	M <sub>s</sub> =5.8		15.0	6.10		
BTO	41.2 344	-iP	18 39 23.5	-0.3				
		PP	18 41 05.0	3.1				
		S	18 45 38.0	3.4				
		LN	M <sub>s</sub> =5.9		15.0	7.60		
		LE			14.0	6.40		
		LSA	42.1 315	-P	18 39 32.0	0.4		
				sP	18 39 45.0	1.6		
S	18 45 50.0			2.0				
LE					14.0	1.41		
M <sub>s</sub> =5.1								



















37.09 N ± 0.67km, 136.91 E ± 0.50km, h267 ± 0.22km Near west coast of Honshu m <sub>b</sub> 5.6/12, m <sub>b</sub> 5.3/120, (226)								
MDJ	9.3 326	+iP	01 06 20.2	2.4				
		PMZ		m <sub>b</sub> = 5.6	1.2	0.60		
		sP	01 07 18.5	2.5				
		S	01 08 06.0	5.5				
		ScP	01 15 18.0	1.6				
		SMN		8.0	5.40			
		ScS	01 18 52.5	3.0				
CN2	11.0 311	eP	01 06 39.2	0.4				
		PMZ		m <sub>b</sub> = 5.2	1.0	0.20		
		PMZ		m <sub>b</sub> = 5.0	4.0	0.50		
		sP	01 07 40.0	0.9				
		S	01 08 40.0	1.9				
		SMN		6.0	2.70			
		SME		6.0	4.60			
SNY	11.3 299	PcP	01 12 12.5	-0.2				
		ScS	01 18 52.0	-0.6				
		-iP	01 06 45.4	2.5				
		PMZ		m <sub>b</sub> = 5.7	1.2	0.65		
		PMZ			3.0	2.56		
		sP	01 07 48.5	4.7				
		iS	01 08 53.0	7.0				
DL2	12.2 283	SMN		9.0	4.28			
		SME		6.0	3.32			
		-iP	01 06 56.0	2.4				
		PMZ		m <sub>b</sub> = 5.4	1.2	0.35		
		PMZ		m <sub>b</sub> = 5.9	5.0	4.67		
		sP	01 07 56.0	0.5				
		S	01 09 08.0	3.1				
SSE	14.3 250	SMN		8.0	2.73			
		SME		4.0	1.49			
		LN		8.0	0.44			
		LE		8.0	1.84			
		LZ		16.0	1.08			
		+P	01 07 21.0	1.3				
		PMZ		m <sub>b</sub> = 5.9	1.0	0.79		
NJ2	15.7 257	S	01 09 53.0	0.8				
		LN		12.0	0.56			
		LZ		16.0	1.32			
		-iP	01 07 36.0	0.2				
		PMZ		m <sub>b</sub> = 5.7	1.0	0.44		
		PMZ		m <sub>b</sub> = 5.8	3.5	1.81		
		sP	01 08 43.0	0.7				
TIA	15.9 273	S	01 10 25.0	2.6				
		-P	01 07 38.0	-0.3				
		eS	01 10 28.5	0.9				
		LN		8.0	2.16			
		eP	01 07 44.0	-0.6				
		PMZ		m <sub>b</sub> = 5.7	1.5	0.64		
		PMZ			3.0	1.62		
BJI	16.5 287	eS	01 10 40.0	0.7				
		eScP	01 15 30.0	2.4				
		ePcS	01 15 54.0	-0.2				
		eScS	01 19 08.0	2.1				
		-iP	01 08 14.4	-0.9				
		PMZ		m <sub>b</sub> = 5.3	1.2	0.17		
		S	01 11 38.0	2.6				
QZH	19.8 237	LE		10.0	0.81			
		-P	01 08 18.0	-0.7				
		iS	01 11 44.0	1.8				
		-P	01 08 19.0	0.0				
		PMZ		m <sub>b</sub> = 5.4	1.0	0.18		
		PMZ		m <sub>b</sub> = 5.7	4.0	1.46		
		S	01 11 48.0	5.7				
WHN	19.8 257	LN		6.0	0.70			
		LE		9.0	1.01			
		HHC	20.0 289	-P	01 08 20.0	-1.3		
		S			01 11 48.0	1.9		
		LN				10.0	0.34	
		LE				7.0	0.47	
		LZ				14.0	1.65	
BTO	21.2 288	-iP	01 08 31.5	-1.3				
		S	01 12 09.0	2.3				
		PcP	01 12 27.0	-1.2				
		LN			10.0	0.90		
		LE			10.0	0.80		
		XAN	22.9 271	-iP	01 08 48.5	-0.9		
		PMZ		m <sub>b</sub> = 5.6	5.0	1.30		
GZH	24.6 242	sP	01 10 13.1	3.7				
		S	01 12 38.0	1.7				
		LN			10.0	0.60		
		LE			7.0	0.40		
		-iP	01 09 06.3	1.3				
		PMZ		m <sub>b</sub> = 5.8	1.0	0.36		
		S	01 13 07.0	2.7				
LZH	26.5 278	-P	01 09 21.4	-0.9				
		PMZ		m <sub>b</sub> = 5.6	2.0	0.40		
		PMZ		m <sub>b</sub> = 5.0	10.0	0.53		
		pP	01 10 14.0	1.4				
		sP	01 10 45.0	0.9				
		PcP	01 12 39.0	-0.4				
		eS	01 13 34.0	-1.7				
GYA	27.7 256	ScS	01 19 42.5	0.6				
		LZ			18.0	1.00		
		-P	01 09 32.0	-1.2				
		PMZ		m <sub>b</sub> = 5.7	1.2	0.30		
		PP	01 10 39.0	2.2				
		PcP	01 12 42.8	0.5				
		S	01 13 52.8	-1.0				
CD2	28.1 267	ScP	01 15 58.8	2.8				
		PcS	01 16 24.0	1.2				
		ScS	01 19 50.0	2.7				
		LN			12.0	0.80		
		LE			12.0	0.70		
		P	01 09 35.0	-1.4				
		PMZ		m <sub>b</sub> = 5.5	0.8	0.11		
GTA	29.1 286	pP	01 10 30.0	2.3				
		LN			12.0	1.10		
		-iP	01 09 44.2	-1.3				
		PP	01 10 55.0	1.7				
		PcP	01 12 46.8	1.0				
		ScP	01 16 03.4	3.1				
		S	01 14 13.0	-2.8				
QZN	29.7 240	SS	01 16 16.0	2.9				
		ScS	01 19 56.0	2.3				
		-P	01 09 52.0	0.9				
		PMZ		m <sub>b</sub> = 5.2	0.8	0.060		
		eS	01 14 28.0	1.1				
		LN			12.0	0.65		
		LE			10.0	0.64		
KMI	31.4 258	-P	01 10 05.0	-0.8				
		PMZ		m <sub>b</sub> = 5.7	1.0	0.25		
		PP	01 11 23.0	2.0				
		LZ			14.0	1.80		
		-iP	01 10 58.0	0.0				
		pP	01 11 55.8	4.1				
		PP	01 12 36.5	4.7				
WMQ	37.6 296	S	01 16 26.0	-0.5				
		SMN			6.0	0.47		
		SS	01 19 12.0	-2.0				
		ScS	01 20 39.0	0.9				
		LN			9.0	0.63		
		P	01 11 07.0	0.1				
		P	01 12 16.5	1.8				
LSA	38.6 273	P	01 11 07.0	0.1				
		P	01 12 16.5	1.8				
KSH	47.1 293	P	01 11 07.0	0.1				
		P	01 12 16.5	1.8				







			S	13 31 38.0	5.6				SMN			12.0	0.85						
			LN			6.0	3.32		SME			14.0	0.59						
			LE			9.0	1.89		sS	13 34 33.0	-0.1								
			LZ			20.0	1.87		LN			7.0	2.08						
GYA	29.6	104	-P	13 27 03.8	-0.1				LE			10.0	0.77						
			pP	13 27 30.0	2.0				LZ			20.0	1.45						
			S	13 31 52.0	3.1			CN2	38.3	65	P	13 28 19.0	0.7						
			ScS	13 37 30.4	1.4				PMZ		$m_b=4.9$	1.0	0.020						
			LN			16.0	3.10		pP	13 28 44.0	0.5								
			LE			16.0	1.10		sP	13 28 58.0	1.1								
TIY	29.8	80	-P	13 27 05.6	0.0				PP	13 29 51.0	0.7								
			pP	13 27 31.5	1.7				PcP	13 30 30.0	0.0								
			sP	13 27 48.0	4.6				S	13 34 04.0	0.8								
			S	13 31 54.0	2.0				LN			6.0	0.70						
			LN			7.5	2.44		LE			6.0	1.00						
			LZ			15.0	2.13		LZ			8.0	2.10						
BJI	32.2	74	eP	13 27 27.0	0.8			SSE	38.8	86	eP	13 28 22.5	0.2						
			PMZ	$m_b=5.2$		1.0	0.042		PMZ		$m_b=5.6$	1.0	0.097						
			epP	13 27 53.0	2.2				pP	13 28 49.5	1.9								
			esP	13 28 04.0	-0.4				sP	13 29 00.0	-0.9								
			PcP	13 30 14.0	1.9				sP	13 29 00.0	-0.9								
			eS	13 32 31.0	1.0				PP	13 29 56.2	0.0								
			esS	13 33 14.0	0.9				PcP	13 30 34.0	2.4								
			eScP	13 33 45.0	1.1				S	13 34 11.0	0.4								
			LN			5.0	1.87		LN			11.0	1.01						
			LZ			12.0	1.51		LE			11.0	0.66						
WHN	33.7	91	-P	13 27 40.0	0.9			QZH	39.6	97	eP	13 28 29.0	0.1						
			PMZ	$m_b=5.4$		1.2	0.070		PMZ		$m_b=5.7$	0.8	0.10						
			pP	13 28 06.0	2.2				pP	13 28 56.0	1.8								
			S	13 32 56.0	3.8				S	13 34 24.0	1.5								
			LN			8.0	1.62		sS	13 35 08.0	0.5								
			LE			10.0	1.05		-P	13 28 41.5	0.3								
TIA	33.8	80	-P	13 27 41.2	0.7			MDJ	41.1	63	PMZ	$m_b=6.1$	2.0	0.60					
			pP	13 28 07.4	2.1				pP	13 29 09.0	2.5								
			eS	13 32 58.3	2.7				sP	13 29 20.0	0.1								
			LN			7.0	1.39		sS	13 35 30.0	0.2								
			LE			7.0	0.92		LN			14.0	4.80						
QZN	36.3	112	eP	13 28 02.5	0.6			<p>MAY 17d 15h 59m <math>55.8 \pm 0.05s</math>, SD1.01 / 282  <math>25.35 S \pm 0.77km</math>, <math>178.13 E \pm 0.73km</math>, <math>h609 \pm 0.81km</math>                      South of Fiji (171)  <math>m_b 5.6 / 6</math>, <math>m_b 5.7 / 77</math>,</p>											
			eS	13 33 33.5	-0.8									QZH	76.2	306	-P	16 10 45.0	-0.1
			sS	13 34 21.0	3.1										PMZ		$m_b=5.6$	1.2	0.36
			LN			11.0	1.57								iS	16 19 41.0	-1.4		
			LE			11.0	1.50								ScS	16 20 04.0	1.6		
GZH	36.5	103	P	13 28 01.5	-1.9									SSE	78.2	313	-P	16 10 55.0	-0.6
			S	13 33 34.0	-2.2										sP	16 14 05.5	3.8		
			LN			12.0	1.75								S	16 20 00.0	-1.3		
DL2	36.5	74	eP	13 28 04.5	1.0										sS	16 23 44.0	0.4		
			pP	13 28 30.0	1.4										SS	16 25 20.0	-5.0		
			sP	13 28 40.0	-2.0			QZN	79.7	297	eP	16 11 03.5	-0.1						
			PP	13 29 31.0	1.7				pP	16 13 12.0	1.8								
			S	13 33 38.0	1.6				eS	16 20 17.5	-0.8								
			SMN			7.0	0.82		-iP	16 11 06.5	-0.4								
			SME			4.0	0.74		PMZ		$m_b=5.2$	1.1	0.11						
			LE			8.0	1.14		PMZ		$m_b=5.6$	3.5	0.80						
			LZ			10.0	0.70		sP	16 14 17.0	3.5								
NJ2	36.6	86	-P	13 28 04.0	0.1				S	16 20 24.0	0.9								
			pP	13 28 31.0	1.9			NJ2	80.4	312	-iP	16 11 18.0	0.0						
			S	13 33 41.0	3.9				PMZ		$m_b=5.5$	1.2	0.20						
			ScP	13 34 01.4	1.8				S	16 20 50.0	5.2								
			sS	13 34 24.0	2.3				+iP	16 11 19.0	0.9								
			LN			11.0	1.39		PMZ		$m_b=5.5$	1.5	0.25						
			LE			7.0	0.77		-P	16 11 18.0	-1.9								
			LZ			12.0	0.91		PMZ		$m_b=5.3$	5.0	0.51						
SNY	37.3	69	-P	13 28 10.4	0.3			MDJ	82.5	327	-iP	16 11 23.0	-0.9						
			PMZ	$m_b=5.5$		1.2	0.10		WHN	82.6	309								
			pP	13 28 34.0	-1.3				DL2	82.9	319								
			sP	13 28 48.0	-0.6				SNY	83.7	322								
			PP	13 29 38.5	-0.5														
			eS	13 33 50.0	0.8														



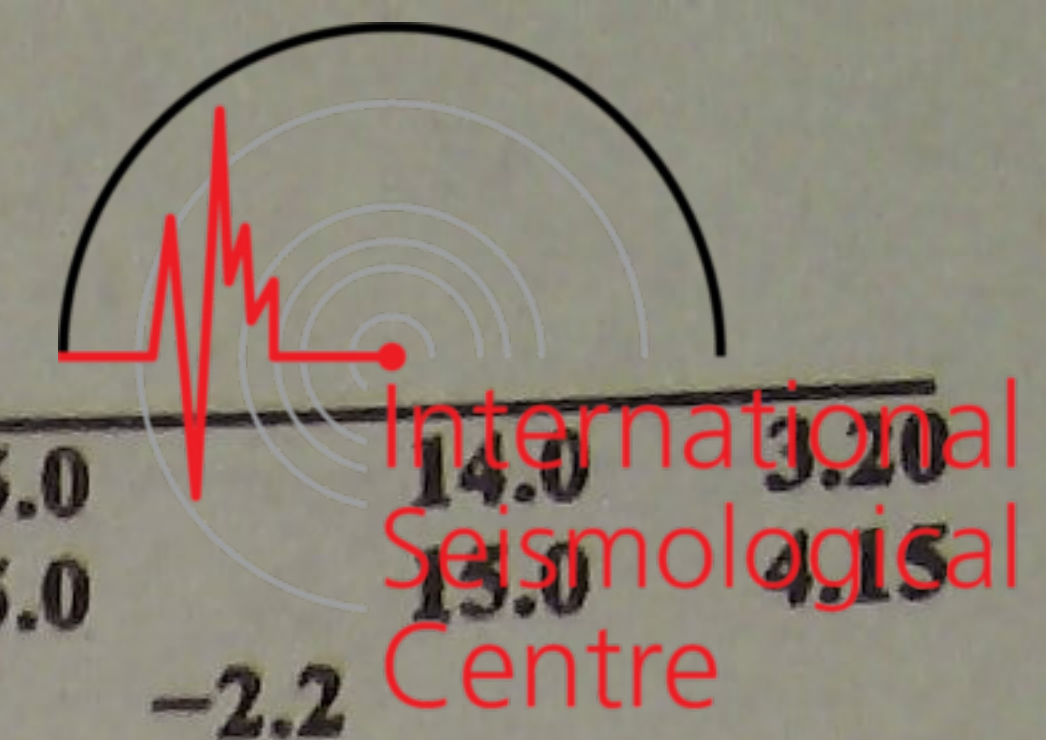


		sP	16 14 28.0	-3.5				NJ2	9.6 307	+P	23 30 20.0	1.6	
		SMN			22.0	1.37				S	23 32 11.0	5.0	
		SME			14.0	0.53				LN	$M_s = 5.5$		9.0 12.6
TIA	84.0 315	-P	16 11 25.5	0.2						LE			10.0 19.1
CN2	84.1 325	-iP	16 11 25.0	-0.5						LZ	$M_s = 5.3$		12.0 17.9
		PMZ	$m_b = 5.8$		1.0	0.30		WHN	12.6 291	+P	23 31 01.0	2.3	
		PMZ	$m_b = 5.8$		4.0	1.20				PMZ	$m_b = 6.1$		1.4 0.49
		pP	16 13 37.0	3.3						sP	23 31 14.0	3.3	
		sP	16 14 36.0	2.8						S	23 33 21.0	2.9	
		SKS	16 20 48.0	-1.0						LE	$M_s = 5.3$		6.0 6.10
		S	16 20 57.0	-2.3						LZ	$M_s = 5.0$		18.0 10.9
		SMN			5.0	0.70		TIA	13.3 319	+P	23 31 11.4	2.9	
		SME			5.0	0.60				sP	23 31 21.4	1.0	
GYA	86.0 302	P	16 11 35.2	0.0						LN	$M_s = 5.3$		12.0 5.15
		SKS	16 21 04.8	2.8						LE			12.0 8.40
BJI	86.9 317	eP	16 11 39.0	-0.2						LZ	$M_s = 5.2$		18.0 14.4
		PMZ	$m_b = 5.7$		1.7	0.25		DL2	13.4 338	+iP	23 31 12.0	2.6	
		PMZ	$m_b = 5.8$		4.0	0.73				PMZ	$m_b = 6.3$		1.5 0.89
		esP	16 14 48.0	0.4						S	23 33 44.0	6.8	
		eSKS	16 21 06.0	-1.6						LN	$M_s = 5.3$		12.0 3.40
		eS	16 21 26.0	-1.7						LE			14.0 10.1
TIY	87.9 314	-P	16 11 44.2	0.1						LZ	$M_s = 5.0$		20.0 9.96
		PMZ	$m_b = 5.8$		1.2	0.19		SNY	15.6 348	+iP	23 31 40.0	1.3	
		SKS	16 21 13.5	-0.4						PMZ	$m_b = 5.7$		1.4 0.53
		S	16 21 40.5	5.2						PMZ	$m_b = 5.9$		7.0 3.69
XAN	88.3 309	-P	16 11 45.6	-0.3						pP	23 31 50.0	4.0	
KMI	88.5 299	-P	16 11 47.5	0.8						sP	23 31 55.0	4.2	
		PMZ	$m_b = 5.9$		1.5	0.32				iS	23 34 32.0	1.2	
HHC	90.3 316	P	16 11 55.0	0.0						SMN			7.0 1.82
CD2	90.5 304	P	16 11 56.0	0.1						SME			7.0 1.90
		PMZ	$m_b = 6.1$		1.3	0.29				sS	23 34 44.0	1.6	
		sP	16 15 05.0	0.1						LN	$M_s = 5.2$		16.0 7.92
		PP	16 15 42.0	-1.0						LE			11.0 3.59
		SKS	16 21 27.0	-1.9						LZ	$M_s = 5.3$		20.0 16.7
BTO	91.1 315	P	16 11 59.0	0.2				BJI	16.6 327	eP	23 31 53.5	2.2	
		S	16 22 05.0	1.8						PMZ	$m_b = 5.7$		1.1 0.41
LZH	92.9 309	-P	16 12 07.5	0.2						PMZ	$m_b = 6.1$		9.0 8.84
		PMZ	$m_b = 5.8$		1.5	0.13				eS	23 34 56.0	2.3	
		pP	16 14 18.0	0.5						LN	$M_s = 5.6$		14.0 15.9
		sP	16 15 14.5	-1.9						LE			13.0 4.68
		ePP	16 15 58.0	-4.9						LZ	$M_s = 5.5$		15.0 18.4
		SKS	16 21 42.5	0.0				TIY	17.1 314	+iP	23 32 01.0	2.7	
		S	16 22 22.0	3.0						PMZ	$m_b = 5.3$		0.8 0.12
		SME			5.0	0.63				PMZ	$m_b = 5.8$		8.0 3.70
GTA	97.3 310	P	16 12 27.2	0.2						PP	23 32 17.0	4.6	
		PMZ	$m_b = 5.6$		1.2	0.050				S	23 35 07.0	1.2	
		SKS	16 22 05.0	-0.3						sS	23 35 18.5	0.2	
WMQ	107.4 311	ePdif	16 13 11.0	-0.8						SS	23 35 32.0	5.0	
KSH	114.7 304	ePKP	16 17 30.0	0.6						LN	$M_s = 5.3$		12.0 7.69
										LZ	$M_s = 5.5$		16.0 17.3
<p>MAY 17d 23h 27m <math>59.5 \pm 0.03s</math>, SD1.18 / 445                  26.61 N <math>\pm 0.85km</math>, 127.92 E <math>\pm 0.75km</math>, h33 <math>\pm 0.19km</math>                  Ryukyu Islands (238)  <math>M_s 5.4 / 53</math>, <math>M_L 5.6 / 1</math>, <math>m_b 5.8 / 23</math>,</p>								CN2	17.3 354	+iP	23 32 01.0	1.1	
SSE	7.4 309	P	23 29 49.2	1.1						PMZ	$m_b = 5.6$		1.0 0.30
		PMZ	$m_b = 6.1$		1.0	0.83				PMZ	$m_b = 5.9$		5.0 3.00
		sP	23 30 04.5	4.6						pP	23 32 11.0	3.5	
		S	23 31 13.0	1.3						sP	23 32 17.0	4.9	
		LN	$M_s = 5.3$		10.0	16.5				S	23 35 10.0	1.1	
		LE			10.0	15.0				sS	23 35 26.0	4.6	
QZH	8.6 261	+P	23 30 04.0	-0.3						PcP	23 36 40.0	-2.2	
		PMZ	$m_b = 5.3$		0.8	0.090				LN	$M_s = 5.2$		12.0 6.00
		PMZ	$m_b = 6.2$		8.0	7.32				LE			12.0 1.40
		S	23 31 38.0	-2.6				XAN	18.0 299	-iP	23 32 10.0	1.1	
		LN	$M_s = 5.1$		6.0	5.19				PMZ	$m_b = 5.8$		5.0 2.57
		LE			6.0	4.44				sP	23 32 25.0	3.9	
		LZ	$M_s = 4.8$		24.0	14.2				S	23 35 28.0	3.0	
										LN	$M_s = 5.3$		11.0 6.00
										LE			10.0 2.17
								QZN	18.3 249	P	23 32 13.0	0.6	









SMN				$M_L = 3.8$	0.8	0.26								
MAY 19d 04h 35m $43.5 \pm 0.57s$ , SD3.44 / 8							NJ2	21.3	255	LN	$M_S = 5.0$	14.0	3.20	
32.04 N $\pm 1.74km$ , 92.35 E $\pm 4.26km$ , h5 $\pm 0.70km$										LZ	$M_S = 5.0$	15.0	4.15	
Tibet (306)										06 51 19.5	-2.2			
GYA	13.7	110	P	04 38 58.4	-2.5				PMZ	$m_b = 4.9$	1.2	0.062		
TIY	17.4	65	eP	04 39 49.7	0.5				LN	$M_S = 4.8$	13.0	1.46		
MAY 19d 06h 30m $14.4 \pm 0.05s$ , SD2.89 / 10							HHC	24.0	282	LE		15.0	1.39	
40.59 N $\pm 0.40km$ , 79.54 E $\pm 0.45km$ , h29 $\pm 0.27km$										LZ	$M_S = 4.5$	18.0	1.79	
Southern Xinjiang Province (321)										P	06 51 48.8	-0.1		
$M_L 4.2 / 7$							TIY	24.0	274	LN	$M_S = 5.1$	13.0	0.93	
KSH	3.0	250	ePn	06 31 01.5	1.2				LE		17.0	3.47		
			Sn	06 31 43.0	6.5				eP	06 51 53.0	4.1			
			SMN		$M_L = 4.3$	0.6	1.10		pP	06 51 53.0	-3.4			
			SME			0.9	1.30		sP	06 52 03.0	3.1			
WMQ	6.9	59	iPn	06 31 56.6	2.8				S	06 55 59.0	-1.8			
			Sn	06 33 17.0	4.1				sS	06 56 14.0	0.0			
			SMN		$M_L = 3.8$	1.0	0.010	BTO	25.2	282	P	06 52 00.0	-0.4	
			SME			1.0	0.080				PP	06 52 39.0	1.0	
MAY 19d 06h 46m $34.7 \pm 0.03s$ , SD1.28 / 250										S	06 56 24.0	3.0		
40.26 N $\pm 1.08km$ , 143.22 E $\pm 0.80km$ , h25 $\pm 0.27km$										LN	$M_S = 5.2$	15.0	1.70	
Near east coast of Honshu (228)										LE		16.0	3.80	
$M_S 5.0 / 47$ , $m_b 5.5 / 3$ , $m_b 5.3 / 92$							WHN	25.4	257	LZ	$M_S = 5.2$	16.0	5.10	
MDJ	11.0	298	+P	06 49 15.1	1.6				+P	06 52 02.0	0.2			
			sS	06 51 24.0	-2.8				PMZ	$m_b = 5.4$	1.0	0.10		
			LN		$M_S = 5.0$	14.0	4.15		pP	06 52 10.0	0.7			
			LE			16.0	7.94		eS	06 56 24.0	-0.4			
			LZ		$M_S = 4.4$	25.0	4.12		LN	$M_S = 5.2$	13.0	0.99		
CN2	13.7	291	+P	06 49 49.0	-0.8				LE		15.0	3.95		
			PMZ		$m_b = 5.3$	1.0	0.060	QZH	25.6	241	LZ	$M_S = 4.9$	16.0	2.97
			pP	06 49 54.0	-1.9				eP	06 52 08.8	4.3			
			eS	06 52 21.0	-1.0				esS	06 56 40.0	-1.8			
			LN		$M_S = 4.7$	15.0	3.00		LE	$M_S = 4.8$	16.0	1.78		
			LE			15.0	1.70	XAN	27.9	268	LZ	$M_S = 4.7$	16.0	1.78
			LZ		$M_S = 4.8$	17.0	5.00		P	06 52 23.5	-2.0			
SNY	14.9	282	+P	06 50 06.0	0.1				LN	$M_S = 5.0$	13.0	1.70		
			PMZ		$m_b = 5.1$	1.0	0.040	GZH	30.5	245	LE		13.0	1.20
			sP	06 50 17.4	1.1				P	06 52 48.8	0.8			
			PP	06 50 19.0	1.4				eS	06 57 50.0	3.4			
			S	06 52 50.0	-0.6				LN	$M_S = 5.2$	13.0	1.78		
			LN		$M_S = 4.9$	13.0	2.06		LE		14.0	2.16		
			LE			15.0	4.10	LZH	31.1	275	LZ	$M_S = 4.9$	15.0	2.13
			LZ		$M_S = 4.9$	17.0	6.18		eP	06 52 53.5	-0.1			
DL2	16.7	272	P	06 50 28.0	-0.9				PMZ	$m_b = 5.1$	2.0	0.070		
			PMZ		$m_b = 5.6$	1.2	0.32		pP	06 53 02.5	1.4			
			eS	06 53 34.0	1.0				sP	06 53 06.5	1.9			
			LN		$M_S = 4.6$	14.0	1.82		ePP	06 53 53.5	-1.8			
			LE			20.0	1.50		eS	06 57 57.0	0.5			
SSE	20.1	250	eP	06 51 09.0	-0.2				LN	$M_S = 4.9$	15.0	0.90		
			PMZ		$m_b = 4.8$	1.2	0.050	GTA	33.1	283	LE		14.0	1.10
			pP	06 51 13.0	-3.4				LZ	$M_S = 4.8$	18.0	1.90		
			S	06 54 46.0	-1.9				+iP	06 53 11.5	0.1			
			sS	06 54 57.0	-2.1				S	06 58 30.0	2.8			
			eSS	06 55 17.0	0.8				LE	$M_S = 5.2$	16.0	2.97		
			LN		$M_S = 4.6$	13.0	0.96	CD2	33.2	266	LZ	$M_S = 5.3$	18.0	5.65
			LE			13.0	0.83		P	06 53 10.8	-1.4			
			LZ		$M_S = 4.6$	16.0	1.76		PMZ	$m_b = 5.2$	0.7	0.030		
BJI	20.7	278	P	06 51 12.5	-2.9				S	06 58 27.0	-1.7			
			PMZ		$m_b = 5.2$	1.5	0.18		LN	$M_S = 5.2$	14.0	2.80		
			PMZ		$m_b = 5.1$	4.0	0.40	GYA	33.2	257	LZ	$M_S = 4.9$	15.0	1.80
			eS	06 54 56.0	-4.2				+iP	06 53 12.0	-0.7			
			eSS	06 55 26.0	-4.3				pP	06 53 18.4	-1.9			
			LN		$M_S = 4.6$	14.0	1.29		S	06 58 30.6	1.1			
			LZ		$M_S = 4.9$	16.0	3.50		LN	$M_S = 5.3$	15.0	2.60		
TIA	20.9	267	P	06 51 15.2	-2.5				LE		15.0	2.10		
			eS	06 55 02.0	-2.5				LZ	$M_S = 4.8$	18.0	1.80		
								QZN	35.6	243	P	06 53 34.0	1.3	





KMI	36.9 258	eS	06 59 08.5	1.8			
		LN		$M_s = 5.2$	17.0	1.67	
		LE			15.0	1.60	
		+P	06 53 44.0	0.0			
		PMZ		$m_b = 5.8$	1.5	0.24	
		pP	06 53 52.0	0.4			
		S	06 59 24.0	-2.0			
WMQ	40.7 294	LN		$M_s = 5.3$	15.0	2.40	
		LE			15.0	1.40	
		LZ		$M_s = 5.4$	16.0	5.10	
		+iP	06 54 16.4	0.6			
		sP	06 54 25.0	-2.1			
		eS	07 00 25.0	0.0			
		sS	07 00 32.0	-5.9			
LSA	43.4 273	LE		$M_s = 5.0$	13.0	1.00	
		LZ		$M_s = 4.9$	20.0	1.80	
		P	06 54 38.5	0.5			
		KSH	50.5 292	P	06 55 34.0	0.6	
		pP		06 55 41.0	-0.1		
		S		07 02 47.0	3.6		
		LN		$M_s = 5.7$	15.0	2.70	
LE			16.0	2.90			

SNY	40.3 359	LZ		$M_g = 4.3$	20.0	0.50
		eP	09 35 36.8	-2.5		
LSA	42.2 315	eS	09 41 44.0	-0.9		
		LZ		$M_g = 4.6$	14.0	0.59
GTA	43.9 333	eP	09 35 52.8	-2.4		
		-iP	09 36 09.4	0.4		
WMQ	53.2 328	PMZ		$m_b = 5.1$	1.0	0.030
		P	09 37 21.0	-0.3		
		pP	09 37 29.0	-1.2		
		eS	09 44 48.0	-1.3		
		LZ		$M_g = 4.4$	24.0	0.39

MAY 19d 12h 57m  $31.1 \pm 0.06s$ , SD2.53 / 24  
 36.33 N  $\pm 0.73km$ , 100.05 E  $\pm 0.62km$ , h19  $\pm 0.08km$   
 Qinghai Province (325)  
 $M_s 3.5 / 4$ ,  $M_L 4.1 / 9$ ,  $m_b 3.8 / 1$

LZH	3.1 93	Pn	12 58 22.0	2.6		
		Pg	12 58 26.5	1.1		
GTA	3.1 357	Sg	12 59 06.5	-1.0		
		SMN		$M_L = 4.3$	0.8	1.09
CD2	6.2 149	SME			0.8	1.37
		Pg	12 58 26.0	0.2		
XAN	7.6 105	Sg	12 59 13.6	5.8		
		SMN		$M_L = 3.5$	0.6	0.10
BTO	8.9 58	SME			0.6	0.27
		LE		$M_s = 3.2$	8.0	0.42
TIY	10.0 78	eP	12 59 26.0	4.8		
		Pn	12 59 20.0	-1.6		
HHC	10.1 60	Pg	12 59 49.5	4.1		
		Sn	13 00 47.5	-2.2		
WMQ	12.0 312	Sg	13 01 28.5	-1.0		
		SMN		$M_L = 4.1$	1.0	0.060
SSE	27.5 314	SME			1.0	0.080
		eP	12 59 40.0	-2.1		
NJ2	29.7 314	eP	12 59 55.9	-1.3		
		LN		$M_s = 3.6$	10.0	0.24
DL2	32.4 327	LZ		$M_s = 3.9$	10.0	0.63
		eP	12 59 57.8	-0.5		
WHN	32.3 307	SMN			1.0	0.030
		SME			1.0	0.030

MAY 19d 13h 27m  $40.6 \pm 0.03s$ , SD1.04 / 229  
 13.11 N  $\pm 0.65km$ , 143.87 E  $\pm 0.63km$ , h139  $\pm 0.06km$   
 South of the Marianas (210)  
 $m_b 5.6 / 15$ ,  $m_b 5.5 / 62$ ,

MAY 19d 09h 28m  $02.8 \pm 0.03s$ , SD1.18 / 85  
 1.35 N  $\pm 0.57km$ , 124.13 E  $\pm 0.83km$ , h30  $\pm 0.08km$   
 Minahassa Peninsula (Celebes) (265)  
 $M_s 4.8 / 7$ ,  $m_b 5.6 / 1$ ,  $m_b 5.1 / 19$

QZN	22.5 322	eP	09 33 01.0	0.0			
		eS	09 37 01.0	-0.1			
		sS	09 37 12.0	-2.8			
		LN		$M_s = 4.8$	15.0	1.42	
		LE			14.0	1.20	
		GZH	24.0 335	P	09 33 17.2	1.1	
		eS		09 37 30.0	1.6		
GYA	30.1 328	eP	09 34 13.0	0.8			
		pP	09 34 21.8	1.0			
		S	09 39 09.0	2.2			
		LN		$M_s = 4.8$	15.0	1.00	
		LE			15.0	0.80	
WHN	30.5 343	eP	09 34 15.0	-0.5			
		pP	09 34 23.5	-0.8			
		eS	09 39 12.0	-1.8			
NJ2	30.9 351	eP	09 34 16.8	-2.8			
		KMI	31.4 321	+P	09 34 25.0	1.1	
PMZ		$m_b = 5.1$		1.7	0.050		
PMZ		$m_b = 5.6$		4.0	0.40		
CD2	35.2 329	LZ		$M_s = 4.9$	8.0	1.10	
		P	09 34 56.0	-0.4			
		S	09 40 28.2	2.2			
XAN	35.5 338	P	09 34 58.5	-0.7			
		S	09 40 34.0	2.9			
TIY	37.7 345	P	09 35 18.0	-0.2			
		eS	09 41 03.0	-3.7			
		sS	09 41 18.0	-3.3			
		LN		$M_s = 4.8$	22.0	1.33	
		LZ		$M_s = 4.6$	20.0	1.00	
BJI	39.2 350	eP	09 35 30.5	0.5			
		PMZ		$m_b = 4.7$	1.5	0.018	
		eS	09 41 28.0	-0.3			
		eSS	09 44 14.0	0.9			
		LN		$M_s = 5.1$	18.0	1.68	
		LE			18.0	0.97	
		LZ		$M_s = 4.1$	28.0	0.41	
LZH	39.3 334	P	09 35 32.5	0.9			
		PMZ		$m_b = 5.1$	2.0	0.070	
		pP	09 35 42.0	1.7			
		eS	09 41 32.0	0.8			
		eSS	09 44 20.0	3.2			

QZH	26.6 300	-P	13 33 07.0	-0.9		
		PMZ		$m_b = 5.5$	0.5	0.060
SSE	27.5 314	P	13 33 16.1	-0.3		
		PMZ		$m_b = 5.2$	1.1	0.058
NJ2	29.7 314	sP	13 33 58.0	-3.9		
		S	13 37 45.0	0.1		
		sS	13 38 32.0	-4.7		
		LE			12.0	0.24
		LZ			20.0	0.93
		+P	13 33 35.0	-0.9		
		PMZ		$m_b = 5.6$	5.0	0.64
WHN	32.3 307	sP	13 34 19.0	-2.7		
		eS	13 38 15.0	-5.4		
		+iP	13 33 59.5	0.8		
		PMZ		$m_b = 5.5$	1.0	0.10
		pP	13 34 27.0	-1.2		
DL2	32.4 327	eS	13 39 02.8	1.7		
		P	13 33 59.0	-0.4		
		PMZ		$m_b = 5.9$	1.0	0.21
		sP	13 34 41.0	-4.4		
		eS	13 39 04.0	1.5		
LN			11.0	0.31		







			sP	02 33	21.0	0.2						S	02 44	13.5	1.0			
			PP	02 35	50.0	3.4						LN		$M_s=7.6$		12.0	134	
			S	02 42	18.0	0.9						LE				20.0	127	
			SS	02 46	48.0	2.1						LZ		$M_s=7.0$		21.0	73.2	
			LN		$M_s=7.6$	16.0	169	WHN	80.7	60	cP	02 34	16.0	0.0				
			LZ		$M_s=7.3$	20.0	174				PMZ		$m_b=6.3$		1.5	0.46		
KMI	70.2	65	-iP	02 33	15.5	-1.2					pP	02 34	21.0	-0.8				
			PMZ		$m_b=6.4$	2.5	1.20				PP	02 37	26.0	5.2				
			PP	02 35	51.0	-1.8					S	02 44	22.0	1.4				
			iS	02 42	28.0	0.5					S	02 44	24.0	3.4				
			LN		$M_s=7.2$	16.0	67.5				LN		$M_s=7.5$		16.0	102		
			LE			16.0	13.6				LE				20.0	76.5		
			LZ		$M_s=6.9$	26.0	87.8	BJI	82.1	50	-P	02 34	24.0	0.4				
CD2	71.6	59	P	02 33	22.4	-2.2					PMZ		$m_b=6.4$		2.0	0.88		
			S	02 42	39.0	-2.1					PMZ		$m_B=6.5$		6.0	2.84		
			LN		$M_s=7.7$	23.0	310				pP	02 34	28.0	-1.4				
			LZ		$M_s=7.1$	22.0	112				eS	02 44	41.0	3.7				
LZH	72.2	54	-iP	02 33	27.5	-0.8					LN		$M_s=7.5$		16.0	94.6		
			PMZ		$m_b=6.5$	2.5	1.54	TIA	82.9	54	-P	02 34	27.6	-0.1				
			PMZ		$m_B=7.0$	4.0	6.40				PMZ		$m_b=6.3$		1.6	0.50		
			sP	02 33	35.0	-1.8					PMZ		$m_B=6.6$		9.0	5.20		
			PP	02 36	12.0	2.8					pP	02 34	33.0	-0.6				
			S	02 42	51.0	3.0					S	02 44	48.0	4.4				
			SMN			36.0	65.0				LN		$M_s=8.0$		17.0	294		
			LN		$M_s=7.8$	18.0	299				LE				17.0	110		
			LE			19.0	119	NJ2	84.5	58	-iP	02 34	35.0	-0.6				
GYA	73.8	64	P	02 33	37.0	-1.0					PMZ		$m_B=6.8$		5.0	4.26		
			PMZ		$m_b=5.9$	1.6	0.20				S	02 45	02.0	2.7				
			PMZ		$m_B=6.6$	4.0	2.70				SS	02 50	35.0	2.5				
			PcP	02 33	56.0	3.3					LN		$M_s=7.7$		18.0	173		
			S	02 43	03.0	-3.8					LZ		$M_s=7.0$		18.0	59.7		
			LN		$M_s=7.8$	20.0	292	QZH	84.6	66	-P	02 34	37.0	0.7				
			LE			20.0	114				PMZ		$m_B=6.8$		4.0	3.63		
			LZ		$M_s=6.7$	28.0	63.8				S	02 45	04.0	3.4				
XAN	76.1	56	P	02 33	50.0	-1.3					LN		$M_s=7.7$		20.0	135		
			S	02 43	38.0	5.5					LE				20.0	112		
			LN		$M_s=7.5$	18.0	117				LZ		$M_s=7.0$		20.0	58.6		
			LE			18.0	81.7	DL2	86.4	51	eP	02 34	45.0	0.0				
QZN	76.7	72	-P	02 33	54.0	-0.3					PMZ		$m_b=6.7$		1.8	1.27		
			S	02 43	42.0	3.6					PMZ		$m_B=6.5$		5.0	2.27		
			LN		$M_s=7.4$	18.0	42.8				pP	02 34	52.0	1.1				
			LE			18.0	91.8				S	02 45	22.0	4.3				
BTO	77.4	50	-iP	02 33	59.0	0.5					SMN				28.0	55.4		
			sP	02 34	08.0	0.9					LN		$M_s=7.8$		22.0	227		
			PP	02 36	56.0	2.6					LE				20.0	48.5		
			iS	02 43	52.0	3.8					LZ		$M_s=6.9$		30.0	67.7		
			LN		$M_s=7.6$	15.0	96.0	SSE	86.5	59	P	02 34	45.0	-0.8				
			LE			15.0	98.0				PMZ		$m_B=6.5$		6.0	2.33		
			LZ		$M_s=7.4$	15.0	150				pP	02 34	50.0	-1.7				
HHC	78.6	50	-iP	02 34	06.0	0.9					SKS	02 45	08.0	-0.1				
			PMZ		$m_b=6.4$	1.2	0.53				S	02 45	22.0	2.8				
			PMZ		$m_B=6.9$	6.0	7.87				sS	02 45	31.0	0.2				
			S	02 44	06.0	6.8					LN		$M_s=7.9$		16.0	173		
			SKS	02 44	10.0	-3.5					LE				18.0	168		
			LN		$M_s=7.4$	18.0	38.3	SNY	87.6	48	-iP	02 34	50.0	-1.2				
			LE			18.0	92.8				PMZ		$m_b=6.4$		2.3	0.69		
			LZ		$M_s=7.3$	26.0	198				PMZ		$m_B=6.5$		7.0	2.72		
TIY	79.2	53	-iP	02 34	07.5	-0.5					sP	02 34	57.5	-2.4				
			PMZ		$m_B=6.4$	12.0	5.30				PP	02 38	23.0	5.1				
			pP	02 34	16.0	2.2					iS	02 45	27.0	-4.5				
			S	02 44	08.0	3.1					LN		$M_s=8.0$		18.0	314		
			SMN			10.0	12.0				LE				20.0	171		
			sS	02 44	14.0	-2.3					-P	02 34	56.0	-0.9				
			LE		$M_s=7.7$	20.0	210	CN2	88.8	46	PMZ		$m_b=5.8$		1.0	0.070		
			LZ		$M_s=7.2$	20.0	113				PMZ		$m_B=6.7$		6.0	3.10		
GZH	79.9	68	P	02 34	13.0	1.2					pP	02 35	01.0	-1.8				
			PMZ		$m_b=6.0$	1.2	0.20				PP	02 38	28.0	0.6				
			PMZ		$m_B=6.6$	6.0	3.66				eS	02 45	44.0	1.4				



MDJ	91.7	45	LN	$M_s = 7.7$	17.0	98.0	WMQ	12.3	313	S	05 51 52.8	2.5	WHN	13.1	111	P	05 50 00.0	-2.0	BJI	13.2	68	PMZ	$m_b = 5.1$	0.5	0.020
			LE		17.0	116				pP	05 50 05.5	-1.2				eP	05 50 13.4	0.8							
			+iP	02 35 09.7	-0.5					S	05 52 17.8	-1.3				sP	05 50 24.0	2.8							
			PP	02 38 50.0	0.1					eP	05 50 13.5	-0.8				PMZ	$m_b = 4.3$	1.0				0.0060			
			PPMZ	$m_b = 6.9$		10.0				4.76															
			S	02 46 09.0	2.4																				
			SMN			30.0				37.1															
			LN	$M_s = 8.1$	20.0	396																			
LE		20.0	175																						
<p>MAY 20d 02h 44m <math>03.3 \pm 0.06s</math>, SD1.54 / 40                  29.55 N <math>\pm 0.84km</math>, 128.12 E <math>\pm 0.64km</math>, h31 <math>\pm 0.09km</math>                  East China Sea (234)  <math>M_s 5.2 / 7</math>, <math>M_L 5.5 / 4</math>, <math>m_b 4.8 / 8</math></p>													<p>MAY 20d 06h 43m <math>44.4 \pm 0.04s</math>, SD0.97 / 324                  43.92 N <math>\pm 0.91km</math>, 147.68 E <math>\pm 0.62km</math>, h18 <math>\pm 0.08km</math>                  Kurile Islands (221)  <math>M_s 4.9 / 33</math>, <math>m_b 5.7 / 5</math>, <math>m_b 5.6 / 104</math></p>												
SSE	6.2	286	P	02 45 36.0	1.1		MDJ	13.0	279	+iP	06 46 53.5	2.4													
			pP	02 45 43.0	1.5					PMZ	$m_b = 5.5$		2.0	0.18											
			S	02 46 44.5	-0.9					sP	06 47 03.4	3.1													
			LN	$M_s = 5.2$		16.0	30.2			S	06 49 15.0	-0.8													
			LE			16.0	11.3			SMN			6.0	2.49											
NJ2	8.3	290	-P	02 46 08.0	2.8					LN	$M_s = 4.6$	11.0	1.87												
			pP	02 46 15.0	3.1					LZ	$M_s = 4.7$	30.0	7.54												
			S	02 47 42.0	2.8					P	06 47 31.0	0.0													
			SMN	$M_L = 5.6$		1.0	1.24			PMZ	$m_b = 5.1$	1.0	0.080												
			SME			1.0	1.41			pP	06 47 37.0	0.6													
QZH	9.6	244	P	02 46 24.0	1.0					eS	06 50 29.0	0.6													
DL2	10.8	332	eP	02 46 39.5	1.0					LN	$M_s = 4.8$	11.0	1.60												
			S	02 48 37.0	-1.7					LE		11.0	1.50												
			SMN			1.2	0.36			LZ	$M_s = 4.6$	24.0	4.30												
			SME			1.3	0.45			+P	06 47 52.6	-0.3													
WHN	12.0	278	eP	02 46 56.0	1.1					PMZ	$m_b = 5.3$	1.0	0.13												
			sP	02 47 06.5	0.0					S	06 51 10.0	2.1													
			S	02 49 12.0	3.9					SMN		6.0	0.70												
			LN	$M_s = 5.2$		12.0	8.97			SME		4.0	0.89												
SNY	12.8	344	-iP	02 47 06.4	0.5					sS	06 51 18.0	0.4													
BJI	14.3	320	eP	02 47 26.0	-0.2					LN	$M_s = 4.8$	9.0	1.62												
			PMZ	$m_b = 5.6$		1.8	0.19			LZ	$M_s = 4.6$	28.0	4.08												
QZN	19.7	242	eP	02 48 36.2	3.6					-P	06 48 21.8	1.1													
LZH	21.4	294	eP	02 48 52.0	1.1					PMZ	$m_b = 5.5$	1.0	0.21												
<p>MAY 20d 05h 47m <math>04.3 \pm 0.04s</math>, SD1.67 / 102                  36.10 N <math>\pm 0.62km</math>, 100.18 E <math>\pm 0.47km</math>, h14 <math>\pm 0.07km</math>                  Qinghai Province (325)  <math>M_s 4.3 / 7</math>, <math>M_L 4.4 / 11</math>, <math>m_b 4.6 / 36</math></p>													<p>DL2</p>												
LZH	3.0	89	+Pn	05 47 55.0	3.4					S	06 51 59.5	-1.0													
			Pg	05 48 00.0	3.2					LN	$M_s = 4.8$	10.0	1.43												
			Sg	05 48 40.0	2.6					eP	06 48 56.5	0.4													
			SMN	$M_L = 5.1$		1.0	8.79			PMZ	$m_b = 5.4$	1.4	0.20												
			SME			1.0	6.22			PMZ	$m_b = 5.4$	4.0	0.57												
GTA	3.3	355	-iPg	05 48 02.0	-1.1					ePP	06 49 30.0	1.8													
			Sg	05 48 51.4	3.1					eS	06 53 07.0	0.2													
			SMN	$M_L = 3.9$		1.0	0.28			LN	$M_s = 4.6$	10.0	0.82												
			SME			1.0	0.48			LZ	$M_s = 4.8$	32.0	4.54												
			LN	$M_s = 3.9$		8.0	1.87			P	06 49 04.0	-0.1													
CD2	6.0	149	Pg	05 48 47.4	-2.6					PMZ	$m_b = 5.6$	1.0	0.21												
			SMN	$M_L = 4.0$		1.2	0.10			sP	06 49 15.0	1.2													
			SME			1.0	0.10			PP	06 49 40.0	0.7													
XAN	7.5	103	Pn	05 48 53.5	0.3					S	06 53 20.0	-0.3													
			Sg	05 51 00.0	2.1					sS	06 53 32.0	0.3													
			SMN	$M_L = 4.4$		1.0	0.16			LN	$M_s = 5.0$	13.0	1.92												
			SME			1.0	0.10			LE		14.0	1.62												
			LN	$M_s = 4.3$		5.0	0.85			LZ	$M_s = 4.3$	18.0	0.90												
			LE			4.0	0.47			P	06 49 05.6	1.2													
BTO	8.9	57	eP	05 49 17.0	0.7					PMZ	$m_b = 5.4$	1.3	0.20												
			LN	$M_s = 4.3$		14.0	1.40			sP	06 49 16.5	2.4													
			LE			14.0	1.30			S	06 53 19.0	-1.8													
HHC	10.1	59	P	05 49 32.0	-0.4					-P	06 49 14.6	0.9													
GYA	11.1	148	P	05 49 46.4	0.4					sP	06 49 29.0	5.6													
			pP	05 49 52.0	0.8					S	06 53 36.0	-1.1													
										LN	$M_s = 5.1$	15.0	2.02												



HHC	26.7 276	LE		13.0	1.97	LSA	46.6 272	LZ	$M_s = 5.3$	18.0	3.52		
		LZ	$M_s = 4.3$	20.0	0.92			P	06 52 14.4	0.3			
		P	06 49 26.9	1.6				S	06 58 56.0	-4.0			
		PMZ	$m_b = 5.4$	1.0	0.090			SMN		5.0	0.40		
		eS	06 53 55.0	-3.4				P	06 52 58.0	1.0			
		SMN			7.0			1.64	pP	06 53 05.0	1.4		
		SME			7.0			2.35	S	07 00 21.0	2.6		
		LN	$M_s = 4.9$	10.0	0.68			sS	07 00 35.0	4.2			
TIY	27.2 269	LE		10.0	0.92	KSH	52.2 292	LN	$M_s = 5.3$	10.0	0.90		
		LZ	$M_s = 5.0$	16.0	3.44								
		eP	06 49 31.0	1.0				MAY 20d 07h 32m $37.9 \pm 0.09s$ , $SD1.12 / 396$					
		pP	06 49 36.0	-0.4				$17.98 S \pm 1.41km$ , $175.15 W \pm 0.85km$ , $h237 \pm 0.62km$					
		S	06 54 11.5	5.7				Tonga (173)					
		LN	$M_s = 4.8$	15.0	1.40			$m_b 6.2 / 34$ , $m_b 5.9 / 75$ ,					
		LZ	$M_s = 4.6$	34.0	2.95			QZH	77.3 302	-P	07 44 07.0	-1.7	
		P	06 49 37.0	0.9				PMZ		$m_b = 5.9$	1.0	0.25	
BTO	27.9 276	pP	06 49 40.5	-2.0		PMZ		$m_b = 6.6$	4.0	4.54			
		S	06 54 19.0	2.4		sP	07 45 30.0	1.1					
		sS	06 54 30.0	1.5		S	07 53 40.0	3.2					
		LN	$M_s = 4.9$	12.0	0.90	SSE	78.2 308	P	07 44 12.0	-1.4			
		LE		12.0	1.30	PMZ		$m_b = 5.5$	1.0	0.097			
		+P	06 49 50.0	-0.1		PMZ		$m_b = 5.9$	6.0	1.55			
		PMZ	$m_b = 5.0$	0.7	0.020	sP	07 45 32.0	-1.7					
		sP	06 50 00.5	0.5		S	07 53 45.0	-0.9					
WHN	29.5 254	eS	06 54 41.8	-0.9		LE			12.0	0.49			
		LN	$M_s = 5.1$	14.0	1.93	LZ			22.0	1.43			
		LE		10.0	0.63	MDJ	80.1 323	-P	07 44 23.4	0.0			
		LZ	$M_s = 4.5$	24.0	1.37	PMZ		$m_b = 6.3$	1.8	1.07			
		P	06 50 09.5	1.9		PMZ		$m_b = 6.5$	5.0	4.50			
		+iP	06 50 32.0	0.8		PcP	07 44 30.0	0.5					
		PMZ	$m_b = 5.7$	1.5	0.19	sP	07 45 43.0	-0.9					
		PMZ	$m_b = 5.7$	3.5	0.41	SKS	07 54 13.0	0.8					
XAN	31.5 265	pP	06 50 39.5	1.8		SME			7.0	4.20			
		sP	06 50 43.5	2.7		sS	07 55 45.0	0.8					
		S	06 55 54.0	-0.8		NJ2	80.4 308	-iP	07 44 25.0	-0.2			
		SME		6.0	0.89	PMZ		$m_b = 6.2$	6.0	3.15			
		LN	$M_s = 4.8$	10.0	0.70	sP	07 45 47.0	1.3					
		LZ	$M_s = 4.9$	16.0	1.64	S	07 54 15.0	6.1					
		eP	06 50 39.3	0.8		GZH	80.9 298	-P	07 44 27.9	0.2			
		+iP	06 50 44.8	0.8		PMZ		$m_b = 5.8$	1.0	0.20			
GZH	35.0 245	PcP	06 53 12.0	0.2		PMZ		$m_b = 6.5$	5.0	4.97			
		S	06 56 13.0	-4.9		pP	07 45 24.0	0.4					
		LE	$M_s = 4.8$	11.0	0.72	sP	07 45 48.0	-0.3					
		+iP	06 50 53.8	0.1		S	07 54 14.0	0.1					
		PMZ	$m_b = 5.7$	0.8	0.10	DL2	81.8 315	-P	07 44 32.0	-0.4			
		S	06 56 29.5	-6.3		PMZ		$m_b = 6.3$	1.7	0.97			
		+iP	06 50 58.2	0.0		PMZ		$m_b = 6.2$	6.0	3.15			
		pP	06 51 07.0	2.2		SME			10.0	2.54			
GTA	35.6 280	sP	06 51 10.8	2.9		LZ			28.0	1.47			
		PcS	06 57 03.8	-0.3		CN2	82.0 321	-P	07 44 32.4	-1.1			
		eP	06 51 22.0	0.1		PMZ		$m_b = 6.2$	1.0	0.50			
		eS	06 57 27.0	-1.0		PMZ		$m_b = 6.4$	5.0	3.90			
		LN	$M_s = 5.2$	14.0	1.31	pP	07 45 29.0	-0.4					
		LE		14.0	1.47	eS	07 54 25.0	-1.9					
		+P	06 51 29.0	0.9		SMN			7.0	0.70			
		PMZ	$m_b = 5.5$	2.0	0.17	SME			7.0	3.00			
CD2	36.8 264	sP	06 51 39.0	1.3		-iP	07 44 33.0	-0.8					
		PP	06 53 09.0	3.9		PMZ		$m_b = 6.3$	2.0	1.29			
		S	06 57 34.0	-3.8		PMZ		$m_b = 6.3$	6.0	4.03			
		LZ	$M_s = 4.7$	24.0	1.20	sP	07 45 53.0	-1.5					
		+iP	06 51 41.2	1.2		iS	07 54 32.0	4.5					
		PMZ	$m_b = 6.1$	4.0	1.42	SMN			6.0	2.19			
		pP	06 51 48.0	1.3		SME			7.0	4.24			
		iS	06 57 56.0	-4.7		LZ			24.0	2.26			
QZN	40.2 244	SMN		5.0	0.64	QZN	82.3 293	-P	07 44 34.5	-0.7			
		sS	06 58 16.0	4.3		PMZ		$m_b = 6.0$	1.8	0.51			
		ScS	07 01 34.0	-4.0		PMZ		$m_b = 6.2$	6.0	2.80			
		LN	$M_s = 5.4$	8.0	1.56	sP	07 45 55.5	-0.4					







		SMN		7.0	0.30	XAN	25.5	94	eP	02 50 00.6	0.2			
		SME		7.0	1.20	TIY	27.0	84	eP	02 50 14.8	0.8			
		sS	10 18 58.0		0.6				eS	02 54 43.0	-5.0			
GYA	90.9	301	+iP	10 06 15.0	0.9				LE	$M_s=4.2$	10.0	0.23		
			PMZ	$m_b=5.5$		1.0	0.13		LZ	$M_s=4.3$	14.0	0.60		
			pP	10 07 37.0	3.3			GYA	27.6	111	P	02 50 21.2	1.3	
			S	10 16 42.0	4.5			SSE	36.1	91	eP	02 51 35.0	0.7	
KMI	93.0	298	+P	10 06 25.0	0.9			<hr/> <p>MAY 21d 06h 55m <math>46.8 \pm 0.10s</math>, SD2.62 / 5  <math>21.24 N \pm 0.89km</math>, <math>111.94 E \pm 0.25km</math>, <math>h8 \pm 0.02km</math>                      Eastern China (664)  <math>M_L 3.4 / 3</math>,</p>						
			PMZ	$m_b=5.2$		2.0	0.12	GZH	2.3	35	Pg	06 56 24.6	-2.0	
			pP	10 07 47.5	3.7						Sn	06 56 49.6	-4.9	
			S	10 17 00.2	4.1						SMN	$M_L=3.2$	0.4	0.17
BJI	93.0	317	eP	10 06 24.0	0.1						SME		0.4	0.16
			PMZ	$m_b=5.3$		0.6	0.044							
			pP	10 07 45.0	1.2			GYA	7.1	318	Pg	06 57 52.8	0.5	
			eSKS	10 16 21.0	-1.4			<hr/> <p>MAY 21d 07h 25m <math>46.7 \pm 0.03s</math>, SD1.78 / 7  <math>26.98 N \pm 0.24km</math>, <math>101.11 E \pm 0.23km</math>, <math>h5 \pm km</math>                      Yunnan Province (318)  <math>M_L 3.0 / 5</math>,</p>						
			eS	10 16 58.0	0.1			KMI	2.3	141	ePg	07 26 27.5	-0.9	
TIY	93.8	313	+iP	10 06 28.0	0.5						Sg	07 27 01.0	0.7	
			pP	10 07 50.0	2.7						SMN	$M_L=3.0$	1.5	0.10
			SKS	10 16 28.5	2.0						SME		1.5	0.10
			SMN			10.0	0.59	CD2	4.5	30	ePn	07 26 57.8	1.2	
			SME			11.0	0.62				Pg	07 27 05.3	-1.7	
XAN	93.8	308	P	10 06 28.0	0.5						Sg	07 28 04.5	-4.7	
			pP	10 07 50.0	2.6						SMN	$M_L=3.2$	1.0	0.030
			S	10 17 08.0	5.2						SME		1.0	0.050
CD2	95.5	303	P	10 06 36.2	0.8			GYA	5.0	95	Pg	07 27 16.4	1.3	
			pP	10 07 56.7	1.4			<hr/> <p>MAY 21d 13h 00m <math>08.8 \pm 0.04s</math>, SD0.84 / 387  <math>53.62 N \pm 0.86km</math>, <math>163.58 W \pm 0.46km</math>, <math>h33 \pm 0.03km</math>                      Unimak Island region (10)  <math>M_s 5.6 / 45</math>, <math>m_b 5.8 / 17</math>, <math>m_b 5.6 / 116</math></p>						
			S	10 17 22.0	4.5			MDJ	43.1	286	-P	13 08 07.3	-1.1	
HHC	96.2	315	eP	10 06 38.5	-0.3						PMZ	$m_b=5.4$	0.5	0.030
BTO	97.0	314	eP	10 06 47.0	4.7						sP	13 08 20.0	-1.8	
LZH	98.4	307	eP	10 06 49.5	1.0						S	13 14 36.0	4.5	
			PMZ	$m_b=5.4$		1.5	0.034				LZ	$M_s=5.3$	23.0	4.44
			pP	10 08 12.0	3.8			CN2	46.0	288	+iP	13 08 30.6	-0.8	
			SKS	10 16 50.0	-1.2						PMZ	$m_b=6.0$	1.0	0.20
			eS	10 17 44.0	0.3						PMZ	$m_b=5.7$	5.0	0.60
GTA	102.8	309	P	10 07 09.0	0.6						pP	13 08 40.0	-0.8	
WMQ	112.9	308	PKP	10 11 44.0	-0.5						PP	13 10 18.0	-1.1	
			PP	10 12 39.0	-3.6						eS	13 15 14.0	0.2	
			PPMZ			1.0	0.020				eSS	13 18 30.0	-0.4	
			PKS	10 15 14.0	-4.8						LN	$M_s=5.4$	14.0	1.90
			SKKS	10 18 59.5	0.8						LE		14.0	1.10
<p>MAY 20d 18h 01m <math>56.9 \pm 0.05s</math>, SD1.41 / 22  <math>28.37 N \pm 0.65km</math>, <math>83.25 E \pm 0.45km</math>, <math>h66 \pm 0.20km</math>                      Nepal-India border region (309)  <math>m_b 4.4 / 6</math>,</p>														
GYA	20.9	90	P	18 06 35.2	-0.9						LZ	$M_s=5.2$	20.0	2.80
<p>MAY 21d 02h 44m <math>32.0 \pm 0.04s</math>, SD1.39 / 57  <math>40.21 N \pm 0.69km</math>, <math>77.75 E \pm 0.43km</math>, <math>h28 \pm 0.12km</math>                      Southern Xinjiang Province (321)  <math>M_s 4.7 / 5</math>, <math>M_L 4.8 / 3</math>, <math>m_b 4.4 / 15</math></p>														
KSH	1.6	244	+iPg	02 45 00.0	-0.3			SNY	48.3	287	+iP	13 08 49.5	0.0	
			Sg	02 45 19.0	-2.8						PMZ	$m_b=5.8$	1.3	0.18
			SMN			3.0	24.0				PMZ	$m_b=5.6$	10.0	0.90
WMQ	8.2	61	P	02 46 33.0	0.1						pP	13 09 00.0	1.1	
			S	02 48 05.0	-0.6						PP	13 10 42.5	1.6	
			LE	$M_s=4.7$		4.0	1.56				S	13 15 48.0	2.4	
GTA	17.0	86	eP	02 48 26.8	-2.7						SME		25.0	1.17
			LE	$M_s=4.2$		9.0	0.43				LN	$M_s=5.4$	15.0	1.50
			LZ	$M_s=4.0$		16.0	0.58				LE		14.0	1.45
LZH	20.9	93	-P	02 49 15.0	-0.2						LZ	$M_s=5.3$	22.0	3.93
			PMZ	$m_b=4.3$		1.4	0.022	DL2	51.4	285	eP	13 09 12.2	-0.6	
			eSS	02 53 34.0	0.7						PMZ	$m_b=5.7$	1.0	0.10
			LZ	$M_s=4.1$		22.0	0.80				PMZ	$m_b=5.6$	6.0	0.49
CD2	23.0	106	eP	02 49 38.4	2.0						S	13 16 29.0	1.1	
BTO	24.5	79	eP	02 49 53.1	2.4						ScS	13 19 00.0	3.3	
											LE	$M_s=5.4$	18.0	2.48





BJI	53.7 290	LZ	$M_s = 5.1$	24.0	2.30	LZH	63.3 295	S	13 19 10.0	6.6	WMQ	65.4 311	S	13 19 06.0	1.3									
		eP	13 09 30.0	-0.2	1.2			0.097	+P	13 10 37.0			-0.5	1.4	0.40	PMZ	$m_b = 6.2$	10.0	0.95					
		PMZ	$m_b = 5.6$	5.0	0.48			PMZ	$m_b = 5.7$	13 10 45.0			-1.9	PMZ	$m_b = 5.9$	6.0	0.90							
		PMZ	$m_B = 5.7$	17.0	2.14			PMZ	$m_B = 5.9$	13 11 01.5			-3.3	sP	13 11 16.7	0.0	PP	13 13 16.7	0.0					
		esP	13 09 41.0	-2.7	20.0			3.05	PMZ	$m_b = 5.0$			1.5	0.030	PP	13 13 16.7	0.0	S	13 19 32.0	1.0				
		ePP	13 11 32.0	0.2	13 09 57.0			2.8	PMZ	$m_B = 5.9$			6.0	0.90	S	13 19 32.0	1.0	ScS	13 20 41.0	1.6				
		eS	13 17 00.0	-0.7	13 10 42.0			-1.1	PMZ	$m_b = 5.6$			15.0	2.77	ScS	13 20 41.0	1.6	LZ	$M_s = 5.6$	15.0	2.77			
		esS	13 17 14.0	-2.5	13 17 31.5			5.2	PMZ	$m_B = 5.6$			8.0	0.70	LZ	$M_s = 5.6$	15.0	2.77	LZ	$M_s = 5.6$	15.0	2.77		
		LN	$M_s = 5.4$	16.0	4.20			S	13 17 43.0	3.2			CD2	67.2 291	+iP	13 11 03.0	0.3	LN	$M_s = 5.6$	13.0	1.46			
		LZ	$M_s = 5.3$	15.0	2.48			LN	$M_s = 5.9$	15.0			4.00	S	13 19 56.0	3.0	LN	$M_s = 5.6$	13.0	1.46				
HHC	55.7 294	+P	13 09 44.8	0.0	15.0	3.70	GZH	67.7 279	+P	13 11 06.0	0.4	GYA	69.0 286	+iP	13 11 14.0	0.2								
		PMZ	$m_b = 6.0$	1.0	0.22	LN			$M_s = 5.7$	14.0	1.65			PMZ	$m_b = 6.0$	1.4	0.30	sP	13 11 25.0	-2.3				
		pP	13 09 57.0	2.8	16.0	1.80			LN	$M_s = 5.7$	14.0			1.65	sP	13 11 25.0	-2.3	PcP	13 11 38.0	0.9				
		PcP	13 10 42.0	-1.1	16.0	0.90			LZ	$M_s = 5.3$	17.0			1.80	PcP	13 11 38.0	0.9	S	13 20 18.0	4.0				
		S	13 17 31.5	5.2	22.0	2.60			LZ	$M_s = 5.3$	24.0			2.29	S	13 20 18.0	4.0	sS	13 20 28.0	-3.3				
		LN	$M_s = 5.9$	15.0	4.00	+iP			13 09 52.0	-0.2	GZA			69.0 286	+iP	13 11 14.0	0.2	sS	13 20 28.0	-3.3	LN	$M_s = 5.9$	20.0	2.90
		LE	15.0	2.48	15.0	3.70			LN	$M_s = 5.9$	15.0			5.20	PMZ	$m_b = 6.0$	1.4	0.30	LE	20.0	4.10			
		LZ	$M_s = 5.6$	20.0	5.49	LZ			$M_s = 5.7$	15.0	5.20			sP	13 11 25.0	-2.3	0.30	LZ	$M_s = 5.1$	24.0	1.40			
		+P	13 09 44.9	-0.8	15.0	0.54			LN	$M_s = 5.7$	15.0			5.20	PcP	13 11 38.0	0.9	0.30	LZ	$M_s = 5.1$	24.0	1.40		
		PMZ	$m_b = 5.7$	1.6	0.16	LN			$M_s = 5.9$	15.0	3.70			PcP	13 11 38.0	0.9	0.30	LZ	$M_s = 5.1$	24.0	1.40			
PMZ	$m_B = 5.6$	8.0	0.70	LE	$M_s = 5.9$	15.0	3.70	S	13 20 18.0	4.0	0.30	LZ	$M_s = 5.1$	24.0	1.40									
TIA	55.8 286	eS	13 17 32.0	2.7	15.0	5.20	KMI	72.3 288	+iP	13 11 14.0	0.2	QZN	72.9 279	P	13 11 37.5	0.3								
		LN	$M_s = 5.5$	16.0	1.80	PMZ			$m_b = 5.4$	2.0	0.10			sP	13 11 48.0	-2.8	KSH	74.0 316	P	13 11 45.0	1.0			
		LE	16.0	0.90	LN	$M_s = 5.6$			20.0	2.90	sP			13 11 48.0	-2.8	sP			13 11 56.0	-1.3				
		LZ	$M_s = 5.3$	22.0	2.60	LZ			$M_s = 5.3$	17.0	1.80			PP	13 14 11.0	-3.9			S	13 21 17.0	5.2			
		+P	13 09 44.9	-0.8	22.0	2.60			LZ	$M_s = 5.3$	24.0			2.29	S	13 21 17.0			5.2	sS	13 21 27.0	-2.2		
		PMZ	$m_b = 5.7$	1.6	0.16	+iP			13 09 52.0	-0.2	GZH			67.7 279	+P	13 11 06.0			0.4	ScS	13 21 50.0	3.1		
		PMZ	$m_B = 5.6$	8.0	0.70	LN			$M_s = 5.9$	15.0	4.00			S	13 20 00.0	1.5			LE	$M_s = 6.2$	16.0	6.10		
		eS	13 17 32.0	2.7	15.0	3.70			LZ	$M_s = 5.7$	15.0			5.20	LN	$M_s = 5.7$			14.0	1.04	LZ	$M_s = 5.7$	20.0	4.30
		LN	$M_s = 5.5$	16.0	1.80	LZ			$M_s = 5.7$	15.0	5.20			LN	$M_s = 5.7$	14.0			1.04	LZ	$M_s = 5.7$	20.0	4.30	
		LE	16.0	0.90	15.0	3.70			+iP	13 09 52.0	-0.2			GZA	69.0 286	+iP			13 11 14.0	0.2	LZ	$M_s = 5.7$	20.0	4.30
LZ	$M_s = 5.3$	22.0	2.60	LE	$M_s = 5.9$	15.0	3.70	LN	$M_s = 5.7$	14.0	1.65	LZ	$M_s = 5.7$	20.0	4.30									
BTO	56.7 295	+iP	13 09 52.0	-0.2	15.0	3.70	QZN	72.9 279	P	13 11 37.5	0.3	LSA	75.0 300	P	13 11 50.0	0.3								
		pP	13 10 03.0	1.5	15.0	3.70			PMZ	$m_b = 6.0$	1.4			0.30	sP	13 11 48.0	-2.8	S	13 21 26.5	4.2				
		S	13 17 43.0	3.2	15.0	3.70			sP	$m_b = 6.0$	1.4			0.30	eS	13 21 03.5	2.8	LN	$M_s = 5.7$	16.0	1.97			
		LN	$M_s = 5.9$	15.0	4.00	LN			$M_s = 5.3$	24.0	2.29			sP	13 11 48.0	-2.8	LE	16.0	0.99					
		LE	15.0	3.70	15.0	3.70			LZ	$M_s = 5.3$	24.0			2.29	PP	13 14 11.0	-3.9	LZ	$M_s = 5.7$	20.0	4.30			
		LZ	$M_s = 5.3$	22.0	2.60	LZ			$M_s = 5.3$	24.0	2.29			S	13 20 58.0	6.2	LZ	$M_s = 5.7$	20.0	4.30				
		+iP	13 09 52.0	-0.2	15.0	3.70			LZ	$M_s = 5.3$	24.0			2.29	LN	$M_s = 5.8$	10.0	0.60	LZ	$M_s = 5.7$	20.0	4.30		
		pP	13 10 03.0	1.5	15.0	3.70			LZ	$M_s = 5.3$	24.0			2.29	LN	$M_s = 5.8$	10.0	0.60	LZ	$M_s = 5.7$	20.0	4.30		
		S	13 17 43.0	3.2	15.0	3.70			LZ	$M_s = 5.3$	24.0			2.29	LE	15.0	2.20	LZ	$M_s = 5.7$	20.0	4.30			
		LN	$M_s = 5.9$	15.0	4.00	LN			$M_s = 5.9$	15.0	4.00			LZ	$M_s = 5.7$	20.0	4.30	LZ	$M_s = 5.7$	20.0	4.30			
LE	15.0	3.70	15.0	3.70	LN	$M_s = 5.9$	15.0	4.00	LZ	$M_s = 5.7$	20.0	4.30	LZ	$M_s = 5.7$	20.0	4.30								
SSE	57.1 279	-P	13 09 55.0	0.0	15.0	3.70	KMI	72.3 288	+iP	13 11 14.0	0.2	QZN	72.9 279	P	13 11 37.5	0.3								
		PMZ	$m_b = 5.8$	1.3	0.18	PMZ			$m_b = 5.4$	2.0	0.10			sP	13 11 48.0	-2.8	KSH	74.0 316	P	13 11 45.0	1.0			
		PMZ	$m_B = 5.9$	5.0	0.87	PMZ			$m_b = 5.4$	2.0	0.10			sP	13 11 48.0	-2.8			sP	13 11 56.0	-1.3			
		S	13 17 48.0	2.8	15.0	3.70			LN	$M_s = 5.6$	20.0			2.90	PP	13 14 11.0			-3.9	S	13 21 17.0	5.2		
		sS	13 18 03.0	0.9	15.0	3.70			LZ	$M_s = 5.3$	17.0			1.80	S	13 21 17.0			5.2	sS	13 21 27.0	-2.2		
		ScS	13 19 40.0	2.8	15.0	3.70			LZ	$M_s = 5.3$	17.0			1.80	sS	13 21 27.0			-2.2	ScS	13 21 50.0	3.1		
		LE	$M_s = 4.9$	16.0	0.54	LZ			$M_s = 5.3$	17.0	1.80			ScS	13 21 50.0	3.1			LE	$M_s = 6.2$	16.0	6.10		
		LZ	$M_s = 4.9$	20.0	0.92	LZ			$M_s = 5.3$	17.0	1.80			LE	$M_s = 6.2$	16.0			6.10	LZ	$M_s = 6.2$	16.0	6.10	
		+iP	13 09 57.2	0.1	15.0	3.70			LZ	$M_s = 5.3$	17.0			1.80	LZ	$M_s = 6.2$			16.0	6.10	LZ	$M_s = 6.2$	16.0	6.10
		PMZ	$m_b = 5.7$	1.3	0.14	LZ			$M_s = 5.3$	17.0	1.80			LZ	$M_s = 6.2$	16.0			6.10	LZ	$M_s = 6.2$	16.0	6.10	
pP	13 10 08.0	1.4	15.0	3.70	LZ	$M_s = 5.3$	17.0	1.80	LZ	$M_s = 6.2$	16.0	6.10	LZ	$M_s = 6.2$	16.0	6.10								
S	13 17 52.0	2.9	15.0	3.70	LZ	$M_s = 5.3$	17.0	1.80	LZ	$M_s = 6.2$	16.0	6.10	LZ	$M_s = 6.2$	16.0	6.10								
LN	$M_s = 5.6$	15.0	2.20	LZ	$M_s = 5.3$	17.0	1.80	LZ	$M_s = 6.2$	16.0	6.10	LZ	$M_s = 6.2$	16.0	6.10									
LZ	$M_s = 5.6$	16.0	3.58	LZ	$M_s = 5.3$	17.0	1.80	LZ	$M_s = 6.2$	16.0	6.10	LZ	$M_s = 6.2$	16.0	6.10									
NJ2	57.8 281	+P	13 09 59.0	-0.7	15.0	3.70	QZN	72.9 279	P	13 11 37.5	0.3	LSA	75.0 300	P	13 11 50.0	0.3								
		PMZ	$m_b = 5.3$	1.2	0.050	PMZ			$m_b = 5.4$	2.0	0.10			sP	13 11 48.0	-2.8	S	13 21 26.5	4.2					
		PMZ	$m_B = 5.8$	5.0	0.57	PMZ			$m_b = 5.4$	2.0	0.10			eS	13 21 03.5	2.8	LN	$M_s = 5.7$	16.0	1.97				
		S	13 17 58.0	3.9	15.0	3.70			sP	13 11 45.0	-1.9			0.10	sP	13 11 48.0	-2.8	LE	16.0	0.99				
		+P	13 10 25.0	-0.3	15.0	3.70			PP	13 14 11.0	-3.9			0.10	PP	13 14 11.0	-3.9	LZ	$M_s = 5.7$	20.0	4.30			
		PMZ	$m_b = 5.3$	1.2	0.050	LZ			$M_s = 5.3$	17.0	1.80			S	13 20 58.0	6.2	LZ	$M_s = 5.7$	20.0	4.30				
		PMZ	$m_B = 5.8$	5.0	0.57	LZ			$M_s = 5.3$	17.0	1.80			LN	$M_s = 5.8$	10.0	0.60	LZ	$M_s = 5.7$	20.0	4.30			
		S	13 17 58.0	3.9	15.0	3.70			LZ	$M_s = 5.3$	17.0			1.80	LN	$M_s = 5.8$	10.0	0.60	LZ	$M_s = 5.7$	20.0	4.30		
		+P	13 10 25.0	-0.3	15.0	3.70			LZ	$M_s = 5.3$	17.0			1.80	LE	15.0	2.20	LZ	$M_s = 5.7$	20.0	4.30			
		PMZ	$m_b = 5.3$	1.2	0.050	LZ			$M_s = 5.3$	17.0	1.80			LZ	$M_s = 5.7$	20.0	4.30	LZ	$M_s = 5.7$	20.0	4.30			
PMZ	$m_B = 5.9$	5.0	0.71	LZ	$M_s = 5.3$	17.0	1.80	LZ	$M_s = 5.7$	20.0	4.30	LZ	$M_s = 5.7$	20.0	4.30									
WHN	61.5 284	pP	13 10 35.5	0.6	15.0	3.70	KSH	74.0 316	P	13 11 45.0	1.0	QZN	72.9 279	P										



Station	Lat	Lon	Phase	Time	Amplitude	Period	Quality	Station	Lat	Lon	Phase	Time	Amplitude	Period	Quality
KMI	33.6	350	+P	13 31 19.0		1.5		MAY 22d 09h 00m 22.8±0.05s, SD1.57 / 26							
GYA	34.5	356	+iP	13 31 26.0		1.5		29.92 N±0.65km, 90.20 E±0.47km, h34±0.06km							
			PMZ		$m_b = 5.2$		1.2 0.050	Tibet (306)							
			sP	13 31 38.6		2.5		LSA	0.9	105	-iP	09 00 37.0		-2.0	
			PcP	13 34 00.0		1.0					S	09 00 50.5		0.8	
			S	13 36 53.0		3.5					LN			5.0	9.80
			ScP	13 37 39.6		-1.4		GTA	12.3	37	eP	09 03 20.0		0.8	
			ScS	13 41 41.0		-1.3					LE		$M_b = 4.1$	9.0	0.56
WHN	38.8	7	eP	13 32 02.5		1.6					LZ		$M_b = 4.0$	12.0	0.66
CD2	39.1	353	eP	13 32 04.0		0.1		LZH	13.0	58	eP	09 03 31.0		2.9	
			eS	13 38 01.0		-1.3					LN		$M_b = 4.5$	7.0	0.90
SSE	40.7	16	-P	13 32 17.0		0.2					LZ		$M_b = 4.3$	8.0	0.80
			PMZ		$m_b = 5.2$		1.0 0.039	WMQ	14.0	353	P	09 03 39.0		-2.4	
			LN		$M_s = 5.0$		15.0 0.88				eS	09 06 14.0		-2.8	
			LE				16.0 0.91				LZ		$M_b = 3.9$	12.0	0.50
			LZ		$M_s = 4.8$		20.0 1.38	GYA	14.9	99	P	09 03 54.0		0.7	
NJ2	41.0	13	-P	13 32 21.8		2.2					pP	09 04 00.2		-0.4	
			PcP	13 34 20.0		0.8		XAN	16.4	71	P	09 04 12.5		0.2	
			ScP	13 38 04.0		-1.7		BTO	19.3	51	eP	09 04 50.0		1.6	
			eS	13 38 31.0		0.4					esS	09 08 30.0		-1.5	
			LN		$M_s = 5.4$		15.0 2.42				LN		$M_s = 4.4$	14.0	0.80
			LE				15.0 1.22	TIY	20.0	61	eP	09 04 55.8		0.0	
			LZ		$M_s = 4.9$		16.0 1.48				S	09 08 31.5		-1.8	
LSA	41.4	336	P	13 32 22.2		-0.5					sS	09 08 42.0		-4.6	
XAN	41.9	360	+iP	13 32 27.1		0.1					LN		$M_b = 4.3$	11.0	0.51
			PMZ		$m_b = 5.6$		1.0 0.10				LZ		$M_b = 4.2$	14.0	0.71
			S	13 38 38.0		-4.8		BJI	23.5	58	eP	09 05 32.0		1.4	
			LN		$M_s = 5.4$		14.0 1.85				LN		$M_b = 4.3$	12.0	0.42
			LE				14.0 1.74	MAY 22d 11h 37m 47.9±0.09s, SD2.15 / 54							
LZH	44.2	354	P	13 32 46.0		0.0		23.06 N±0.93km, 120.40 E±0.81km, h29±0.06km							
			PMZ		$m_b = 5.3$		1.5 0.073	Taiwan region (243)							
			pP	13 32 54.0		-0.1		$M_s 4.2 / 8, M_L 4.5 / 10, m_b 4.0 / 9$							
			PcP	13 34 31.0		1.1		QZH	2.5	319	Pn	11 38 25.5		-1.6	
			S	13 39 17.5		0.9					Pg	11 38 32.5		0.3	
TIA	44.8	9	eP	13 32 49.2		-0.7					Sn	11 39 03.5		5.4	
			PMZ		$m_b = 5.1$		1.2 0.036				SMN		$M_L = 4.4$	1.0	2.11
TIY	45.7	4	P	13 32 57.3		-0.3					SME			0.8	2.14
GTA	48.1	350	+iP	13 33 16.8		0.6		GZH	6.5	272	P	11 39 26.0		1.8	
			PMZ		$m_b = 5.1$		1.0 0.030				S	11 40 45.0		7.0	
			PcP	13 34 43.0		-0.3					LN		$M_s = 4.6$	4.0	2.02
			ScP	13 38 32.8		-1.6					LE			3.0	0.71
			ScS	13 43 01.0		-2.7		SSE	8.0	5	P	11 39 46.5		0.9	
DL2	48.2	13	eP	13 33 16.0		-1.4					PMZ		$m_b = 5.0$	0.5	0.031
			PMZ		$m_b = 5.5$		1.0 0.070				sP	11 39 54.0		-2.7	
BJI	48.4	7	eP	13 33 18.5		0.0					S	11 41 18.0		1.9	
			PMZ		$m_b = 5.6$		1.0 0.085				SMN		$M_L = 4.4$	1.2	0.093
			PcP	13 34 45.0		0.6					SME			1.0	0.11
			eScS	13 43 05.0		-0.8					LE		$M_s = 4.7$	6.0	2.45
BTO	48.5	1	eP	13 33 20.0		0.5		NJ2	9.1	352	+P	11 40 01.0		1.2	
HHC	48.8	3	P	13 33 22.0		0.2					S	11 41 39.6		-2.1	
SNY	51.5	14	eP	13 33 39.8		-2.3					SMN			1.0	0.33
			PMZ		$m_b = 5.3$		1.1 0.050				SME			1.0	0.26
CN2	53.8	15	+P	13 33 57.4		-2.0					LN			2.5	0.56
			PMZ		$m_b = 5.5$		1.0 0.060				LE			2.5	0.78
			epP	13 34 06.0		-1.8		WHN	9.2	325	+eP	11 40 02.0		0.2	
			PcP	13 35 05.0		0.7					PMZ		$m_b = 4.1$	0.5	0.0030
WMQ	55.2	341	P	13 34 08.3		-1.5					pP	11 40 12.0		3.5	
			PMZ		$m_b = 5.0$		1.0 0.020				S	11 41 48.8		3.5	
			pP	13 34 17.0		-1.1					LN		$M_s = 4.4$	4.0	0.71
			PcP	13 35 06.5		-3.2		QZN	10.6	250	eP	11 40 21.0		-0.7	
			PP	13 36 10.5		-3.4					eS	11 42 22.0		0.9	
			ScP	13 39 04.2		-0.8					LN		$M_s = 4.1$	15.0	1.10
			S	13 41 47.0		-1.8		GYA	12.9	288	P	11 40 56.4		3.6	
			SKS	13 43 51.0		-0.5					pP	11 41 00.8		1.5	
MDJ	55.7	18	eP	13 34 12.0		-1.3									
KSH	56.5	330	eP	13 34 18.0		-1.0									
			pP	13 34 26.0		-1.2									







SME							Philippine Islands region (248)								
MAY 23d 02h 36m 05.4 ± 0.42s, SD3.60 / 6 40.20 N ± 0.89km, 75.70 E ± 4.01km, h37 ± km Southern Xinjiang Province (321) M <sub>L</sub> 3.8 / 5,							M <sub>S</sub> 5.0 / 51, M <sub>L</sub> 4.6 / 7, m <sub>b</sub> 5.4 / 2,								
WMQ	9.6	64	eP	02 38 21.5	-3.4		QZH	4.7	335	ePn	12 53 33.1	-0.7			
										Pg	12 53 48.0	0.3			
										Sn	12 54 23.5	-5.7			
										SMN	M <sub>L</sub> = 4.6	0.7	0.77		
										SME		0.7	1.02		
										LE	M <sub>g</sub> = 4.5	14.0	8.30		
							GZH	7.3	291	+iP	12 54 08.8	-3.3			
										PMZ	m <sub>b</sub> = 5.7	0.6	0.23		
										S	12 55 35.0	0.2			
										LN	M <sub>g</sub> = 4.8	14.0	4.96		
										LE		14.0	8.89		
										LZ	M <sub>g</sub> = 4.8	14.0	8.67		
							SSE	10.4	2	P	12 54 54.3	-0.2			
										sS	12 57 01.0	-0.7			
										LN	M <sub>g</sub> = 4.7	14.0	2.24		
										LE		14.0	3.24		
										LZ	M <sub>g</sub> = 4.5	20.0	4.60		
							QZN	10.4	263	eP	12 54 54.5	-0.7			
										eS	12 56 51.0	-1.2			
										LN	M <sub>g</sub> = 4.9	13.0	4.30		
										LE		14.0	4.40		
							WHN	11.4	331	+P	12 55 06.0	-2.6			
										pP	12 55 13.0	-2.4			
										LN	M <sub>S</sub> = 4.9	18.0	5.29		
										LE		14.0	5.00		
										LZ	M <sub>S</sub> = 4.8	16.0	6.53		
							NJ2	11.5	352	eP	12 55 08.0	-1.2			
										sP	12 55 20.0	-0.6			
										S	12 57 15.0	-2.0			
										LN	M <sub>S</sub> = 4.7	13.0	2.34		
										LE		14.0	2.83		
										LZ	M <sub>S</sub> = 4.2	18.0	1.79		
							GYA	14.2	297	-P	12 55 43.0	-2.5			
										pP	12 55 55.0	2.8			
										SMN		2.0	1.30		
										SME		2.0	0.40		
										LN	M <sub>S</sub> = 5.0	13.0	3.30		
										LE		13.0	3.60		
							TIA	15.8	349	eP	12 56 08.8	2.1			
										sS	12 59 11.0	-1.3			
										LN	M <sub>S</sub> = 4.9	14.0	2.55		
										LE		14.0	2.40		
										LZ	M <sub>S</sub> = 4.7	16.0	3.42		
							XAN	17.0	324	-P	12 56 22.2	0.9			
										PMZ	m <sub>b</sub> = 5.3	1.5	0.20		
										LN	M <sub>S</sub> = 5.1	13.0	5.00		
										LE		10.0	1.70		
							KMI	17.2	288	-P	12 56 24.2	-0.4			
										PMZ	m <sub>b</sub> = 4.7	2.5	0.10		
										pP	12 56 29.0	-2.6			
										S	12 59 35.0	2.2			
										LN	M <sub>S</sub> = 4.7	12.0	0.90		
										LE		8.0	1.10		
										LZ	M <sub>S</sub> = 4.9	15.0	4.30		
							DL2	18.2	2	eP	12 56 37.0	0.5			
										sP	12 56 47.0	-1.3			
										eS	12 59 57.0	1.4			
										sS	13 00 12.0	4.8			
										LN	M <sub>S</sub> = 4.8	12.0	1.97		
										LZ	M <sub>S</sub> = 4.5	18.0	2.11		
							CD2	18.4	307	eP	12 56 38.7	-0.5			
										eS	13 00 03.0	2.6			
										LN	M <sub>S</sub> = 5.2	12.5	5.46		
										LZ	M <sub>S</sub> = 5.1	15.0	6.20		
							TIY	18.5	339	-P	12 56 41.6	1.5			
										LN	M <sub>S</sub> = 5.1	15.0	5.71		
MAY 23d 10h 51m 47.3 ± 0.06s, SD2.75 / 9 40.12 N ± 0.64km, 76.74 E ± 0.60km, h33 ± km Southern Xinjiang Province (321) M <sub>L</sub> 4.0 / 2, m <sub>b</sub> 4.8 / 5,															
KSH	0.9	227	Pg	10 52 00.0	-3.7										
MAY 23d 12h 52m 24.4 ± 0.03s, SD1.24 / 237 20.67 N ± 0.58km, 120.79 E ± 0.80km, h31 ± 0.22km															























			PMZ	$m_B = 7.0$	6.0	32.6		
			pP	20 19 05.0	0.9			
			ScP	20 21 29.0	-2.6			
			iS	20 23 38.0	-4.1			
			SME			10.0	22.9	
GTA	50.2	339	+iP	20 17 28.8	-0.1			
			PMZ	$m_B = 7.3$	5.5	57.5		
			S	20 23 59.0	0.6			
CN2	51.0	5	+iP	20 17 31.8	-2.8			
			PMZ	$m_B = 6.5$	6.0	10.4		
			PcP	20 18 39.0	-1.0			
			pP	20 19 19.0	-1.8			
			ePP	20 19 40.0	-0.7			
			eS	20 24 07.0	-3.4			
			SMN			9.0	12.8	
			SME			9.0	21.3	
			ScS	20 26 21.0	-1.0			
			SS	20 27 55.0	-0.9			
MDJ	52.3	8	+iP	20 17 42.7	-1.0			
			PcP	20 18 44.0	-0.8			
			pP	20 19 31.0	0.3			
			S	20 24 24.0	-2.2			
			SME			11.0	25.8	
			ScS	20 26 32.0	1.1			
			SS	20 28 10.0	-5.2			
WMQ	58.8	333	+iP	20 18 28.0	-1.1			
			S	20 25 48.0	-2.8			

5.46 N ± 0.89km, 31.86 E ± 0.75km, h9 ± 0.03km Sudan (557) $M_S 5.2 / 3, m_b 5.1 / 54,$									
KSH	52.2	43	P	00 51 46.0	0.6				
			sP	00 51 53.0	-0.4				
			S	00 59 09.0	1.5				
			LN	$M_S = 5.4$	14.0	1.60			
WMQ	62.0	43	-P	00 52 54.0	-1.0				
			eS	01 01 16.0	-2.1				
			LZ	$M_S = 4.8$	24.0	0.85			
GTA	69.6	50	-iP	00 53 43.0	-0.7				
			PMZ	$m_b = 5.0$	1.0	0.020			
LZH	72.2	54	eP	00 54 00.0	0.0				
GYA	74.0	64	P	00 54 09.4	-0.8				
XAN	76.2	56	P	00 54 22.0	-1.1				
HHC	78.7	50	P	00 54 38.0	1.4				
TIY	79.2	53	eP	00 54 40.0	0.4				
			pP	00 54 48.0	3.1				
			LN	$M_S = 5.2$	16.0	0.52			
			LZ	$M_S = 5.1$	20.0	1.00			
WHN	80.8	60	eP	00 54 48.0	0.1				
BJI	82.2	50	eP	00 54 55.5	0.4				
			PMZ	$m_b = 5.2$	1.9	0.048			
NJ2	84.6	58	eP	00 55 08.0	0.6				

MAY 24d 22h 16m 02.9 ± 0.04s, SD1.05 / 230 5.46 N ± 0.78km, 31.87 E ± 0.70km, h9 ± 0.05km Sudan (557) $M_S 5.7 / 5, m_B 5.9 / 2, m_b 5.4 / 48$									
KSH	52.2	43	P	22 25 17.0	0.3				
			sP	22 25 27.0	2.3				
			S	22 32 42.0	3.2				
			LN	$M_S = 6.2$	16.0	13.3			
LSA	60.7	59	P	22 26 17.2	-1.0				
WMQ	62.0	43	P	22 26 25.2	-1.1				
			PMZ	$m_b = 5.2$	2.0	0.060			
			PP	22 28 39.0	-5.1				
			eS	22 34 50.5	1.1				
GTA	69.6	50	-P	22 27 14.2	-0.8				
			PMZ	$m_b = 5.7$	2.0	0.17			
KMI	70.4	65	+P	22 27 20.0	-0.3				
			PMZ	$m_b = 5.4$	2.5	0.10			
			PMZ	$m_B = 5.7$	5.0	0.50			
CD2	71.7	59	eP	22 27 28.7	0.8				
LZH	72.2	54	-P	22 27 31.0	-0.3				
			PMZ	$m_b = 5.2$	2.0	0.053			
			pP	22 27 34.5	-2.0				
GYA	74.0	64	+iP	22 27 41.4	-0.1				
BTO	77.5	50	eP	22 28 02.2	0.9				
HHC	78.7	50	P	22 28 09.6	1.7				
			PMZ	$m_b = 5.3$	1.2	0.040			
TIY	79.2	53	-P	22 28 12.0	1.1				
			S	22 38 13.5	5.0				
			LN	$M_S = 5.6$	15.0	1.43			
WHN	80.8	60	eP	22 28 18.0	-1.2				
BJI	82.2	50	eP	22 28 28.0	1.6				
			PMZ	$m_b = 5.5$	2.0	0.088			
TIA	83.0	54	+P	22 28 31.6	0.9				
NJ2	84.6	58	eP	22 28 40.0	1.2				
DL2	86.4	51	eP	22 28 49.3	1.4				
SSE	86.6	59	eP	22 28 50.5	1.6				
SNY	87.7	48	eP	22 28 55.0	1.0				
CN2	88.8	46	eP	22 29 00.0	0.4				

MAY 25d 02h 03m 27.2 ± 0.03s, SD1.34 / 262 2.83 S ± 0.83km, 130.35 E ± 1.04km, h13 ± 0.06km Seram (272) $M_S 5.4 / 53, m_B 5.9 / 10, m_b 5.7 / 64$									
QZN	29.6	318	eP	02 09 35.0	0.0				
			S	02 14 28.0	-0.1				
			LN	$M_S = 5.6$	14.0	7.02			
			LE		10.0	1.70			
QZH	29.9	338	eP	02 09 40.0	3.0				
			S	02 14 33.0	1.2				
			LN	$M_S = 5.2$	13.0	2.98			
GZH	30.6	328	-P	02 09 44.6	0.8				
			S	02 14 46.0	2.2				
			LN	$M_S = 5.3$	11.0	2.36			
			LE		11.0	1.42			
			LZ	$M_S = 5.0$	29.0	5.29			
SSE	34.8	346	+P	02 10 20.0	-0.5				
			PMZ	$m_b = 5.4$	1.0	0.068			
			pP	02 10 25.0	-1.5				
			sP	02 10 30.0	0.6				
			PcP	02 12 54.0	1.0				
			S	02 15 50.0	0.6				
			LN	$M_S = 5.2$	13.0	1.34			
			LE		11.0	1.14			
			LZ	$M_S = 4.8$	20.0	1.84			
NJ2	36.4	343	+P	02 10 33.8	0.4				
			PP	02 11 58.8	2.7				
			ScP	02 16 45.4	3.1				
			S	02 16 15.0	2.1				
			LN	$M_S = 5.2$	11.0	1.39			
			LE		10.0	1.04			
			LZ	$M_S = 4.9$	20.0	2.14			
WHN	36.5	336	-P	02 10 35.0	0.3				
			PMZ	$m_b = 5.6$	1.0	0.10			
			PMZ	$m_B = 5.9$	4.0	0.92			
			pP	02 10 44.0	3.3				
			eS	02 16 16.0	-0.3				
			LE	$M_S = 5.3$	12.0	2.49			
			LZ	$M_S = 5.0$	20.0	2.50			
GYA	37.0	323	+iP	02 10 40.0	0.8				
			PMZ	$m_b = 5.8$	1.2	0.20			
			pP	02 10 46.0	1.0				
			PcP	02 13 00.8	1.3				

MAY 25d 00h 42m 31.6 ± 0.05s, SD1.08 / 194



		S	02 16 24.0	0.8				eS	02 18 46.0	0.3		
		ScP	02 16 47.8	3.0				SS	02 22 04.0	0.7		
		PcS	02 16 51.0	4.5				LN	$M_s = 5.6$	18.0	4.00	
		ScS	02 20 53.0	2.2				LE		18.0	1.50	
		LN	$M_s = 5.6$	15.0	4.50			LZ	$M_s = 5.5$	20.0	5.60	
		LE		15.0	2.50	HHC	46.7 340	eP	02 11 58.0	-0.5		
		LZ	$M_s = 4.8$	20.0	1.60			S	02 18 50.0	3.8		
KMI	38.6 318	+P	02 10 53.0	0.6				SMN		7.0	0.66	
		PMZ	$m_b = 6.0$	1.5	0.40			SME		7.0	1.10	
		PMZ	$m_b = 6.1$	4.0	1.30			LN	$M_s = 5.4$	14.0	2.13	
		S	02 16 46.0	-1.1				LZ	$M_s = 5.3$	30.0	5.45	
		LN	$M_s = 5.4$	13.0	2.30	BTO	47.0 339	P	02 12 01.0	0.1		
		LE		10.0	0.80			pP	02 12 10.5	3.6		
		LZ	$M_s = 5.3$	18.0	3.90			S	02 18 52.0	1.3		
TIA	40.8 344	eP	02 11 09.0	-1.0				SS	02 22 14.0	3.4		
		LN	$M_s = 5.2$	9.0	1.24			LN	$M_s = 5.4$	15.0	0.80	
		LZ	$M_s = 6.0$	20.0	20.0			LE		15.0	2.40	
XAN	41.9 333	P	02 11 18.2	-1.0				LZ	$M_s = 4.9$	15.0	1.10	
		S	02 17 34.2	-1.6				MDJ	47.2 359	-iP	02 12 02.0	-0.3
		LN	$M_s = 5.4$	13.0	2.30			PcP	02 13 36.0	2.8		
		LE		12.0	1.10			S	02 18 55.0	1.6		
CD2	42.0 325	P	02 11 20.2	-0.5				LN	$M_s = 5.2$	12.0	1.14	
		PMZ	$m_b = 5.4$	1.0	0.070			LZ	$M_s = 5.3$	33.0	5.01	
		S	02 17 38.0	-0.5				LSA	49.5 314	P	02 12 19.2	-1.3
		LN	$M_s = 5.5$	12.0	2.56			PMZ		3.0	0.76	
		LZ	$M_s = 5.1$	18.0	2.27			pP	02 12 29.0	3.0		
DL2	42.3 350	-P	02 11 24.0	1.3				PP	02 14 09.0	-5.1		
		S	02 17 43.0	0.8				S	02 19 25.0	-0.3		
		LN	$M_s = 5.4$	17.0	2.43			SMN		6.0	0.69	
		LE		15.0	2.00			SME		7.0	0.51	
		LZ	$M_s = 5.1$	18.0	2.42	GTA	50.5 329	-iP	02 12 27.2	-0.9		
TIY	43.6 339	-P	02 11 32.9	-0.7				PMZ	$m_b = 5.7$	1.0	0.12	
		PMZ	$m_b = 5.8$	0.8	0.13			ScP	02 17 42.2	2.9		
		S	02 18 00.0	-1.6				S	02 19 40.0	0.4		
		LE	$M_s = 5.4$	13.0	2.05			ScS	02 22 18.2	3.5		
		LZ	$M_s = 5.1$	27.0	3.35			LN	$M_s = 5.2$	12.0	1.03	
BJI	44.6 344	eP	02 11 40.5	-0.9				LZ	$M_s = 5.4$	20.0	3.90	
		PMZ	$m_b = 5.7$	1.0	0.12	WMQ	60.1 326	P	02 13 36.2	-1.3		
		PMZ	$m_b = 5.7$	4.0	0.48			iS	02 21 49.0	-0.1		
		PcP	02 13 22.5	-1.5				SME		7.0	0.65	
		ScP	02 17 12.0	-2.4				ScS	02 23 25.0	2.0		
		eS	02 18 16.0	-0.6				LZ	$M_s = 5.3$	22.0	2.34	
		LN	$M_s = 5.2$	14.0	1.38	KSH	65.3 316	eP	02 14 12.0	0.3		
		LZ	$M_s = 5.0$	24.0	2.29			PP	02 16 35.0	-1.3		
SNY	44.9 353	-P	02 11 42.0	-1.6				S	02 22 56.0	3.8		
		PMZ	$m_b = 5.8$	0.8	0.12			sS	02 23 03.0	-0.7		
		pP	02 11 52.2	2.6				LE	$M_s = 5.7$	16.0	2.40	
		iS	02 18 16.0	-4.6								
		SMN		9.5	0.97			MAY 25d 16h 21m 46.8 ± 0.04s, SD1.66 / 79				
		SME		11.5	1.12			37.32 N ± 0.93km, 72.97 E ± 0.65km, h82 ± 0.27km				
		sS	02 18 36.0	5.2				Afghanistan-USSR border region (717)				
		ScS	02 21 40.0	2.5				$M_s 5.1 / 23, m_b 4.7 / 17,$				
		LN	$M_s = 5.7$	18.0	5.28	KSH	3.2 46	P	16 22 39.0	2.7		
		LE		14.0	1.01			S	16 23 13.0	-0.1		
		LZ	$M_s = 5.6$	20.0	7.15			LN	$M_s = 5.1$	5.0	21.7	
LZH	46.0 330	+P	02 11 52.0	-0.4				WMQ	12.9 55	P	16 24 48.3	-0.8
		PMZ	$m_b = 6.0$	4.0	0.96			S	16 27 10.0	-1.1		
		PP	02 13 40.0	0.4				LN	$M_s = 5.1$	8.0	4.33	
		S	02 18 34.0	-1.1				LZ	$M_s = 4.6$	17.0	3.48	
		sS	02 18 49.0	2.7				GTA	21.1 76	+iP	16 26 27.0	-0.2
		ScS	02 21 45.0	0.6				PMZ	$m_b = 4.9$	0.8	0.050	
		LN	$M_s = 5.5$	13.0	2.00			LN	$M_s = 4.9$	12.0	2.07	
		LE		12.0	1.50			LZ	$M_s = 4.8$	18.0	2.94	
		LZ	$M_s = 5.2$	25.0	3.20	LZH	24.7 83	eP	16 27 03.0	0.6		
CN2	46.6 355	P	02 11 56.9	-0.6				PMZ	$m_b = 4.9$	2.5	0.12	
		PMZ	$m_b = 5.9$	1.0	0.20			PP	16 27 38.0	-3.9		
		PMZ	$m_b = 5.9$	4.0	0.70			eS	16 31 20.0	3.9		
		pP	02 12 06.0	2.5				sS	16 31 42.0	-5.5		



CD2	26.2	95	LN	$M_s = 5.0$	9.0	1.30	BJI	36.4	318	eP	18 35	56.0	-0.5	1.4	0.033	
			LE		12.0	1.70					PMZ		$m_b = 5.0$			
			LZ	$M_s = 4.8$	20.0	2.90	TIY	37.8	312	eP	18 36	09.7	1.2			
KMI	28.1	107	eP	16 27	18.8	2.7				LZ		$M_s = 4.6$	15.0	0.71		
			LN		$M_s = 5.1$	11.0	2.17	GYA	39.3	293	P	18 36	23.0	1.8		
			LZ		$M_s = 4.8$	8.0	1.06	BTO	40.8	315	eP	18 36	33.0	-0.1		
BTO	28.9	72	eP	16 27	34.5	1.1	CD2	42.6	299	P	18 36	47.8	0.1			
			S	16 32	16.0	6.0	KMI	42.7	290	+P	18 36	50.0	0.7			
			LN		$M_s = 4.8$	10.0	0.60	LZH	43.7	306	-P	18 36	57.5	0.5		
XAN	29.3	86	LE			8.0				PMZ		$m_b = 5.4$	2.0	0.12		
			LZ		$M_s = 4.7$	14.0	1.30				LZ		$M_s = 4.2$	20.0	0.30	
			eP	16 27	39.0	-1.2	LSA	53.3	295	P	18 38	12.1	0.6			
HHC	30.0	71	S	16 32	27.0	4.8	WMQ	57.5	312	-iP	18 38	41.6	-0.1			
			LN		$M_s = 5.4$	15.0	2.30				sP	18 38	55.3	-0.5		
			LE			15.0	4.70				eS	18 46	33.3	-1.8		
GYA	30.4	101	LZ		$M_s = 5.3$	15.0	4.80				LZ		$M_s = 4.5$	16.0	0.35	
			eP	16 27	42.6	-1.3	KSH	66.0	307	eP	18 39	39.9	1.2			
			LN		$M_s = 5.0$	14.0	1.00	<hr/> <p>MAY 25d 20h 38m 04.8 ± 0.06s, SD3.42 / 10 43.87 N ± 0.75km, 82.20 E ± 0.69km, h17 ± 0.61km Northern Xinjiang Province (332) <math>M_L 3.7 / 6,</math></p>								
TIY	31.2	77	LE			13.0	1.60	WMQ	4.0	89	ePn	20 39	09.1	3.4		
			eP	16 27	50.0	-0.4				Sg	20 40	10.0	0.4			
			S	16 32	44.0	3.7				SMN		$M_L = 3.7$	0.5	0.15		
BJI	33.6	72	LN		$M_s = 5.1$	12.0	1.70				SME			0.5	0.17	
			LE			12.0	0.82	GTA	13.9	103	eP	20 41	21.8	-2.1		
			LZ		$M_s = 5.1$	18.0	3.63	<hr/> <p>MAY 26d 02h 57m 34.7 ± 0.04s, SD1.51 / 153 1.35 N ± 0.79km, 123.41 E ± 1.17km, h32 ± 0.04km Minahassa Peninsula (Celebes) (265) <math>M_s 5.4 / 56, m_b 5.7 / 21, m_b 5.2 / 39</math></p>								
KSH	3.2	43	P	16 26	18.0	-2.7	QZN	22.0	324	-P	03 02	27.5	-0.9			
			S	16 26	56.0	-1.0				pP	03 02	37.0	-0.1			
			LN		$M_s = 5.1$	4.0	16.0				sP	03 02	41.0	-0.2		
GTA	21.0	76	-iP	16 30	12.6	0.6				S	03 06	24.0	0.0			
			PMZ		$m_b = 4.9$	1.0	0.060				sS	03 06	39.0	0.2		
			LN		$M_s = 4.9$	11.0	2.01				LN		$M_s = 5.4$	15.0	6.13	
LZH	24.6	83	LZ		$M_s = 4.6$	18.0	2.06	GZH	23.7	336	+P	03 02	46.2	1.3		
			-P	16 30	46.0	-1.1				LN		$M_s = 5.4$	13.0	5.33		
			PMZ		$m_b = 4.8$	2.0	0.085				LE			12.0	2.62	
BTO	28.8	72	eP	16 31	21.5	-3.7	QZH	23.9	349	-P	03 02	47.0	0.2			
			P	16 31	38.8	-0.2				PMZ		$m_b = 5.9$	5.0	2.23		
			eP	16 31	45.4	0.0				S	03 06	58.0	0.5			
TIY	31.1	77	eP	16 32	07.0	0.3				LN		$M_s = 5.2$	12.0	2.05		
			eS	16 37	27.0	4.5				LE			12.0	2.45		
			LN		$M_s = 4.9$	12.0	0.97	SSE	29.7	356	eP	03 03	39.0	-0.9		
BJI	33.5	72	LZ		$M_s = 5.2$	18.0	3.82				PMZ		$m_b = 4.8$	1.0	0.019	
			eP	16 32	41.0	-1.2				PMZ		$m_b = 5.7$	4.0	0.64		
			eP	16 32	49.8	-1.0				S	03 08	30.0	-1.5			
NJ2	37.7	84	LN		$M_s = 4.9$	12.0	0.97				LN		$M_s = 5.1$	13.0	2.05	
			LZ		$M_s = 5.2$	18.0	3.82				LE			12.0	1.22	
			eP	16 32	41.0	-1.2				LZ		$M_s = 5.0$	20.0	3.68		
SNY	38.7	67	eP	16 32	49.8	-1.0	GYA	29.7	329	P	03 03	40.0	-0.5			
										pP	03 03	50.4	1.0			
										S	03 08	36.0	3.7			
SSE	28.4	307	P	18 34	45.5	-1.3				LN		$M_s = 5.4$	13.0	3.20		
			eP	18 35	03.8	-2.7				LE			13.0	2.50		
			pP	18 35	15.5	-0.6				LZ		$M_s = 4.8$	18.0	2.10		
SNY	33.1	326	eP	18 35	25.3	-3.1	WHN	30.3	344	eP	03 03	46.5	1.1			
			-P	18 35	32.5	-0.3				pP	03 03	56.0	1.5			
			eP	18 35	32.5	-0.4				eS	03 08	41.5	-0.6			
CN2	33.6	331	-P	18 35	32.5	-0.3				LN		$M_s = 5.6$	15.0	6.84		
			eP	18 35	32.5	-0.4				LE			12.0	2.49		
										LZ		$M_s = 5.3$	17.0	5.99		
WHN	33.6	302	eP	18 35	32.5	-0.4	NJ2	30.8	352	-P	03 03	51.0	0.6			







		PMZ		$m_b = 5.4$	1.0	0.10	GYA	20.0	316	P	13 30	29.0	-0.5					
		pP	08 03	10.8	1.4					pP	13 30	39.0	1.0					
		PP	08 03	18.0	1.6					S	13 34	14.0	6.9					
		LN		$M_s = 4.3$	9.0	0.54				LN		$M_s = 4.9$	16.0	2.30				
		LE			7.0	0.45				LE			16.0	2.60				
		LZ		$M_s = 3.8$	12.0	0.45				LZ		$M_s = 4.7$	18.0	2.80				
BTO	16.1	86	eP	08 03	49.0	2.0	KMI	22.1	308	+P	13 30	53.0	2.3					
			LN		$M_s = 4.0$	8.0	0.20			PMZ		$m_b = 5.0$	2.5	0.18				
			LE			8.0	0.20			pP	13 31	01.5	1.9					
CD2	16.1	126	P	08 03	50.4	3.2			sP	13 31	06.0	2.1						
HHC	17.2	85	+P	08 04	02.0	0.9			LN		$M_s = 4.6$	11.0	0.90					
XAN	17.6	109	P	08 04	04.3	-2.0			LZ		$M_s = 4.8$	20.0	3.20					
TIY	18.7	94	eP	08 04	19.0	-0.1	TIA	24.1	350	eP	13 31	10.3	0.4					
			LE		$M_s = 4.1$	8.0	0.28			S	13 35	26.0	4.4					
			LZ		$M_s = 4.4$	11.0	0.87			LE		$M_s = 4.5$	14.0	0.80				
KMI	20.1	140	-P	08 04	35.5	-0.4			LZ		$M_s = 4.5$	20.0	1.50					
BJI	20.8	85	eP	08 04	44.0	0.8	XAN	24.6	333	P	13 31	13.5	-1.2					
			PMZ		$m_b = 5.3$	0.7	0.088			S	13 35	34.0	4.1					
GYA	21.1	130	P	08 04	46.4	0.0			LN		$M_s = 4.8$	15.0	1.63					
TIA	22.7	94	eP	08 05	03.3	1.1	CD2	24.9	320	eP	13 31	16.8	-1.1					
WHN	23.4	110	+P	08 05	10.5	1.7			S	13 35	38.0	2.4						
			PMZ		$m_b = 5.6$	0.5	0.12			LN		$M_s = 4.9$	17.5	2.54				
DL2	25.2	85	P	08 05	27.6	1.3			LZ		$M_s = 4.8$	20.0	2.55					
			PMZ		$m_b = 5.6$	1.0	0.16	DL2	26.4	359	eP	13 31	31.0	-0.7				
NJ2	25.8	102	eP	08 05	33.0	0.7			eS	13 36	00.0	-0.7						
			LZ		$M_s = 3.9$	20.0	0.31			sS	13 36	20.0	3.7					
SNY	25.9	78	+P	08 05	33.6	0.3			LN		$M_s = 4.8$	16.0	1.28					
			PMZ		$m_b = 5.5$	0.8	0.090			LE			16.0	1.26				
			eS	08 10	01.5	-1.1			LZ		$M_s = 4.2$	20.0	0.60					
			LZ		$M_s = 4.2$	20.0	0.61	TIY	26.6	343	eP	13 31	33.0	-0.6				
CN2	27.0	73	P	08 05	42.8	0.0			S	13 36	04.0	0.8						
			eS	08 10	20.0	0.4			LN		$M_s = 5.0$	17.0	3.08					
			LZ		$M_s = 4.3$	16.0	0.60			LZ		$M_s = 5.0$	18.0	3.41				
SSE	28.0	101	eP	08 05	52.7	0.2			BJI	28.0	351	eP	13 31	46.0	-0.3			
			PMZ		$m_b = 5.0$	1.0	0.029			PMZ		$m_b = 4.9$	1.5	0.039				
			sS	08 10	44.0	0.8			eS	13 36	26.0	-0.6						
			LZ		$M_s = 4.1$	20.0	0.46			LN		$M_s = 4.4$	15.0	0.61				
QZN	28.8	135	eP	08 05	59.4	0.0			LZ		$M_s = 4.2$	20.0	0.54					
MDJ	29.8	70	eP	08 06	08.0	-0.4			LZH	28.7	328	P	13 31	51.6	-0.9			
										PMZ		$m_b = 5.0$	1.8	0.061				
										PMZ		$m_b = 5.3$	4.0	0.24				
										pP	13 32	02.0	0.3					
										sP	13 32	08.5	2.6					
										eS	13 36	37.0	-0.8					
										LN		$M_s = 5.0$	15.0	1.48				
										LE			15.0	1.71				
										LZ		$M_s = 4.8$	22.0	2.33				
										SNY	29.3	3	+P	13 31	59.0	0.6		
										sP	13 32	13.0	1.0					
										eS	13 36	48.0	-0.3					
										LN		$M_s = 4.8$	15.0	0.83				
										LE			14.0	0.94				
										LZ		$M_s = 4.7$	16.0	1.52				
										HHC	29.7	344	eP	13 32	01.0	-1.2		
										eS	13 36	58.0	2.8					
										LN		$M_s = 4.7$	17.0	0.35				
										LE			16.0	1.10				
										BTO	30.0	342	eP	13 32	06.0	1.9		
										eS	13 37	00.0	1.5					
										LN		$M_s = 5.2$	17.0	1.90				
										LE			17.0	2.80				
										LZ		$M_s = 4.9$	17.0	2.40				
										CN2	31.4	5	eP	13 32	16.0	-0.9		
										epP	13 32	27.0	0.7					
										eS	13 37	19.0	-2.2					
										LN		$M_s = 5.0$	16.0	1.70				
										LE			16.0	0.50				
										LZ		$M_s = 4.6$	22.0	1.50				

MAY 26d 13h 25m  $56.3 \pm 0.04s$ , SD1.36 / 119  
 12.42 N  $\pm 0.68km$ , 121.93 E  $\pm 0.87km$ , h35  $\pm 0.08km$   
 Panay (254)

$M_s 4.8 / 40$ ,  $m_b 5.1 / 5$ ,  $m_b 4.8 / 26$

QZN	13.4	301	eP	13 29	06.5	0.3									
			LN		$M_s = 4.8$	15.0	2.50								
			LE			18.0	3.90								
SSE	18.6	358	P	13 30	13.0	-0.1									
			PMZ			3.0	0.41								
			sP	13 30	26.0	0.3									
			S	13 33	36.0	0.4									
			SS	13 33	59.0	-1.2									
			LN		$M_s = 4.6$	15.0	1.14								
			LE			15.0	1.15								
			LZ		$M_s = 4.2$	20.0	1.20								
WHN	19.4	340	eP	13 30	18.5	-3.4									
			pP	13 30	28.4	-1.6									
			eS	13 33	59.0	6.0									
			LN		$M_s = 5.0$	15.0	3.65								
			LZ		$M_s = 4.8$	16.0	2.97								
NJ2	19.7	352	-P	13 30	28.0	1.8									
			PMZ		$m_b = 5.1$	4.5	0.43								
			pP	13 30	37.2	2.5									
			sP	13 30	42.0	2.7									
			S	13 34	01.5	0.3									
			LN		$M_s = 4.7$	15.0	1.61								
			LE			14.0	0.76								
			LZ		$M_s = 4.3$	20.0	1.22								





















Station	Mag	Depth (km)	Type	Time	Mag	Depth (km)	Type	Time	Mag	Depth (km)	Type	Time	Mag	Depth (km)	Type	Time				
MDJ	55.0	49	+P	21 59 03.7	-2.1															
			PMZ		$m_b = 5.7$		1.8	0.18												
			PP	22 01 10.0	0.5															
			eS	22 06 45.0	0.3															
			LN		$M_s = 5.6$		16.0	2.90												
BJI	56.4	62	LZ		$M_s = 5.4$		24.0	4.00												
			eP	21 59 16.0	0.4															
			PMZ		$m_b = 5.7$		1.6	0.17												
			PMZ		$m_B = 5.9$		5.0	0.81												
			ePcP	22 00 15.0	3.2															
SNY	56.4	55	ePP	22 01 24.0	2.1															
			eS	22 07 04.0	1.1															
			eSS	22 10 51.0	2.0															
			LN		$M_s = 5.7$		14.0	1.98												
			LE				14.0	1.99												
			LZ		$M_s = 5.7$		20.0	6.28												
			-iP	21 59 14.0	-1.7															
			PMZ		$m_b = 5.2$		1.2	0.040												
			sP	21 59 28.0	-0.2															
			S	22 07 08.0	6.1															
LZH	57.0	74	SME				11.0	0.58												
			SS	22 10 50.0	0.8															
			LN		$M_s = 5.8$		15.0	2.25												
			LE				17.5	3.64												
			LZ		$M_s = 5.6$		21.0	5.22												
			-iP	21 59 20.5	0.2															
			PMZ		$m_b = 5.9$		2.5	0.39												
			PMZ		$m_B = 6.1$		5.0	1.24												
			pP	21 59 26.5	-2.4															
			sP	21 59 31.0	-1.6															
TIY	57.6	66	PP	22 01 28.5	0.9															
			S	22 07 12.0	2.1															
			SME				15.0	2.56												
			SME				10.0	1.47												
			SS	22 11 01.0	1.3															
			LN		$M_s = 6.2$		18.0	10.1												
			LE				14.0	3.98												
			LZ		$M_s = 6.1$		20.0	14.7												
			-P	21 59 25.0	0.1															
			S	22 07 20.0	1.3															
DL2	58.7	57	sS	22 07 29.0	-5.4															
			LN		$M_s = 5.8$		16.0	4.42												
			LZ		$M_s = 5.7$		18.0	6.08												
			eP	21 59 31.0	-1.3															
			pP	21 59 42.0	0.9															
LSA	59.6	89	SME				12.0	1.01												
			LN		$M_s = 6.1$		16.0	7.03												
			LZ		$M_s = 5.7$		20.0	6.04												
			P	21 59 39.4	0.5															
			sP	21 59 52.0	1.1															
TIA	60.2	62	PP	22 01 52.0	0.9															
			S	22 07 50.0	5.9															
			SME				7.0	1.13												
			SME				15.0	2.65												
			LN		$M_s = 5.5$		14.0	1.59												
XAN	60.2	70	-P	21 59 42.0	-0.7															
			PMZ		$m_b = 5.9$		2.5	0.37												
			PMZ		$m_B = 5.9$		5.5	0.90												
			sP	21 59 56.5	1.3															
			LN		$M_s = 5.8$		14.0	2.60												
CD2	61.9	76	LE				14.0	2.20												
			LZ		$M_s = 5.5$		20.0	4.00												
			P	21 59 42.3	-0.6															
			PMZ		$m_B = 5.9$		5.0	0.71												
			PP	22 01 56.0	-0.9															
GTA	61.9	76	LN		$M_s = 5.9$		14.0	3.77												
			LE				16.0	2.91												
			-iP	21 59 53.8	0.0															
NJ2	64.6	62	-P	22 00 09.5	-2.4															
			PP	22 02 40.0	4.8															
			S	22 08 50.0	2.7															
			LN		$M_s = 5.8$		15.0	2.82												
			LE				14.0	1.14												
WHN	64.9	67	LZ		$M_s = 5.4$		18.0	2.39												
			eP	22 00 13.0	-1.1															
			PMZ		$m_B = 5.8$		5.0	0.57												
			sP	22 00 26.0	-0.7															
			eS	22 08 56.0	3.4															
SSE	66.1	60	LN		$M_s = 5.8$		13.0	2.97												
			LZ		$M_s = 5.5$		20.0	3.13												
			P	22 00 20.5	-0.9															
			PMZ		$m_b = 5.8$		2.0	0.26												
			PMZ		$m_B = 5.9$		4.0	0.64												
GYA	66.9	75	S	22 09 07.0	1.7															
			SS	22 13 22.0	-0.3															
			LE		$M_s = 6.1$		18.0	6.82												
			LZ		$M_s = 5.7$		20.0	4.51												
			-P	22 00 26.0	-0.4															
KMI	67.1	79	pP	22 00 33.0	-2.2															
			S	22 09 17.0	2.4															
			sS	22 09 26.0	-4.6															
			LN		$M_s = 5.7$		20.0	3.00												
			LE				20.0	1.00												
QZH	71.4	64	LZ		$M_s = 5.4$		28.0	3.60												
			+P	22 00 27.5	-0.3															
			PMZ		$m_b = 5.9$		1.5	0.25												
			pP	22 00 37.5	1.1															
			iS	22 09 25.0	6.1															
GZH	71.8	70	LN		$M_s = 5.8$		17.0	2.80												
			LE				17.0	2.20												
			LZ		$M_s = 6.1$		20.0	11.0												
			eP	22 00 52.0	-2.0															
			S	22 10 12.0	4.2															
QZN	74.8	74	P	22 00 58.0	1.3															
			S	22 10 16.0	2.9															
			LN		$M_s = 6.2$		17.0													



BTO	6.3	118	Pn	03 43	55.7	3.4		
			Pg	03 44	14.7	2.4		
			Sg	03 45	37.6	-0.5		
			SMN		$M_L=4.4$	1.0	0.19	
			SME			1.0	0.28	
HHC	7.2	111	Pn	03 44	07.0	2.5		
			Sn	03 45	26.6	0.0		
			SMN		$M_L=4.6$	1.0	0.25	
			SME			1.0	0.28	
LZH	7.8	174	ePn	03 44	15.0	2.2		
			eSn	03 45	40.5	-0.9		
			SMN		$M_L=4.9$	1.5	0.25	
			SME			1.5	0.47	
			LN		$M_S=4.2$	7.0	1.11	
			LZ		$M_S=4.0$	10.0	1.04	
CD2	12.9	176	eP	03 45	29.3	3.8		
GYA	17.6	168	P	03 46	30.4	4.2		

MAY 28d 07h 15m  $50.6 \pm 0.05s$ ,  $SD1.82 / 45$   
 $37.70 N \pm 0.78km$ ,  $73.42 E \pm 0.71km$ ,  $h33 \pm 0.05km$   
 Tadjhikistan (715)  
 $M_S4.1 / 4$ ,  $M_L4.9 / 1$ ,  $m_b4.6 / 12$

KSH	2.7	46	Pn	07 16	35.0	3.1		
WMQ	12.4	56	P	07 18	47.5	-0.7		
			eS	07 21	05.5	-1.2		
			LN		$M_S=4.3$	5.0	0.42	
			LZ		$M_S=4.1$	10.0	0.75	
GTA	20.7	77	+P	07 20	30.2	-0.6		
			PMZ		$m_b=4.4$	0.8	0.015	
			LE		$M_S=4.0$	9.0	0.22	
LZH	24.3	84	-P	07 21	08.0	1.0		
			PMZ		$m_b=4.8$	1.8	0.061	
			pP	07 21	16.0	0.4		
			sP	07 21	21.0	1.4		
			LE		$M_S=4.1$	10.0	0.23	
			LZ		$M_S=4.0$	16.0	0.39	
CD2	25.9	96	eP	07 21	21.7	0.1		
XAN	28.9	86	eP	07 21	47.5	-1.5		
GYA	30.2	102	P	07 22	00.6	0.2		
TIY	30.7	78	P	07 22	10.2	5.0		
			LZ		$M_S=4.3$	18.0	0.61	
SNY	38.3	68	eP	07 23	10.2	-0.3		
			esP	07 23	24.6	0.9		
			eS	07 29	03.0	0.3		
			LZ		$M_S=4.4$	14.0	0.41	

MAY 28d 10h 59m  $35.0 \pm 0.17s$ ,  $SD2.89 / 11$   
 $40.15 N \pm 1.11km$ ,  $76.11 E \pm 0.71km$ ,  $h27 \pm 1.06km$   
 Southern Xinjiang Province (321)  
 $M_S4.1 / 1$ ,  $M_L3.8 / 5$ ,

KSH	0.7	193	Pg	10 59	47.5	0.0		
			Sg	10 59	59.5	2.7		
WMQ	9.4	63	eP	11 01	55.5	3.9		
			S	11 03	42.5	5.6		
			LN		$M_S=4.1$	4.0	0.32	
GTA	18.2	85	eP	11 03	44.4	-3.7		

MAY 28d 11h 28m  $47.5 \pm 0.03s$ ,  $SD0.94 / 374$   
 $20.84 S \pm 0.74km$ ,  $177.98 W \pm 0.68km$ ,  $h486 \pm 0.27km$   
 Fiji region (181)  
 $m_b5.8 / 18$ ,  $m_b5.9 / 80$ ,

QZH	76.6	303	-P	11 39	49.5	0.3		
			PMZ		$m_b=6.1$	1.0	0.75	
SSE	77.9	310	-iP	11 39	56.4	0.1		
			PMZ		$m_b=5.3$	1.0	0.14	
			PMZ		$m_b=5.4$	4.0	0.56	
			sP	11 42	32.0	1.2		
			eS	11 49	08.0	-2.0		

GZH	79.9	299	-P	11 40	07.4	0.6		
NJ2	80.1	310	-iP	11 40	08.5	0.6		
			PMZ		$m_b=6.1$	2.0	1.33	
			sP	11 42	44.0	1.2		
			S	11 49	37.0	6.0		
MDJ	80.8	325	-P	11 40	11.5	0.0		
			PMZ		$m_b=5.9$	1.2	0.56	
			PMZ		$m_b=5.9$	4.0	2.05	
			pP	11 42	02.0	4.4		
			sP	11 42	50.0	3.4		
			IS	11 49	44.0	4.3		
			SME			6.0	2.11	
QZN	81.0	294	-P	11 40	12.5	-0.1		
			PP	11 43	27.0	0.1		
			eS	11 49	37.5	-4.3		
DL2	82.0	317	-iP	11 40	17.0	-0.6		
			PMZ		$m_b=6.0$	1.0	0.50	
			PMZ		$m_b=5.7$	5.0	1.49	
			sP	11 42	56.0	3.1		
			S	11 49	47.0	-2.9		
SNY	82.5	320	-iP	11 40	19.0	-1.0		
			PMZ		$m_b=5.7$	1.0	0.24	
			PMZ		$m_b=5.7$	5.0	1.48	
			sP	11 42	56.0	0.6		
			PP	11 43	36.0	-2.5		
			SKS	11 49	51.5	0.6		
			S	11 49	57.5	2.7		
			SS	11 55	34.0	0.8		
CN2	82.6	322	-iP	11 40	20.0	-0.5		
			PMZ		$m_b=6.0$	1.0	0.50	
			PMZ		$m_b=6.0$	4.0	2.30	
			pP	11 42	08.0	0.9		
			sP	11 42	57.0	1.0		
			S	11 49	55.0	-0.7		
			SMN			7.0	0.30	
			SME			7.0	0.80	
WHN	82.7	306	eP	11 40	21.0	0.1		
			PMZ		$m_b=5.6$	1.0	0.23	
TIA	83.5	313	-P	11 40	24.9	-0.4		
			PMZ		$m_b=5.9$	1.6	0.60	
			PMZ		$m_b=5.8$	4.0	1.16	
			S	11 50	00.0	-4.9		
BJI	86.1	315	-eP	11 40	37.0	-1.0		
			PMZ		$m_b=6.0$	1.5	0.58	
			PMZ		$m_b=5.9$	4.0	1.21	
			pP	11 42	26.0	0.5		
			esP	11 43	16.0	1.8		
			eSKS	11 50	15.0	-0.3		
			eS	11 50	29.0	-2.6		
GYA	86.8	300	P	11 40	42.0	0.5		
			PMZ		$m_b=5.8$	1.2	0.30	
			sP	11 43	22.0	4.4		
			SKS	11 50	22.0	2.2		
TIY	87.5	312	-iP	11 40	44.5	-0.2		
			PMZ		$m_b=6.0$	1.2	0.40	
			PMZ		$m_b=6.1$	4.0	1.59	
			PP	11 44	22.5	3.2		
			SKS	11 50	24.5	0.5		
			S	11 50	45.0	2.3		
XAN	88.3	307	P	11 40	48.6	0.0		
			PMZ		$m_b=5.8$	1.2	0.25	
			PMZ		$m_b=6.1$	4.0	1.45	
			pP	11 42	42.0	5.5		
			sP	11 43	30.0	5.0		
			SKS	11 50	28.0	-1.2		
KMI	89.5	297	-iP	11 40	55.0	0.8		
			PMZ		$m_b=6.2$	2.0	0.93	
			pP	11 42	46.0	3.8		













		PMZ	$m_b = 5.3$	4.0	0.60			LN	$M_s = 4.9$	15.0	1.50
		pP	12 39 53.5	-1.6				LE		15.0	0.90
		sP	12 39 56.5	-4.2				LZ	$M_s = 4.7$	15.0	1.50
		PP	12 40 07.5	5.6		CN2	28.1 8	eP	12 41 18.5	0.3	
		sS	12 43 20.0	-4.5				epP	12 41 29.0	-0.2	
		LN	$M_s = 4.4$	9.0	0.30			ePP	12 42 08.0	-0.3	
		LE		9.0	0.50			S	12 46 00.0	2.7	
		LZ	$M_s = 4.7$	15.0	2.60			LN	$M_s = 4.8$	14.0	1.10
TIA	20.3 353	-P	12 40 04.5	0.8				LE		14.0	0.40
		eS	12 43 46.0	1.7				LZ	$M_s = 4.4$	24.0	1.10
		LN	$M_s = 4.5$	14.0	1.07	GTA	29.4 327	-P	12 41 30.0	-0.1	
		LZ	$M_s = 4.5$	17.0	1.63			S	12 46 21.0	2.7	
XAN	20.7 332	P	12 40 06.0	-1.2				LE	$M_s = 4.7$	12.0	0.93
		S	12 43 53.0	3.2				LZ	$M_s = 4.7$	22.0	1.95
		LN	$M_s = 4.8$	12.0	1.80	MDJ	29.6 14	eP	12 41 31.5	-0.4	
		LE		10.0	0.40	LSA	30.0 302	P	12 41 34.2	-1.6	
CD2	21.2 317	eP	12 40 12.1	-0.2		WMQ	39.1 322	P	12 42 54.0	0.3	
		eS	12 44 04.0	4.0				S	12 48 50.5	1.4	
		LN	$M_s = 4.8$	12.5	1.76			ScS	12 53 00.0	4.2	
		LZ	$M_s = 4.5$	18.0	1.46			LN	$M_s = 5.0$	12.0	0.70
TIY	22.7 344	-P	12 40 29.4	1.7				LE		11.0	0.58
		PMZ	$m_b = 5.2$	1.2	0.13			LZ	$M_s = 4.9$	16.0	1.39
		pP	12 40 40.0	1.6		KSH	45.1 310	eP	12 43 44.0	1.2	
		S	12 44 30.0	2.3		MAY 29d 18h 31m $11.0 \pm 0.03s$ , $SD1.02 / 496$ $56.97 N \pm 0.72km$ , $153.60 W \pm 0.58km$ , $h24 \pm 0.10km$ Kodiak Island region (13) $M_s 6.2 / 60$ , $m_b 5.9 / 28$ , $m_b 5.8 / 108$					
		sS	12 44 43.0	-3.5		MDJ	47.6 290	+P	18 39 46.0	-1.1	
		LN	$M_s = 4.9$	15.0	2.20			PMZ	$m_b = 5.5$	1.2	0.080
		LZ	$M_s = 4.7$	17.0	2.16			pP	18 39 55.0	0.2	
DL2	22.9 3	eP	12 40 29.0	-0.1				S	18 46 36.0	-3.1	
		sP	12 40 41.0	-3.9				LN	$M_s = 5.9$	14.0	6.36
		S	12 44 32.0	1.7				LZ	$M_s = 5.1$	20.0	2.01
		LN	$M_s = 4.6$	13.0	0.86			+iP	18 40 07.0	-0.9	
		LE		10.0	0.28			PMZ	$m_b = 6.3$	1.0	0.40
		LZ	$M_s = 4.1$	18.0	0.60			PMZ	$m_b = 6.0$	6.0	1.30
BJI	24.2 352	eP	12 40 43.0	0.7		CN2	50.3 292	pP	18 40 17.0	1.4	
		PMZ	$m_b = 5.4$	1.2	0.19			PP	18 42 03.0	-0.5	
		PMZ	$m_b = 5.0$	10.0	0.64			eS	18 47 15.0	-2.9	
		PcP	12 44 22.5	-0.1				SMN		6.0	1.00
		eS	12 44 56.0	1.2				SME		6.0	1.10
		LZ	$M_s = 4.5$	20.0	1.50			ScS	18 49 52.0	-1.7	
LZH	24.8 327	-iP	12 40 49.0	1.0				LN	$M_s = 6.0$	17.0	8.40
		PMZ	$m_b = 5.3$	1.5	0.18			LE		17.0	1.90
		PMZ	$m_b = 5.3$	4.0	0.48			LZ	$M_s = 5.7$	19.0	8.20
		pP	12 40 55.5	-3.2				+iP	18 40 25.0	-0.8	
		sP	12 40 59.8	-3.8		SNY	52.6 291	PMZ	$m_b = 6.1$	1.2	0.30
		PcP	12 44 25.0	1.2				PMZ	$m_b = 6.0$	7.0	1.60
		eS	12 45 07.0	2.2				sP	18 40 37.0	0.0	
		sS	12 45 18.0	-4.7				PP	18 42 22.0	-3.4	
		LN	$M_s = 4.9$	14.0	1.84			S	18 47 48.0	-1.5	
		LE		12.0	0.71			SMN		34.0	4.03
		LZ	$M_s = 4.6$	20.0	1.70			SME		24.0	3.06
HHC	25.9 345	P	12 40 59.0	0.6				sS	18 48 06.0	2.4	
		sP	12 41 12.0	-2.1				LN	$M_s = 6.1$	20.0	7.55
		PP	12 41 44.0	5.1				LE		14.0	7.82
		S	12 45 26.0	4.1				LZ	$M_s = 5.9$	18.0	11.4
		sS	12 45 41.5	0.0				+P	18 40 48.0	-1.0	
		LN	$M_s = 4.9$	13.0	1.60			PMZ	$m_b = 5.7$	1.0	0.11
		LE		13.0	0.30			PMZ	$m_b = 5.8$	7.0	0.84
		LZ	$M_s = 4.8$	16.0	2.01			PP	18 42 54.0	-0.3	
SNY	25.9 6	-P	12 40 57.7	-0.7		DL2	55.8 290	S	18 48 32.0	-0.1	
		PMZ	$m_b = 5.2$	1.0	0.060			LN	$M_s = 6.0$	15.0	5.60
		pP	12 41 06.2	-3.0				LE		16.0	4.80
		eS	12 45 25.0	2.1				LZ	$M_s = 5.8$	18.0	8.15
		LN	$M_s = 4.9$	19.0	2.26			eP	18 41 01.5	-1.1	
		LE		15.0	1.03			PMZ	$m_b = 5.7$	1.4	0.16
		LZ	$M_s = 4.6$	14.0	1.18						
BTO	26.1 342	P	12 41 00.5	0.4		BJI	57.7 295				
		pP	12 41 11.0	0.1							
		S	12 45 28.0	3.0							



		PMZ	$m_B = 5.7$	8.0	0.87			LZ	$M_S = 5.7$	20.0	5.01
		ePP	18 43 11.0	-0.4		LZH	66.8 301	+P	18 42 03.0	-0.6	
		eS	18 48 57.0	-1.4				PMZ	$m_b = 6.0$	1.5	0.36
		esS	18 49 13.0	1.5				PMZ	$m_B = 6.0$	7.0	1.49
		LN	$M_S = 6.2$	14.0	8.70			pP	18 42 12.5	1.2	
		LZ	$M_S = 6.0$	16.0	9.90			PcP	18 42 35.0	3.7	
HHC	59.3 298	+P	18 41 14.0	-0.2				PP	18 44 33.0	1.6	
		PMZ	$m_b = 6.2$	1.0	0.29			S	18 50 52.0	0.2	
		PMZ	$m_B = 5.7$	7.0	0.66			SMN		6.0	0.90
		PcP	18 42 04.0	3.1				sS	18 51 09.0	2.7	
		S	18 49 19.0	0.3				ScS	18 51 55.0	0.6	
		sS	18 49 35.0	2.1				SS	18 55 10.0	-1.6	
		LN	$M_S = 6.1$	15.0	5.63			LN	$M_S = 6.4$	15.0	10.3
		LE		15.0	4.95			LE		16.0	7.90
TIA	60.2 291	-P	18 41 19.3	-0.5				LZ	$M_S = 6.3$	18.0	17.3
		eS	18 49 29.0	-1.5		WMQ	67.2 316	+iP	18 42 06.5	0.1	
		LN	$M_S = 6.1$	19.0	5.49			PMZ	$m_b = 5.6$	1.0	0.080
		LE		16.0	4.86			PMZ	$m_B = 6.2$	6.0	1.95
		LZ	$M_S = 5.9$	19.0	8.77			LN	$M_S = 6.0$	13.0	3.71
BTO	60.3 299	P	18 41 20.0	-0.6				LZ	$M_S = 6.3$	16.0	15.3
		pP	18 41 30.0	1.7		QZH	68.3 282	+P	18 42 12.5	-0.3	
		S	18 49 30.0	-0.7				PMZ	$m_B = 5.9$	6.0	0.91
		LN	$M_S = 6.2$	15.0	6.20			pP	18 42 23.0	2.2	
		LE		15.0	7.00			S	18 51 10.0	0.1	
		LZ	$M_S = 6.0$	14.0	7.90			LN	$M_S = 5.8$	14.0	1.84
TIY	61.3 296	+P	18 41 27.4	-0.5				LE		14.0	1.81
		PMZ	$m_b = 5.7$	1.0	0.090			LZ	$M_S = 5.4$	19.0	2.24
		pP	18 41 40.0	4.4		CD2	71.1 298	eP	18 42 29.6	-0.3	
		S	18 49 41.0	-3.4				PMZ	$m_B = 5.9$	8.0	1.07
		sS	18 49 54.0	-4.7				sS	18 52 02.0	5.1	
		LN	$M_S = 6.3$	14.0	11.0			LN	$M_S = 6.3$	16.0	9.37
		LZ	$M_S = 6.2$	14.0	13.8			LZ	$M_S = 6.0$	17.0	6.85
SSE	62.0 285	+P	18 41 32.0	-0.3		GZH	72.6 285	P	18 42 38.0	-0.9	
		PMZ	$m_b = 5.6$	1.0	0.077			S	18 52 03.5	3.5	
		PMZ	$m_B = 5.9$	8.0	1.16			LN	$M_S = 6.1$	20.0	3.07
		S	18 49 58.0	5.0				LE		21.0	5.41
		sS	18 50 08.0	0.7				LZ	$M_S = 5.8$	15.0	4.27
		LN	$M_S = 5.8$	14.0	2.61	GYA	73.3 293	P	18 42 43.0	-0.2	
		LE		14.0	1.81			pP	18 42 53.4	2.6	
		LZ	$M_S = 5.5$	20.0	3.22			S	18 52 14.0	6.1	
NJ2	62.5 287	+P	18 41 34.0	-1.5				LN	$M_S = 6.3$	18.0	4.10
		PMZ	$m_B = 5.9$	7.0	1.05			LE		18.0	7.50
		pP	18 41 44.0	0.5		KSH	75.2 323	P	18 42 56.0	1.6	
		S	18 50 03.0	4.0				pP	18 43 06.0	3.9	
		LN	$M_S = 6.1$	16.0	5.81			PP	18 45 47.0	3.0	
		LE		18.0	4.14			eS	18 52 33.5	2.1	
		LZ	$M_S = 5.8$	16.0	5.61			sS	18 52 49.0	4.9	
GTA	65.9 306	+P	18 41 57.4	-0.7				LE	$M_S = 6.5$	16.0	12.7
		PMZ	$m_b = 6.5$	1.2	0.80			LZ	$M_S = 6.4$	19.0	18.5
		PMZ	$m_B = 6.2$	5.0	1.50	KMI	76.3 295	+P	18 43 01.5	0.6	
		S	18 50 44.5	3.1				PMZ	$m_b = 5.6$	2.0	0.14
		sS	18 50 53.0	-2.9				PMZ	$m_B = 6.0$	5.0	1.00
		i	18 50 58.5					PP	18 45 57.5	4.7	
		LN	$M_S = 6.6$	16.0	13.6			S	18 52 46.0	4.3	
		LE		17.0	13.5			LZ	$M_S = 6.1$	17.0	9.00
		LZ	$M_S = 5.6$	18.0	3.38	QZN	77.8 286	+P	18 43 08.0	-0.6	
XAN	66.0 296	P	18 41 58.0	-0.4				eS	18 52 57.0	-1.9	
		PMZ	$m_B = 5.9$	8.0	1.10			LN	$M_S = 6.0$	15.0	2.70
		sS	18 50 50.0	-6.6				LE		15.0	2.40
		LN	$M_S = 6.3$	14.0	5.48	LSA	77.9 306	P	18 43 10.6	0.6	
		LE		14.0	5.56			S	18 53 01.5	2.4	
WHN	66.0 289	+P	18 41 58.2	-0.4				LN	$M_S = 6.3$	16.0	5.65
		PMZ	$m_b = 5.6$	1.0	0.080			LE		16.0	3.97
		PMZ	$m_B = 6.0$	7.0	1.37			LZ	$M_S = 6.4$	17.0	15.3
		pP	18 42 08.0	1.4							
		S	18 50 48.0	5.2							
		LN	$M_S = 6.2$	18.0	6.80						
		LE		18.0	5.24						

MAY 30d 02h 34m 05.4 ± 0.03s, SD1.30 / 516  
 5.98 S ± 0.80km, 77.18 W ± 1.06km, h23 ± 0.09km  
 Northern Peru (111)









GZH	160.2	330	LE	20.0	8.20	
			PKP	02 54 04.5	0.7	
			PKP2	02 54 47.0	1.9	
			PPMZ	$m_b = 6.4$	12.0	3.94
KMI	160.9	0	LZ	$M_s = 6.6$	22.0	9.52
			PKP	02 54 06.0	1.2	
			sPKP	02 54 17.0	3.3	
			PKP2	02 54 50.0	1.7	
			PP	02 58 30.0	-2.5	
			PPMZ	$m_b = 6.4$	9.0	3.30
			LN	$M_s = 6.2$	17.0	1.00
			LE		17.0	1.90
QZN	165.3	333	LZ	$M_s = 6.9$	20.0	15.7
			PKP	02 54 09.0	0.0	
			pPKP	02 54 20.0	4.6	
			PKP2	02 55 06.5	-0.9	
			PP	02 58 55.0	-0.5	
			SKS	03 01 06.0	-1.5	
			SKKS	03 05 36.5	-2.0	
			LN	$M_s = 6.8$	19.0	3.54
LE		19.0	8.90			

MAY 30d 09h 22m  $22.8 \pm 0.04s$ , SD1.34 / 116  
 8.84 S  $\pm 0.60km$ , 122.61 E  $\pm 0.98km$ , h94  $\pm 0.13km$   
 Savu Sea (288)  
 $m_b 5.2 / 30$ ,

QZN	30.4	336	P	09 28 29.0	0.2	
			eS	09 33 23.0	1.2	
			LN		13.0	0.50
			LE		13.0	0.51
QZH	33.8	353	eP	09 28 58.5	0.2	
			+iP	09 29 37.6	0.8	
GYA	38.4	337	pP	09 30 00.8	2.6	
			S	09 35 21.0	-2.3	
			+P	09 29 43.5	1.8	
KMI	38.9	331	PMZ	$m_b = 5.5$	1.4	0.10
			P	09 29 50.5	2.5	
SSE	39.7	358	PMZ	$m_b = 4.9$	0.8	0.016
			eS	09 35 45.0	0.0	
			sS	09 36 22.0	-0.4	
			+P	09 29 51.5	1.6	
WHN	40.0	349	PMZ	$m_b = 5.2$	1.0	0.040
			+P	09 29 57.7	0.7	
NJ2	40.8	355	+P	09 29 57.7	0.7	
			+iP	09 30 15.8	-2.9	
CD2	43.5	336	PMZ	$m_b = 5.7$	1.2	0.15
			eP	09 30 48.0	-1.1	
TIY	47.3	349	S	09 37 30.0	-3.6	
			LE		15.0	0.54
			LZ		16.0	0.48
			+iP	09 30 55.6	0.3	
LZH	48.1	339	PMZ	$m_b = 5.6$	1.4	0.12
			pP	09 31 16.0	-1.0	
			eS	09 37 43.0	-2.8	
			LZ		20.0	0.39
LSA	48.8	323	P	09 31 01.1	-0.5	
			eP	09 31 01.0	-1.3	
BJI	49.0	353	PMZ	$m_b = 5.3$	1.1	0.043
			eP	09 31 11.0	-2.3	
HHC	50.5	349	eP	09 31 13.0	-0.9	
BTO	50.5	348	eP	09 31 14.5	0.1	
CN2	52.5	3	eP	09 31 28.5	-0.1	
GTA	52.5	338	+P	09 31 28.6	-0.2	
MDJ	53.6	6	eP	09 31 35.6	-1.3	
WMQ	61.2	332	P	09 32 29.8	-1.0	
			S	09 40 38.0	-2.7	
			SMN		5.0	0.35
			ScS	09 42 06.0	-2.4	

MAY 30d 10h 40m $05.7 \pm 0.03s$ , SD1.02 / 701 45.87 N $\pm 0.39km$ , 26.69 E $\pm 0.35km$ , h91 $\pm 0.23km$ Romania (358) $m_b 7.1 / 48$ , $m_b 6.5 / 65$ ,						
KSH	36.3	82	-iP	10 47 05.0	2.5	
			pP	10 47 27.0	3.7	
			S	10 52 35.0	0.1	
			LZ		12.0	140
WMQ	42.4	70	P	10 47 54.4	1.3	
			PP	10 49 38.2	3.3	
			S	10 54 08.0	1.3	
			LN		10.0	206
LSA	52.1	84	P	10 49 09.5	0.2	
			pP	10 49 32.0	1.4	
			PcS	10 54 14.5	-1.3	
			sS	10 57 01.5	-0.8	
			SMN		10.0	30.6
			SME		8.0	24.6
			+iP	10 49 12.0	0.1	
			PMZ	$m_b = 7.1$	1.2	2.72
GTA	52.4	69	PMZ	$m_b = 7.1$	10.0	27.0
			pP	10 49 30.0	-3.5	
			sP	10 49 44.0	-0.2	
			PP	10 51 16.0	3.7	
			iS	10 56 30.0	0.0	
			SMN		9.0	36.7
			sS	10 57 04.0	-3.5	
			SS	11 00 10.0	4.4	
			LE		12.0	79.8
			LZ		24.0	145
			+iP	10 49 45.0	0.3	
			PMZ	$m_b = 6.3$	2.5	1.03
LZH	57.0	70	PMZ	$m_b = 7.2$	9.0	29.1
			pP	10 50 05.0	-1.5	
			sP	10 50 16.0	-1.1	
			PcP	10 50 39.0	1.2	
			PP	10 51 54.0	1.1	
			PcS	10 54 40.0	2.9	
			iS	10 57 30.0	-0.4	
			SMN		10.0	17.4
			sS	10 58 06.0	-2.4	
			SS	11 01 18.0	-1.8	
			LN		12.0	46.9
			LE		10.0	27.1
BTO	58.3	63	LZ		36.0	167
			+iP	10 49 54.0	0.0	
			PMZ	$m_b = 7.3$	6.0	23.2
			pP	10 50 15.0	-1.0	
			PP	10 52 07.0	2.1	
			iS	10 57 48.0	0.1	
			sS	10 58 30.0	3.9	
			LN		11.0	31.1
HHC	59.1	62	LE		11.0	38.3
			LZ		11.0	27.8
			+iP	10 49 59.0	-0.6	
			PMZ	$m_b = 7.2$	6.0	18.4
			PP	10 52 12.0	-0.2	
			S	10 57 57.0	0.0	
			LN		12.0	58.8
			LE		12.0	89.0
CD2	60.0	75	LZ		34.0	166
			+iP	10 50 05.4	-0.3	
			PMZ	$m_b = 7.4$	6.0	28.7
			sP	10 50 39.5	1.1	
XAN	61.5	69	PP	10 52 16.0	-4.2	
			iS	10 58 05.5	-4.3	
			+iP	10 50 15.5	-0.4	
			PMZ	$m_b = 7.2$	9.0	30.8



			PP	10 52 32.0	-1.8				iS	10 59 20.0	-0.1		
			S	10 58 30.0	2.3				SMN			11.5	18.9
			LN			10.0	37.5		SME			10.5	14.2
			LE			10.0	34.3		sS	11 00 00.0	0.8		
TIY	61.5	64	+iP	10 50 15.7	-0.3				SS	11 03 36.0	0.0		
			PMZ		$m_b = 6.5$	1.0	0.68		LN			14.0	56.7
			PMZ		$m_B = 7.2$	8.0	23.3		LE			15.5	86.6
			pP	10 50 35.0	-3.3				LZ			32.0	80.6
			PP	10 52 34.0	0.1			DL2	66.4	58	+P	10 50 46.6	-1.1
			S	10 58 30.0	2.2				PMZ		$m_b = 6.7$	1.6	1.96
			sS	10 59 09.5	1.7				PMZ		$m_B = 7.1$	6.0	16.5
			SS	11 02 34.0	2.1				pP	10 51 10.0	-0.4		
			LN			12.0	46.0		S	10 59 28.0	-0.1		
			LE			10.0	32.7		SMN			10.0	16.9
			LZ			28.0	82.7		SME			6.0	7.89
BJI	62.4	60	+P	10 50 21.5	-0.3				sS	11 00 10.0	1.5		
			PMZ		$m_b = 6.3$	1.5	0.59		LN			15.0	58.2
			PMZ		$m_B = 7.1$	6.0	16.6		LE			14.0	73.3
			pP	10 50 42.0	-2.3				LZ			30.0	53.0
			sP	10 50 52.0	-2.8			MDJ	67.1	49	+iP	10 50 51.0	-1.2
			eS	10 58 40.0	-0.2				PMZ		$m_b = 6.7$	2.0	2.46
			esS	10 59 15.0	-4.0				PMZ		$m_B = 7.2$	6.0	23.4
			eSS	11 02 46.0	-0.1				pP	10 51 16.0	1.1		
			LN			8.0	80.4		PP	10 53 24.0	2.1		
			LE			10.0	35.1		iS	10 59 40.0	2.1		
KMI	62.9	81	+iP	10 50 25.5	-0.2				SMN			10.0	31.9
			PMZ		$m_B = 7.1$	12.0	33.2		sS	11 00 22.0	5.0		
			PP	10 52 43.0	-2.6				ScS	11 00 37.0	0.4		
			iS	10 58 48.0	0.5			WHN	67.3	69	+iP	10 50 53.0	-0.3
			SS	11 02 56.0	1.3				PMZ		$m_b = 6.7$	1.5	1.64
			LN			9.0	10.6		PMZ		$m_B = 7.1$	8.0	20.3
			LE			9.0	2.40		pP	10 51 15.0	-1.0		
			LZ			36.0	47.5		iS	10 59 40.0	-0.1		
GYA	64.8	77	+iP	10 50 37.0	-0.6				LN			10.0	9.23
			PMZ		$m_b = 6.5$	1.2	0.80		LE			11.0	21.3
			PMZ		$m_B = 7.5$	4.0	27.6		LZ			24.0	46.2
			pP	10 51 01.0	1.0			NJ2	69.2	65	+iP	10 51 04.0	-1.1
			PcP	10 51 07.0	-2.3				PMZ		$m_b = 6.7$	1.2	1.40
			PP	10 53 01.0	-1.1				PMZ		$m_B = 6.9$	6.0	10.6
			S	10 59 10.0	1.5				pP	10 51 27.0	-0.9		
			LN			18.0	22.6		sP	10 51 41.0	2.7		
			LE			18.0	32.3		PP	10 53 39.0	-1.7		
			LZ			24.0	30.4		iS	11 00 02.0	-0.9		
TIA	65.4	63	+P	10 50 40.2	-1.2				sS	11 00 43.5	1.3		
			PMZ		$m_B = 7.0$	9.0	17.7		ScS	11 00 52.0	-1.0		
			PP	10 53 08.0	0.3				LN			11.0	14.9
			S	10 59 12.0	-3.9				LE			13.0	15.3
			sS	10 59 58.0	1.8				LZ			30.0	30.2
			SS	11 03 36.0	3.4			SSE	71.3	65	-iP	10 51 17.2	-0.8
			LN			12.0	26.7		PMZ		$m_B = 6.9$	12.0	22.1
			LE			12.0	33.8		PcP	10 51 35.0	-1.6		
CN2	65.4	52	+iP	10 50 40.5	-0.9				pP	10 51 38.0	-2.9		
			PMZ		$m_B = 7.2$	6.0	19.5		sP	10 51 48.0	-3.2		
			pP	10 51 01.5	-2.5				PP	10 53 58.0	-0.7		
			sP	10 51 11.0	-3.4				S	11 00 23.0	-3.0		
			eS	10 59 16.0	-1.3				SKS	11 01 03.0	-4.1		
			SMN			9.0	18.7		ScS	11 01 06.0	-3.6		
			SME			9.0	15.3		SS	11 05 08.0	3.9		
			SS	11 03 31.0	-1.7				LN			12.0	18.8
			LN			17.0	64.2		LZ			11.0	5.71
			LE			17.0	81.0	GZH	71.6	76	+iP	10 51 20.0	0.5
			LZ			18.0	47.4		PMZ		$m_B = 7.2$	10.0	37.7
SNY	65.6	55	+iP	10 50 42.0	-0.9				pP	10 51 42.0	-0.4		
			PMZ		$m_b = 6.7$	1.3	1.33		sP	10 51 53.0	0.3		
			PMZ		$m_B = 7.0$	9.0	20.9		iS	11 00 33.0	2.6		
			pP	10 51 03.5	-2.0				LN			17.0	34.4
			PcP	10 51 13.0	0.3				LE			12.0	8.45
			PP	10 53 10.0	0.1				LZ			30.0	60.4



QZN	71.9	81	+iP	10 51 22.2	0.6		
			PMZ	$m_b = 6.8$	1.0	1.60	
			PMZ	$m_B = 7.1$	12.0	35.0	
			pP	10 51 43.0	-1.5		
			PP	10 54 03.0	-0.4		
			iS	11 00 35.0	0.5		
			SMN		12.0	18.3	
			SME		11.0	24.2	
			sS	11 01 12.0	-2.0		
			LN		16.5	16.0	
			LE		13.0	23.2	
QZH	73.8	71	+iP	10 51 31.5	-1.2		
			PMZ	$m_b = 6.8$	0.9	1.46	
			PMZ	$m_B = 6.9$	7.0	14.8	
			pP	10 51 54.5	-1.2		
			iS	11 00 54.5	-1.3		
			sS	11 01 32.0	-3.7		
			SS	11 05 38.0	-4.4		
			LN		11.0	15.9	
			LE		12.0	13.5	
			LZ		26.0	29.3	

MAY 30d 16h 49m  $26.5 \pm 0.05s$ , SD1.75 / 219  
 6.00 S  $\pm 0.85km$ , 77.08 W  $\pm 1.52km$ , h19  $\pm 0.27km$   
 Northern Peru (111)  
 $M_S 5.6 / 1$ ,  $m_b 5.2 / 51$ ,

MDJ	135.0	333	ePKP	17 08 45.7	-0.1		
CN2	137.5	336	ePKP	17 08 50.0	-0.3		
SNY	139.9	336	PKP	17 08 50.8	-3.8		
WMQ	140.0	17	ePKP	17 08 50.2	-4.8		
DL2	143.1	335	ePKP	17 08 57.8	-2.5		
BJI	144.1	343	ePKP	17 08 59.5	-2.4		
			LZ	$M_S = 5.5$	16.0	0.58	
HHC	144.4	349	ePKP	17 09 02.0	-0.7		
BTO	145.0	351	ePKP	17 09 02.0	-1.7		
GTA	146.6	4	PKP	17 09 07.7	1.2		
			PP	17 12 37.0	2.9		
			LZ	$M_S = 5.6$	24.0	1.12	
TIA	147.2	338	ePKP	17 09 08.3	0.9		
TIY	147.3	346	PKP	17 09 09.4	1.9		
			LE	$M_S = 5.6$	16.0	0.52	
			LZ	$M_S = 5.5$	24.0	0.95	
SSE	149.7	328	PKP	17 09 08.0	-3.3		
			pPKP	17 09 18.0	1.3		
LZH	150.0	358	+PKP	17 09 14.5	2.4		
			pPKP	17 09 20.0	2.8		
			PKP2	17 09 25.0	1.5		
			ePP	17 12 52.0	-1.6		
			LZ	$M_S = 5.3$	28.0	0.67	
NJ2	150.1	332	PKP	17 09 13.0	1.1		
			pPKP	17 09 18.3	1.0		
			PKP2	17 09 23.0	-0.8		
XAN	151.5	349	PKP	17 09 16.0	1.8		
WHN	153.3	338	ePKP	17 09 18.5	1.9		
CD2	155.2	358	ePKP	17 09 22.5	3.3		
GYA	159.3	350	PKP	17 09 27.2	2.5		
			pPKP	17 09 34.8	5.0		
			PKP2	17 10 04.4	1.4		
			PP	17 13 49.4	4.3		
KMI	161.0	0	+PKP	17 09 28.5	2.1		
QZN	165.4	333	ePKP	17 09 26.4	-4.2		

MAY 31d 00h 17m  $47.4 \pm 0.03s$ , SD1.04 / 624  
 45.85 N  $\pm 0.40km$ , 26.80 E  $\pm 0.35km$ , h91  $\pm 0.24km$   
 Romania (358)  
 $m_b 6.3 / 21$ ,  $m_B 6.0 / 100$ ,

KSH	36.2	82	+iP	00 24 45.0	1.3		
			pP	00 25 03.0	-1.4		

			PP	00 26 08.0	1.0		
			S	00 30 18.0	2.4		
			LE		10.0	20.0	
			LZ		15.0	20.2	
WMQ	42.3	70	-iP	00 25 34.0	-0.4		
			PMZ	$m_b = 6.1$	2.5	0.68	
			PP	00 27 13.5	-2.5		
			iS	00 31 47.0	-1.7		
			LE		9.0	17.5	
LSA	52.0	85	P	00 26 51.0	0.4		
			PMZ		3.0	3.26	
			iS	00 34 08.0	1.9		
			SMN		9.0	4.05	
			SS	00 37 40.0	0.2		
GTA	52.4	69	-P	00 26 53.2	0.0		
			pP	00 27 15.0	0.3		
			S	00 34 13.0	3.5		
			LE		16.0	19.8	
			LZ		30.0	43.6	
LZH	56.9	70	-P	00 27 26.5	0.5		
			PMZ	$m_b = 6.5$	2.5	1.47	
			PMZ	$m_B = 6.4$	5.0	2.72	
			pP	00 27 48.0	0.3		
			sP	00 27 57.5	-0.8		
			PcP	00 28 22.0	2.7		
			S	00 35 11.0	1.2		
			SMN		12.0	4.41	
			sS	00 35 53.0	3.8		
			ScS	00 37 06.0	4.3		
			SS	00 39 00.0	-0.5		
			LN		9.0	5.62	
			LE		10.0	4.59	
			LZ		29.0	23.5	
BTO	58.2	63	-iP	00 27 35.0	-0.3		
			PMZ	$m_B = 6.5$	4.0	2.40	
			pP	00 27 58.0	0.7		
			PP	00 29 48.0	1.8		
			iS	00 35 30.0	1.1		
			sS	00 36 08.0	1.0		
			LN		9.0	7.10	
			LE		9.0	8.60	
			LZ		9.0	4.60	
HHC	59.0	62	-P	00 27 41.0	0.0		
			PMZ	$m_b = 6.1$	0.8	0.20	
			PMZ	$m_B = 6.6$	5.0	4.35	
			pP	00 28 04.0	1.0		
			sP	00 28 11.0	-2.5		
			PP	00 29 55.0	1.6		
			S	00 35 44.0	6.0		
			SMN		10.0	4.78	
			SME		10.0	1.96	
			LN		10.0	9.72	
			LE		10.0	8.18	
			LZ		21.0	20.3	
CD2	59.9	75	P	00 27 47.1	0.1		
			PMZ	$m_b = 6.4$	0.7	0.38	
			pP	00 28 08.8	-0.3		
			sP	00 28 20.1	0.5		
			iS	00 35 53.2	2.5		
			sS	00 36 29.0	0.0		
			LZ		10.0	4.02	
XAN	61.4	69	-iP	00 27 58.0	0.8		
			PMZ	$m_B = 5.9$	5.0	0.80	
			pP	00 28 21.0	1.5		
			S	00 36 14.0	5.3		
			LN		10.0	5.65	
			LE		9.0	3.35	
TIY	61.5	64	+P	00 27 57.2	-0.2		



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			PMZ	$m_b = 5.8$	1.0	0.13			SMN				10.9	3.43	
			pP	00 28 19.5	-0.1				LN				8.0	5.27	
			PP	00 30 16.5	1.5				LE				2.0	4.36	
			S	00 36 13.0	4.1				LZ				30.0	9.57	
			sS	00 36 52.5	3.8			MDJ	67.0	49	-iP	00 28 33.5	-0.2		
			SS	00 40 17.0	4.3						PMZ	$m_b = 5.6$	1.2	0.10	
			LN			13.5	11.8				pP	00 28 56.0	-0.3		
			LZ			20.0	16.5				iS	00 37 20.0	0.8		
BJI	62.4	60	eP	00 28 03.0	-0.2						sS	00 38 02.0	3.8		
			PMZ	$m_b = 6.3$		1.7	0.64				LN		9.0	7.15	
			pP	00 28 24.0	-1.6						LZ		25.0	16.6	
			PP	00 30 22.0	-0.8			WHN	67.2	69	P	00 28 34.5	-0.1		
			eS	00 36 20.0	-1.3						PMZ	$m_b = 5.6$	1.0	0.080	
			SS	00 40 27.0	0.0						PMZ	$m_b = 6.2$	4.0	1.46	
			LN			8.0	9.62				pP	00 28 56.0	-1.3		
			LZ			23.0	15.3				S	00 37 22.0	2.2		
KMI	62.9	81	-P	00 28 06.5	-0.5						LN		14.0	2.70	
			pP	00 28 30.0	0.9						LE		12.0	3.99	
			PP	00 30 24.5	-2.2			NJ2	69.1	65	-iP	00 28 47.0	0.5		
			S	00 36 28.0	1.4						PMZ	$m_b = 6.0$	1.0	0.21	
			LN			8.0	1.10				PMZ	$m_b = 6.2$	4.0	1.51	
			LE			8.0	0.80				pP	00 29 08.0	-1.3		
			LZ			32.0	14.7				sP	00 29 22.0	2.4		
GYA	64.7	77	-P	00 28 19.0	0.1						S	00 37 46.0	3.4		
			PMZ	$m_b = 6.0$		1.0	0.20				LN		12.0	4.61	
			pP	00 28 42.4	1.2						LE		12.5	2.41	
			PcP	00 28 52.0	1.3						LZ		22.0	3.15	
			S	00 36 52.0	2.5			SSE	71.2	65	-P	00 28 59.0	-0.3		
			sS	00 37 32.0	2.4						PMZ	$m_b = 5.7$	1.0	0.11	
			ScS	00 38 04.0	3.9						PMZ	$m_b = 6.1$	4.0	1.21	
TIA	65.3	63	P	00 28 22.1	-0.7						pP	00 29 18.0	-4.2		
			PMZ	$m_b = 6.8$		1.0	1.27				PP	00 31 38.0	-1.9		
			pP	00 28 44.2	-1.1						eS	00 38 08.0	-0.5		
			S	00 36 56.0	-1.0						ScS	00 38 50.0	-1.0		
			ScS	00 38 09.4	4.6						SS	00 42 44.0	-1.0		
			SS	00 41 13.0	-0.5						LN		11.0	2.78	
			LN			11.0	3.84				LE		11.0	0.88	
			LE			11.0	5.70				LZ		20.0	3.22	
			LZ			32.0	15.9	GZH	71.5	76	P	00 29 02.0	1.2		
CN2	65.3	52	+iP	00 28 22.5	-0.4						PMZ	$m_b = 5.7$	1.2	0.14	
			PMZ	$m_b = 6.4$		1.0	0.50				pP	00 29 24.0	0.3		
			PMZ	$m_b = 6.7$		4.0	4.80				sP	00 29 33.0	-1.0		
			pP	00 28 43.5	-1.9						S	00 38 15.0	5.1		
			PP	00 30 46.0	-3.1						LN		11.0	1.86	
			S	00 36 57.0	-0.2						LE		10.0	5.49	
			sS	00 37 33.0	-4.4						LZ		30.0	9.72	
			SS	00 41 12.0	-1.8										
			LN			8.0	5.30	QZN	71.8	81	P	00 29 03.2	0.3		
			LE			8.0	10.6				PMZ	$m_b = 5.7$	0.8	0.087	
			LZ			14.0	13.7				pP	00 29 25.0	-0.8		
SNY	65.6	55	-iP	00 28 23.5	-0.8						eS	00 38 16.0	0.6		
			PMZ	$m_b = 5.9$		1.2	0.19				sS	00 39 00.0	5.2		
			PMZ	$m_b = 6.5$		7.0	5.28				SS	00 42 54.0	0.3		
			pP	00 28 45.0	-1.9						LN		12.0	2.51	
			PcP	00 28 55.0	0.7						LE		13.0	3.22	
			S	00 36 58.0	-2.0			QZH	73.7	71	eP	00 29 13.6	-0.5		
			SMN			10.5	2.70				PMZ	$m_b = 5.6$	0.7	0.070	
			SME			11.0	1.80				pP	00 29 36.0	-1.0		
			sS	00 37 37.0	-3.2						S	00 38 37.5	2.1		
			ScS	00 38 07.0	0.2						sS	00 39 12.5	-4.2		
			LN			10.0	4.41				LE		11.0	2.70	
			LE			9.0	5.24				LZ		27.0	4.77	
			LZ			32.0	15.0			-----					
DL2	66.3	58	-iP	00 28 29.0	-0.2			MAY 31d 07h 35m 26.3±0.03s, SD1.11/330							
			PMZ	$m_b = 6.0$		0.7	0.14	17.28 N±0.86km, 100.70 W±0.76km, h21±0.30km							
			PMZ	$m_b = 6.2$		4.0	1.44	Near coast of Guerrero, Mexico (58)							
			pP	00 28 51.0	-0.8			$M_S 6.4 / 31, m_b 6.3 / 11, m_b 5.7 / 67$							
			S	00 37 10.0	0.8			MDJ	103.3	326	+P	07 49 25.0	-1.8		
											PP	07 53 40.0	-3.8		



CN2	106.0	327	SKS	08 00	02.0	-0.8			SS	08 12	28.6	0.5				
			S	08 01	04.0	-4.0			LN		$M_s=6.5$	16.0	3.78			
			LN		$M_s=6.5$	14.0	6.00			LE			14.0	1.58		
			Pdif	07 49	38.0	-0.8			LZH	122.1	337	LZ		$M_s=5.9$	20.0	2.50
			PP	07 54	04.0	0.1			+PKP			07 54	21.0	0.3		
SNY	108.4	327	SS	08 09	01.0	0.0			PP	07 55	58.0	-0.4				
			LN		$M_s=6.3$	17.0	4.30		PPMZ		$m_B=6.2$	7.0	0.70			
			LE			17.0	1.10		SS	08 12	30.0	-2.8				
			LZ		$M_s=6.3$	18.0	8.10		LN		$M_s=6.4$	16.0	1.75			
			-Pdif	07 49	51.0	1.8			LE			16.0	3.04			
DL2	111.5	326	PP	07 54	17.0	-4.7			LZ		$M_s=6.1$	21.0	4.36			
			LN		$M_s=6.4$	16.0	3.96	KSH	123.4	3	ePKP	07 54	23.0	-0.3		
			LE			14.0	2.10		sPKP	07 54	37.0	5.4				
			LZ		$M_s=6.4$	17.0	8.00		PP	07 56	13.0	5.2				
			ePKP	07 54	00.0	0.1			SKS	08 01	30.0	-0.1				
BJI	113.4	330	PP	07 54	40.0	-4.3			SKKS	08 03	00.0	2.8				
			PPMZ		$m_B=6.5$	5.0	0.78		LE		$M_s=6.6$	15.0	5.60			
			LN		$M_s=6.4$	15.0	2.69		LZ		$M_s=6.4$	18.0	6.80			
			LE			14.0	2.70	CD2	126.6	334	ePKP	07 54	30.0	0.6		
			LZ		$M_s=5.9$	16.0	2.63		PP	07 56	24.6	-4.0				
HHC	114.9	333	Pdif	07 50	12.0	0.5			PPMZ		$m_B=6.4$	6.0	1.02			
			PP	07 54	59.0	0.0			LN		$M_s=6.4$	15.0	3.19			
			PPMZ		$m_B=6.1$	12.0	0.83		LZ		$M_s=6.0$	17.0	2.79			
			LN		$M_s=6.3$	16.0	3.62	GYA	129.0	328	PKP	07 54	35.0	0.9		
			LZ		$M_s=6.3$	15.0	6.10		PP	07 56	44.0	-1.1				
BTO	115.7	334	ePKP	07 54	05.8	-0.9			LN		$M_s=6.7$	18.0	6.00			
			PP	07 55	07.0	-2.0			LE			18.0	4.60			
			SKS	08 01	13.0	-0.9			LZ		$M_s=5.8$	24.0	2.50			
			LN		$M_s=6.5$	14.0	3.53	LSA	131.9	346	PKP	07 54	37.0	-3.0		
			LE			14.0	2.92	KMI	132.0	331	PKP	07 54	40.5	0.5		
TIA	115.9	327	LZ		$M_s=6.1$	20.0	4.98		PP	07 57	02.0	-2.1				
			ePKP	07 54	11.0	2.7			PPMZ		$m_B=6.4$	6.0	1.10			
			eSS	08 11	11.0	0.6			LZ		$M_s=6.3$	18.0	4.90			
			LN		$M_s=6.5$	15.0	4.00	QZN	133.1	319	PKP	07 54	42.0	0.3		
			LE			15.0	2.50		PP	07 57	10.0	-0.3				
TIY	117.0	331	LZ		$M_s=6.3$	16.0	5.80		LN		$M_s=6.5$	17.0	3.00			
			ePKP	07 54	10.0	1.4			LE			16.5	2.90			
			LN		$M_s=6.3$	15.0	2.50									
			LE			15.0	1.70									
			LZ		$M_s=6.3$	12.0	4.60									
SSE	117.3	320	ePKP	07 54	11.8	1.0										
			PP	07 55	21.0	-3.2										
			LN		$M_s=6.7$	16.0	7.66									
			LZ		$M_s=6.6$	16.0	12.9									
			ePKP	07 54	09.0	-2.2										
NJ2	118.0	322	sPKP	07 54	22.5	2.9										
			PP	07 55	27.0	1.1										
			PPMZ		$m_B=6.1$	8.0	0.63									
			eSS	08 11	28.0	-2.7										
			LN		$M_s=6.4$	16.0	3.12									
WMQ	118.7	353	LE			16.0	2.26									
			LZ		$M_s=6.2$	16.0	4.59									
			ePKP	07 54	11.0	-1.6										
			LN		$M_s=6.3$	15.0	2.42									
			LE			15.0	1.07									
GTA	120.4	342	LZ		$M_s=5.7$	20.0	1.95									
			PKP	07 54	14.3	0.2										
			PP	07 55	33.0	-3.1										
			SS	08 11	48.0	-1.4										
			LZ		$M_s=6.6$	22.0	16.4									
WHN	121.7	324	PKP	07 54	18.0	0.5										
			PP	07 55	44.0	-2.8										
			SS	08 12	08.0	-3.7										
			LN		$M_s=6.4$	15.0	3.66									
			LZ		$M_s=6.4$	18.0	7.65									
WHN	121.7	324	PKP	07 54	19.0	-0.8										
			sPKP	07 54	33.0	4.8										
			PP	07 55	56.0	0.2										